

1 **Distribution of stress state in the Nankai subduction zone, southwest**

2 **Japan and a comparison with Japan Trench**

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4 Weiren Lin<sup>1,2\*</sup>, Timothy B. Byrne<sup>3</sup>, Masataka Kinoshita<sup>4,5</sup>, Lisa C. McNeill<sup>6</sup>, Chandong  
5 Chang<sup>7</sup>, Jonathan C. Lewis<sup>8</sup>, Yuzuru Yamamoto<sup>9</sup>, Demian M. Saffer<sup>10</sup>, J. Casey Moore<sup>11</sup>,  
6 Hung-Yu Wu<sup>5</sup>, Takeshi Tsuji<sup>12</sup>, Yasuhiro Yamada<sup>5</sup>, Marianne Conin<sup>13</sup>, Saneatsu Saito<sup>5</sup>,  
7 Takatoshi Ito<sup>14</sup>, Harold J. Tobin<sup>15</sup>, Gaku Kimura<sup>16</sup>, Kyuichi Kanagawa<sup>17</sup>, Juichiro Ashi<sup>18</sup>,  
8 Michael B. Underwood<sup>19</sup>, Toshiya Kanamatsu<sup>20</sup>

9

10 <sup>1</sup>Graduate School of Engineering, Kyoto University, Kyoto, Japan

11 <sup>2</sup>Kochi Institute for Core Sample research, Japan Agency for Marine-Earth Science and Technology,  
12 Nankoku, Japan

13 <sup>3</sup>Center for Integrative Geosciences, University of Connecticut, Storrs, Connecticut, USA.

14 <sup>4</sup>Earthquake Research Institute, The University of Tokyo, Tokyo, Japan

15 <sup>5</sup>Institute for Research on Earth Evolution, Japan Agency for Marine-Earth Science and Technology,  
16 Yokohama, Japan.

17 <sup>6</sup>Southampton Oceanography Centre, University of Southampton, Southampton, UK.

18 <sup>7</sup>Department of Geology, Chungnam National University, Daejeon, Korea

19 <sup>8</sup>Department of Geoscience, Indiana University of Pennsylvania, Indiana, Pennsylvania, USA.

20 <sup>9</sup>Department of Mathematical Science and Advanced Technology, Japan Agency for Marine and Earth  
21 Science and Technology, Yokohama, Japan

22 <sup>10</sup>Department of Geosciences and Center for Geofluids, Geomechanics, and Geohazards, The Pennsylvania  
23 State University, Pennsylvania, USA

24 <sup>11</sup>Earth and Planetary Sciences Department, University of California, Santa Cruz, California, USA

25 <sup>12</sup>International Institute for Carbon-Neutral Energy Research, Kyushu University, Fukuoka, Japan

26 <sup>13</sup>University of Lorraine – ENSMN, Nancy, France

27 <sup>14</sup>Institute of Fluid Science, Tohoku University, Sendai, Japan

28 <sup>15</sup>Department of Geoscience, Univ. Wisconsin — Madison, Madison, USA

29 <sup>16</sup>Department of Earth and Planetary Science, The University of Tokyo, Tokyo, Japan

30 <sup>17</sup>Department of Earth Sciences, Chiba University, Chiba, Japan.

31 <sup>18</sup>Atmosphere and Ocean Research Institute, The University of Tokyo, Tokyo, Japan

32 <sup>19</sup>Department of Geological Science, University of Missouri, Columbia, USA

33 <sup>20</sup>Research and Development Center for Earthquake and Tsunami, Japan Agency for Marine - Earth  
34 Science and Technology, Yokosuka, Japan

35

36 \*Corresponding author:

37 Address: Graduate School of Engineering, Kyoto University, C1-1-109

38 C-cluster, Kyoto Daigaku Katsura, Nishikyo-ku, Kyoto 615-8540, Japan.

39 E-mail: lin@kumst.kyoto-u.ac.jp Fax: +81 75 383 3203

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43 **Abstract:** To better understand the distribution of three dimensional stress states in the

44 Nankai subduction zone, southwest Japan, we review various stress-related

45 investigations carried out in the first and second stage expeditions of the Nankai Trough

46 Seismogenic Zone Experiment (NanTroSEIZE) by the Integrated Ocean Drilling Program

47 (IODP) and compile the stress data. Overall, the maximum principal stress  $\sigma_1$  in the

48 shallower levels ( $<\sim 1\text{km}$ ) is vertical from near the center of forearc basin to near the

49 trench and; the maximum horizontal stress  $S_{H\text{max}}$  (interpreted to be the intermediate

50 principal stress  $\sigma_2$ ) is generally parallel to the plate convergence vector. The exception to

51 this generalization occurs along the shelf edge of the Nankai margin where  $S_{H\text{max}}$  is along

52 strike rather than parallel to the plate convergence vector. Reorientation of the principal

53 stresses at deeper levels (e.g.,  $>\sim 1\text{km}$  below seafloor or in underlying accretionary

54 prism) with  $\sigma_1$  becoming horizontal is also suggested at all deeper drilling sites. We also

55 make a comparison of the stress state in the hanging wall of the frontal plate-interface  
56 between Site C0006 in the Nankai and Site C0019 in the Japan Trench subduction zone  
57 drilled after the 2011 Mw9.0 Tohoku-Oki earthquake. In the Japan Trench, the  
58 comparison between stress state before and after the 2011 mega-earthquake shows that  
59 the stress changed from compression before the earthquake to extension after the  
60 earthquake. As a result of the comparison between the Nankai Trough and Japan Trench,  
61 a similar current stress state with trench parallel extension was recognized at both  
62 C0006 and C0019 sites. Hypothetically, this may indicate that in Nankai Trough it is still  
63 in an early stage of the interseismic cycle of a great earthquake which occurs on the  
64 décollement and propagates to the toe (around site C0006).

65

## 66 **1. Introduction**

67 Stress and earthquakes are known to be interrelated: stress triggers earthquakes and  
68 earthquakes alter the shear and normal stresses on surrounding faults (Stein, 1999;  
69 Seeber and Armbruster, 2000; Hardebeck, 2004; Ma et al., 2005; Lin et al., 2007). On the  
70 other hand, the stresses both on the fault and in the formation gradually build up in the  
71 interseismic period (Kanamori and Brodsky, 2001). The Nankai Trough Seismogenic  
72 Zone Experiment (NanTroSEIZE), a comprehensive scientific drilling project conducted

73 by the Integrated Ocean Drilling Program (IODP) in the Nankai subduction zone,  
74 southwest Japan, is designed to investigate the mechanics of the subduction megathrust  
75 through drilling and a wide range of allied studies (Tobin and Kinoshita, 2006; Tobin et  
76 al., 2009a). In this area, Mw 8.0 class great earthquakes repeat at intervals of 100–200  
77 years as a result of the convergence of the Philippine Sea and Eurasian plates (Ando,  
78 1975; Fig. 1). The last two great earthquakes in the Nankai subduction zone occurred in  
79 1944 (Tonankai, M 8.0-8.3) and 1946 (Nankai, M 8.1-8.4), generating tsunamis and  
80 causing significant damage in southwest Japan (Kanamori 1972). The NanTroSEIZE  
81 project sampled and continues to monitor the characteristics of the seismogenic zone  
82 during the interseismic interval. In contrast, IODP expedition 343 to the Japan Trench  
83 (also referred to as the Japan Trench Fast Drilling Project or JFAST), was conducted just  
84 after a great earthquake, about 13 months after the 2011 Mw 9.0 Tohoku-Oki, Japan  
85 earthquake (Mori et al., 2012; Chester et al., 2012; Fig. 1).

86 Establishing the in situ stress state along active subduction zones is critical for  
87 understanding the accumulation and release of most of Earth's seismic energy  
88 (Lallemand and Funiciello, 2009). Determination of in situ stress is one of the most  
89 important scientific objectives of both NanTroSEIZE and JFAST, and also one of the  
90 major goals of the IODP as the seismogenic parts of plate margins are often only

91 accessible through drilling. First, we review various stress-related investigations carried  
92 out in association with NanTroSEIZE stages 1 and 2. We then compare the present-day  
93 stress states in the frontal part of the plate-interface at the Nankai and Japan Trench  
94 subduction zones and propose hypotheses on the temporal and spatial evolution of  
95 stresses in the frontal plate-interface in Nankai, SW Japan.

96

## 97 **2. Stress estimates and direct measurements from stage 1 and 2 of the** 98 **NanTroSEIZE drilling project**

99 The multi-stage scientific drilling project NanTroSEIZE, conducted by the drilling vessel  
100 D/V *Chikyu*, began in 2007 with IODP expedition 314 and is continuing with planned  
101 deep riser drilling in the coming years (Kinoshita et al., 2008; Hirose et al., 2013). To  
102 date more than 10 drilling sites have been drilled along the NanTroSEIZE transect with  
103 at least one vertical borehole(s) at each site. This transect is approximately orthogonal  
104 to the Nankai Trough axis (plate boundary) (Fig. 2, 3 and 4a and Table 1).

105 In the first stage of NanTroSEIZE (2007–2008), borehole wall images obtained by  
106 logging while drilling (LWD) technology yielded regional patterns of stress orientations  
107 and magnitudes through observations of drilling-induced compressive failures  
108 (borehole breakouts) and tensile fractures (DITFs) (e.g., Tobin et al., 2009b; Chang et al,

109 2010; Lin et al., 2010a; Moore et al., 2011; Lee et al., 2013). This stage involved five  
110 drilling sites in three structural settings in which LWD was performed: the frontal thrust  
111 at the toe of the accretionary prism, Site C0006; the megasplay hanging wall and  
112 footwall, Sites C0010, C0004 and C0001, and the seaward edge of the Kumano forearc  
113 basin, Site C0002 (Fig. 2, 3 and 4a). These regional studies were followed by more  
114 detailed core-based analyses and geophysical studies, including interpretation of  
115 high-resolution seismic reflection data and S-wave splitting that provided a  
116 three-dimensional understanding of the stress field and the evolution of stresses  
117 through time (Byrne et al., 2009; Kimura et al., 2011; Tsuji et al., 2011a; Lewis et al.,  
118 2013; Moore et al., 2013; Sacks et al., 2013; Conin et al., 2014). Taken together, these  
119 results show that at all sites except C0004 and C0010, the maximum principal stress  $\sigma_1$   
120 is vertical at shallow levels and that the orientation of the intermediate principal  
121 stress  $\sigma_2$  changes from trench perpendicular at C0006 and C0001 to trench parallel at  
122 C0002. At sites C0004 and C0010  $\sigma_1$  is interpreted possibly to be horizontal and  
123 approximately parallel to the plate convergent direction.

124 In the second stage of NanTroSEIZE (2009-2010), D/V *Chikyu* carried out the first  
125 riser drilling in IODP history at Site C0009 of Expedition 319. This expedition targeted  
126 the hanging wall above the high slip region of the 1944 Tonankai earthquake (Saffer *et*

127 *al.*, 2009). The borehole penetrated the Kumano forearc basin sediments and the  
128 underlying accretionary prism; and was the deepest drilling (~1.6 km) during the first  
129 and second stages of NanTroSEIZE. In a depth range from approximately 700 mbsf  
130 (meters below seafloor) to the target depth of 1600 mbsf, wireline logging included a  
131 borehole caliper and a fullbore formation microimager (FMI) that provided resistivity  
132 images. From the borehole images and caliper data, borehole breakouts and DITFs were  
133 identified and the horizontal stress orientations were obtained (Saffer et al., 2009; Lin et  
134 al., 2010a; Wu et al., 2012). Due to limited azimuthal coverage (~50%) of the wellbore  
135 walls by FMI, the width of breakouts was not well constrained, and therefore no reliable  
136 information about stress magnitudes could be extracted from the wellbore failures.

137       The first hydraulic fracturing experiments in the scientific ocean drilling history  
138 also were carried out using two techniques at Site C0009. The first, an “extended leak-off  
139 test”, was conducted as part of drilling operations and provided a measurement of  
140 minimum principal stress magnitude at ~708 mbsf (Saffer et al., 2013; Lin et al., 2008).  
141 The second technique, a “two dual-packer hydraulic fracture test” was conducted using  
142 Modular Dynamic Tester (MDT) tool (Ito et al., 2013; Saffer et al., 2013; Haimson and  
143 Cornet, 2003), and yielded two additional measurements of in situ minimum principal  
144 stress magnitude: one at ~877 mbsf and a less reliable determination at ~1534 mbsf.

145 Drill core samples were also recovered in a ~80m depth interval in mudstones  
146 interpreted as either the uppermost accretionary prism or a paleo-slope basin. Anelastic  
147 strain recovery (ASR) measurements on core samples were used to determine the  
148 three-dimensional stress orientations by the same method as Byrne et al. (2009) (Lin et  
149 al., 2010b). In addition, results of a “walkaround” vertical seismic profiling (VSP)  
150 experiment recorded at Site C0009 and conducted by D/V *Chikyu* and R/V *Kairei* showed  
151 a clear anisotropy in P wave velocity and amplitude, and documented S wave splitting.  
152 These data have also been interpreted as indicators of horizontal stress orientations  
153 (Tsuji et al., 2011b).

154 During IODP expeditions 322 in stage 2, two reference sites were drilled on the  
155 incoming Philippine Sea Plate: Site C0012, located ~31 km seaward of the trench on  
156 basement high to sample a condensed sedimentary section, and Site C0011, ~22 km  
157 seaward of the trench designed to sample the section at a basement low. LWD resistivity  
158 images documented borehole breakouts and provide an indication of horizontal  
159 principal stress orientations at Site C0011 (Expedition 322 Scientists, 2010; Wu et al.,  
160 2013). Site C0012 was not drilled with LWD; however, ASR measurements on core  
161 samples yielded constraints on stress states in both the oceanic crust (basalt) and the  
162 sedimentary cover (Yamamoto et al., 2013).

163

### 164 **3. Results of Stage 1 drilling, Nankai subduction zone, SW Japan**

#### 165 *3.1. C0001*

166 Borehole breakouts, tensile fractures and core-scale faults are present in the upper half  
167 of the boreholes at Site C0001 and provide constraints on the orientation, ratios and  
168 magnitudes of the principal stresses (Expedition 314 Scientists, 2009a). The maximum  
169 horizontal stress  $S_{Hmax}$  orientation determined from borehole breakouts and tensile  
170 fractures consistently trend  $\sim 335^\circ$  throughout the hole, although Chang et al. (2010)  
171 proposed that the stress regime changes with depth, likely due to increasing  $S_{Hmax}$  (Fig.  
172 2). At shallow levels ( $< \sim 500$  mbsf)  $S_{Hmax}$  is interpreted to be  $\sigma_2$  and smaller in  
173 magnitude than the vertical stress, reflecting a normal faulting regime. Consolidation  
174 and triaxial compression tests of slope sediments in the uppermost  $\sim 200$  mbsf also  
175 suggest horizontal effective stresses are  $\sim 41\%$  of the vertical effective stress consistent  
176 with a normal faulting regime (Song et al., 2011). Stress inversion of core-scale faults  
177 from C0001 provide a measure of the three-dimensional stress state at relatively  
178 shallow levels and also show normal faulting with extension parallel to the margin  
179 (Lewis et al., 2013). These results are consistent with faulting patterns observed in  
180 seismic reflection data as well as with the borehole breakout data that show  $\sigma_2$

181 subparallel to the plate convergence vector. Lewis et al. (2013) also recognized an older  
182 suite of faults that, when inverted for stress orientations, show  $\sigma_1$  trending northwest,  
183 parallel to the plate convergence vector. Chang et al. (2010) interpret  $S_{Hmax}$  at deeper  
184 levels ( $>\sim 500$  mbsf) to be  $\sigma_1$ , reflecting a change with depth from normal faulting to  
185 strike-slip, or possibly thrusting. Unfortunately, sediment cores were not retrieved from  
186 deeper levels where the principal stresses appear to permute.

### 187 3.2. C0002

188 Site C0002, which penetrated the Kumano forearc basin and the upper part of the  
189 underlying accretionary prism, also shows a consistent orientation of borehole  
190 breakouts with depth and a possible permutation of stresses with depth.  $S_{Hmax}$   
191 determined from breakouts, however, trend northeast, approximately perpendicular to  
192  $S_{Hmax}$  at C0001, which is only 10 km to the southeast (Fig. 2 and 3). Analysis of the  
193 breakouts, results from ASR experiments and inversion of core-scale faults show a  
194 normal faulting regime in the forearc sequence with the minimum principal stress  $\sigma_3$   
195 nearly parallel to the plate convergence vector and perpendicular to the shelf break.  
196 These results are consistent with numerous margin parallel normal faults observed in  
197 seismic reflection data (Gulick et al., 2010; Moore et al., 2013; Sacks et al., 2013). Many  
198 of the faults also cut the seafloor, suggesting that they are active or recently active, and

199 the lack of growth data suggests that the transition to an extension dominated basin  
200 occurred less than  $\sim 1$  Ma ago (Gulick et al, 2010). Sacks et al. (2013) and Moore et al.  
201 (2013) also show that there is a systematic change from any an early phase of generally  
202 trench-parallel extension that started before 0.44 Ma to trench-normal extension  
203 associated with faults that often cut the seafloor. These results are consistent with  
204 observations of core-scale fault populations that show a change from NE-SW extension  
205 to NW-SE extension (Expedition 315 Scientists, 2009). Chang et al. (2010) propose that  
206 the stress regime changes below the forearc sediments with  $S_{Hmax}$  becoming  $\sigma_1$ ,  
207 suggesting a change from normal faulting to strike-slip or thrusting similar to the change  
208 proposed for Site C0001. The stress states at the two sites, however, are still  
209 fundamentally different as the borehole breakouts, and therefore  $S_{Hmax}$ , are  
210 perpendicular even at the deepest structural levels. In fact, the trend of  $S_{Hmax}$ , which is  
211 interpreted to be  $\sigma_1$  in the deeper levels of C0002, suggests margin-parallel shortening  
212 rather than margin perpendicular shortening as interpreted for the deeper levels of  
213 C0001 (Fig. 2).

### 214 3.3. C0004

215 Site C0004 penetrated the megasplay fault, which appears to have slipped coseismically  
216 during the 1944 earthquake (Sakaguchi et al., 20011b) and borehole breakouts show

217 consistent trends throughout the hole with  $S_{Hmax}$  trending northwest-southeast,  
218 approximately parallel to  $S_{Hmax}$  at C0001 (Expedition 314 Scientists, 2009b; Fig. 2). Site  
219 C0004 is only a few kms from C0001 and Byrne et al. (2009) assumed a relatively  
220 homogeneous stress field and proposed that  $S_{Hmax}$  at this site represented  $\sigma_2$  rather than  
221  $\sigma_1$ . More recent analyses of borehole breakouts, however, by Olcott and Saffer (2012)  
222 and Yamada and Shibanuma (2015) suggest that  $S_{Hmax}$  at this site possibly represents  $\sigma_1$   
223 consistent with a reverse or strike-slip faulting regime. They described that the  
224 magnitude of the vertical stress  $S_v$  may be smaller than that of  $S_{Hmax}$  but within the  
225 possible range of  $S_{hmin}$  (see Fig. 4 in Yamada and Shibanuma, 2015).

#### 226 *3.4. C0006*

227 Site C0006 penetrated and sampled the hanging wall of the frontal thrust and borehole  
228 breakouts, anelastic strain and core-scale faults provide a more complete picture of the  
229 stress state than at C0004. Borehole breakouts occur throughout most of the hole  
230 although they appear much more weakly developed than at the other three sites. The  
231 breakouts trend  $060^\circ$  consistent with results from Sites C0001 and C004, indicating that  
232  $S_{Hmax}$  trends about  $330^\circ$ , approximately parallel to the plate convergence vector  
233 (Expedition 314 Scientists, 2009c). ASR on a core sample from the hanging wall and  
234 inversion of the youngest suite of core-scale faults show a steeply plunging  $\sigma_1$  with  $\sigma_3$

235 trending northeast, indicating normal faulting and margin-parallel extension, similar to  
236 Site C0001 at shallow depths (Fig. 6b). Interpretations of the stress field around Site  
237 C0006 using a slip deficit model also indicate a normal faulting regime (Fig. 6a; Wu et al.,  
238 2013), and conjointly a significant erosion at the top of the slope sediments can be  
239 observed (Strasser et al, 2011; Conin et al, 2011). Anisotropy of magnetic susceptibility  
240 data (Byrne et al., 2009; Kitamura et al., 2010) and suites of core-scale structures that  
241 pre-date the normal faults show an earlier phase of margin-perpendicular shortening,  
242 which is also similar to the observations from Site C0001 (Lewis et al. 2013).

### 243 *3.5. C0007*

244 Site C0007, located less than a kilometer seaward of Site C0006 and a few hundred  
245 meters from the deformation front, was drilled after coring at Site C0006 failed to reach  
246 the frontal thrust (Fig. 3). Although the holes drilled at Site C0007 were not logged, so  
247 borehole images are not available, observations of cores indicate a deformation history  
248 similar to the history documented at Site C0006; that is, early northwest-southeast  
249 shortening followed by normal faulting. In addition, vitrinite reflectance measurements  
250 of samples from the frontal thrust show anomalously high temperatures, suggesting that  
251 the fault moved co-seismically (Sakaguchi et al., 2011a). Sites C0006 and C0007 together  
252 therefore may represent an analogous setting to Site C0019 in the Tohoku area which

253 also sampled the front thrust after it slipped co-seismically.

254

## 255 **4. Results from Stage 2, Nankai subduction zone, SW Japan**

### 256 *4.1. C0009*

257 At Site C0009, direct measurements of  $\sigma_3$  via hydraulic fracturing tests and leak-off test  
258 (LOT) indicate that the stress regime changes from a normal faulting stress regime in the  
259 Kumano basin sediments to a possible strike-slip or thrusting stress regime in the  
260 underlying slope basin or accretionary wedge, to a depth of at least ~1600 mbsf similar  
261 to the change at Site C0001 (Fig. 2; Lin et al., 2010b; Ito et al., 2013; Saffer et al., 2013;  
262 Wu et al., 2013). Estimates of stress magnitude from the width of borehole breakouts at  
263 Site C0002 suggested a similar pattern, i.e. changing from a normal faulting stress  
264 regime in the basin sediments to a strike slip or thrust faulting regime in the underlying  
265 accretionary prism to the depth of ~1380 mbsf (the lower limit of breakout occurrence  
266 in borehole C0002A) (Tobin et al., 2009a; Byrne et al., 2009; Chang et al., 2010; Lee et al.,  
267 2013).

### 268 *4.2. C0010*

269 Site C0010 is located a few km along strike from Site C0004 and, similar to C0004,  
270 penetrated the hanging wall and footwall of the megasplay, one of primary drilling

271 targets of the NanTroSEIZE. Shipboard analysis of the borehole breakouts showed a  
272 consistent pattern above the megasplay with the maximum horizontal stress trending  
273 NW-SE. McNeill et al. (2010) noted that the megasplay corresponds to a seismic reflector  
274 with negative polar, suggesting a reduction in velocity and/or density in the footwall.  
275 They also recognized an abrupt change in orientation of the breakouts across the  
276 megasplay and proposed that the fault zone represented a sharp mechanical  
277 discontinuity. Although Olcott and Saffer (2012) proposed that  $\sigma_1$  remained horizontal  
278 beneath in the footwall similar to the results from C0004, they also documented a shift  
279 to lower stress magnitudes in the footwall, based on the widths of borehole breakouts.

#### 280 *4.3. C0011 and C0012*

281 At Site C0011, the orientation of  $S_{Hmax}$  was determined by borehole breakouts observed  
282 in a narrow depth interval (~600 – 650 mbsf, Expedition 322 Scientists, 2010) and is  
283 oblique to the plate convergence vector. Although estimates of stress magnitude are  
284 strongly dependent on assumed rock strength parameters, a normal faulting stress  
285 regime was suggested on the basis of wellbore breakout widths at ~610 mbsf (Wu et al.,  
286 2013).

287           At Site C0012, which is the most seaward input site and occurs on the crest of a  
288 prominent basement high (Kashinosaki Knoll), ASR results suggest a normal faulting

289 regime in the sedimentary sequence, with  $S_{Hmax}$  oriented WNW-ESE (Yamamoto et al.,  
290 2013). In contrast, ASR analysis of a core sample of oceanic basement basalt shows a  
291 strike slip or a reverse faulting stress regime, with the maximum horizontal stress  
292 orientated northeast – southwest approximately parallel to the trough axis. The  
293 basement stress orientation could be the result of hinge extension during bending of the  
294 Philippine Sea plate, either in association with subduction or with the formation of an  
295 anticline during intraoceanic thrusting (Yamamoto et al., 2013).

296

## 297 **5. Discussion: Nankai Margin**

298 Although the drilling depths in stages 1 and 2 are relatively shallow (<~1.6 km at Site  
299 C0009), the results suggest important trends in both depth and map view. For example,  
300 observations at many of the sites suggest a change from a normal faulting regime at  
301 shallow structural levels to strike-slip or thrusting at deeper levels. These results  
302 suggest that gradients in topography may play an important role in defining the state of  
303 stress. Deeper drilling, like the programs completed as part of Expedition 348 which  
304 penetrated to ~3 kmbsf at Site C0002 and the future NanTroSEIZE expeditions planned  
305 to drill to > 5 kmbsf in the same borehole will better define change in stress states with

306 depth and provide a clearer understanding of how stress changes temporally and  
307 spatially in the prism.

308         The above review suggests two general patterns for the states of stress at  
309 relatively shallow levels: First,  $\sigma_1$  appears to be vertical at all sites except in the hanging  
310 wall of the megasplay at Sites C0004 and C0010 where  $\sigma_1$  is interpreted to be  
311 sub-horizontal and parallel to the plate convergence vector. Second, the maximum  
312 horizontal stresses  $S_{Hmax}$  appear to be parallel to the plate convergence vector except  
313 near the seaward edge of the Kumano Basin at Site C0002 where  $\sigma_3$  is parallel to the  
314 plate convergence vector.

315         A possible explanation for the reorientation of  $\sigma_1$  at C0004 and C0010 may be  
316 that the sediments being carried in the hanging wall are relatively strong and capable of  
317 supporting plate tectonic stresses. The occurrence of an extensional regime at higher  
318 structural levels where slope sediments are dominant (e.g., Site C0001) and the  
319 identification of a relatively weak footwall (Olcott and Saffer, 2012; McNeill et al, 2010)  
320 are consistent with this interpretation. We therefore propose that the hanging wall of the  
321 megasplay is relatively strong and supports a compressional stress state that is  
322 consistent with plate convergence. In contrast, the transmission of the stresses  
323 associated with plate convergence appears to be less effective in the slope sequence

324 where  $\sigma_2$  is observed to be parallel to the plate convergence vector and in the footwall  
325 where stress magnitudes decrease and possibly reorient. Drilling and sampling of  
326 core-scale faults across the décollement at Site 808 during the Ocean Drilling Program  
327 (ODP) Leg 131 along the Muroto transect also documented a reorientation of stresses  
328 (Lallemant et al., 1993). At this site  $\sigma_1$  is sub-horizontal and NW-trending above the  
329 décollement, similar to the results from C0004 and C0010, and but sub-vertical below  
330 the décollement (Lallemant et al., 1993). One possibility is that the stresses below the  
331 megasplay have also been reoriented and  $\sigma_1$  is vertical (Fig. 3) or they record a transition  
332 in stress states.

333         At C0002 the reorientation of  $\sigma_3$  relative to the regional pattern may reflect  
334 gravitation collapse of the prism as the décollement weakens either continuously or  
335 during large earthquakes as suggested for the Tohoku region (McKenzie and Jackson,  
336 2012; Kimura et al., 2012; Tsuji et al., 2013). A seismic reflection profile running NW–SE  
337 and including Site C0002 displays a clear sequence of trough-parallel normal faults in  
338 the basin sediments consistent with the maximum horizontal stress orientation data (e.g.  
339 Tobin et al., 2009a). Sacks et al. (2013) (and see also Moore et al., 2013) analyzed this  
340 regional-scale fault system in more detail and recognized two patterns of extension – an  
341 early phase of generally northeast-southwest, or margin-parallel, extension and a later

342 phase of trench-perpendicular extension that is concentrated on the seaward edge of the  
343 basin. The fact that trench-perpendicular extension appears to be limited to the area of  
344 the shelf edge, which is both relatively far from the plate interface and at the topographic  
345 crest, is consistent with the hypothesis that gradients in topography (including effects of  
346 the “notch” proposed by Martin et al., 2010) are important in defining the state of stress  
347 along the margin. Theoretical studies as well as analog and numerical models also  
348 suggest that variations in the strength of the décollement below the wedge can lead to  
349 extension in the overlying accretionary wedge. For example, Haq and Davis (2008) show  
350 that for wedges with a ductile base, accretion can lead to over steepened topography and  
351 flow at lower structural levels, which drive trench-perpendicular extension (i.e., normal  
352 faulting) at higher structural levels. In fact, several authors have proposed that a regional  
353 low-velocity zone beneath the Nankai margin represents weak, and probably  
354 overpressured sediments (Park et al., 2010; Byrne et al. 2009; Bangs et al., 2009; Kamei  
355 et al., 2012; Kitajima & Saffer, 2012) that may act like the ductile lower crust in the  
356 analog models.

357 The above hypothesis for the pattern of regional-scale stresses, however, fails to  
358 consider the possible change in stresses associated with the earthquake cycle. For  
359 example, this region of the Nankai margin experienced a major earthquake and tsunami

360 in 1944; and Sakaguchi et al. (2011a), based on maturation studies of vitrinite collected  
361 from fault zones sampled at Sites C0004 and C0007, proposed that megasplay and  
362 décollement slipped during the earthquake(s). Presumably, for some period before, and  
363 up to the beginning of the earthquake the state of stress in the hanging wall would have  
364 been compressional with  $\sigma_1$  orientated sub-parallel to the plate convergence vector. The  
365 evidence from all of the sites along the Kumano transect where the principal stress  
366 orientations can be determined, however, shows a normal faulting regime, at least at  
367 shallow structural levels and excluding Sites C0004 and C0010 which sampled the  
368 hanging wall of the megasplay. These data also show that the rocks failed exclusively by  
369 normal faulting; that is, there is no evidence in the cores or seismic reflection data for  
370 alternating periods of extension and compression that could be interpreted as stress  
371 permutations associated with an earthquake cycle. For example, observation from Site  
372 C0002 and detailed studies of the deformation history in the Kumano Basin (Lewis et al.,  
373 2013 and Sacks et al., 2013, respectively) show an early phase of trench-parallel  
374 extension followed by a phase of trench-perpendicular extension. Neither data set shows  
375 stress permutations where the principal stresses switch multiple times, for example over  
376 several earthquake cycles. At least two explanations are possible, either: 1) all of the late  
377 stage normal faults formed after the last earthquake (e.g., after 1944) due to stress

378 relaxation and stress permutations or 2) the stress states vary during the seismic cycle  
379 (e.g.,  $\sigma_1$  alternates between horizontal and vertical from one cycle to the next) (Wang and  
380 Hu, 2006; Conin et al., 2012; Kinoshita and Tobin, 2013; Sacks et al., 2013; Hashimoto et  
381 al., 2014), but during an earthquake, failure is accommodated only or primarily by slip  
382 on major thrust faults and not on core-scale faults. After a major earthquake, the  
383 associated stress drop and relaxation leads to decrease in  $S_{Hmax}$ , such that the vertical  
384 stress  $S_v$  becomes  $\sigma_1$ , depending on the local stress field. Hsu et al. (2009) recently  
385 proposed an interpretation similar to the second alternative (#2 above) for stress  
386 permutations before and after the 1999 Chichi earthquake in Taiwan.

387

## 388 **6. Stress states at the Japan Trench**

### 389 *6.1. IODP drilling Site C0019 and ODP Sites 1150 and 1151*

390 The Japan Trench lies along the eastern edge of Japan and marks the boundary where  
391 the Pacific plate subducts beneath the Okhotsk plate (or North American plate) at  $\sim 8$   
392 cm/year (Loveless and Meade, 2010) (Fig. 1). The Tohoku-Oki earthquake (Mw 9.0)  
393 occurred on March 11, 2011 and was followed by a huge tsunami (Simons et al., 2011;  
394 Ide et al., 2011) that flooded many coastal regions of northeast Japan, taking over 18,000  
395 lives. Planning for IODP Expedition 343 (informally called the “Japan Trench Fast Drilling

396 Project” or JFAST) began soon after the earthquake with the primary goal of better  
397 understanding the stress and slip history along the fault. To this end, the goals of the  
398 expedition were to: 1) test the possibility that coseismic slip on a major fault generated  
399 frictional heat; 2) to investigate stress state on the fault and 3) retrieve samples from the  
400 proposed fault zone. To achieve these goals IODP expedition 343 conducted a rapid  
401 response drilling program about 13 months after the earthquake. The expedition  
402 successfully penetrated and sampled the frontal fault at a depth of ~820 mbsf at IODP  
403 Site C0019 where coseismic displacements were relatively large (~50 m) (Mori et al.,  
404 2012; Chester et al., 2012). Site C0019 is located ~93 km seaward from the epicenter of  
405 the mainshock of the Tohoku-Oki earthquake and ~6 km landward of the trench axis (Fig.  
406 4b and 5).

407 In addition to the JFAST site, Sites 1150 and 1151, also located near the source  
408 area of the Tohoku-Oki earthquake, were drilled during ODP Leg 186 in 1999 prior to the  
409 earthquake (Lin et al., 2011) (Fig. 4b). Lin et al. (2011) integrated FMS images with  
410 caliper data to interpret the orientation of  $S_{Hmax}$  at the two sites.

#### 411 *6.2. Results from C0019*

412 Lin et al. (2013) analyzed LWD data collected by JFAST at Site C0019 (Fig. 4b)  
413 and integrated these data with compressive strength and core-based observations to

414 determine the stress state and to infer stress history at this site. Although borehole  
415 breakouts are present throughout the hanging wall of the plate boundary, they show  
416 a wide range in orientations at shallow structural levels (<500 mbsf), suggesting that  
417  $S_{Hmax}$  and  $S_{Hmin}$  are close in magnitude, and/or that  $S_{Hmax}$  orientation is highly variable  
418 with depth. At deeper levels (>500 mbsf)  $S_{Hmax}$  shows a clear trend to the northwest  
419 ( $319 \pm 23^\circ$ ), which is sub parallel to the plate convergence vector of  $292^\circ$  at this location  
420 (Fig.4b; Argus et al., 2011). Lin et al. (2013) also used the width of the borehole  
421 breakouts and the results of initial shipboard experiments on the unconfined  
422 compressive strength (UCS) of sediments from two depth intervals to determine the  
423 stress magnitudes. Their results show that the frontal part of the prism above the plate  
424 boundary fault is in, or close to, a normal faulting regime (Fig. 6c). These results contrast  
425 with core-scale observations, however, that show dominantly thrusting and horizontal  
426 shortening with only limited evidence of extension at relatively shallow structural levels.  
427 Based on these results, the authors suggested a distinct coseismic stress change from a  
428 reverse faulting stress regime before the earthquake to a normal faulting stress regime  
429 after the earthquake (Fig. 7). This interpretation is well-consistent with Hasegawa et al.  
430 (2012).

431 *6.3. Results from ODP Sites 1150 and 1151*

432 FMS and caliper data from Sites 1150 and 1151 were used to define the orientation of  
433  $S_{Hmax}$  at these two sites, which were drilled prior to the Tohoku-Oki earthquake. The FMS  
434 images showed the development of drilling induced tensile fractures (DITF) and  
435 borehole breakouts at deeper structural levels (e.g., > 700mbsf) and the caliper data  
436 provide a general constraint on the orientation of borehole breakouts. Although there is  
437 variability between the two sites, the combined data set shows  $S_{Hmax}$  trending northwest,  
438 generally parallel to the plate convergence vector (Lin et al., 2011) (Fig. 4b). Based on  
439 the presence of DITFs at both sites and significant seismic activity associated with  
440 northwest-southeast directed shortening, Lin et al. (2011) concluded that the hanging of  
441 the plate boundary in this area possibly was in a thrusting regime before the 2011  
442 earthquake.

443

## 444 **7. Comparison between Nankai and Japan Trench**

445 The general comparison of the Nankai and Tohoku margins presented above shows that  
446 the margins share important similarities as well as at least one critical difference (Fig. 5).  
447 First, available data suggest that both margins are dominated by an extensional stress  
448 regime with a vertically oriented maximum principal stress. Extension along the Tohoku  
449 area is show by the dominance of normal faulting aftershocks in the hanging wall above

450 the décollement (Tsuji et al., 2013) as well as the in situ stress data from Site C0019.  
451 Extension along Nankai is documented by seismic reflection data along the shelf edge  
452 and observations from 3 drill sites that span the accretionary prism. Horizontal  
453 compression may occur at deeper levels and in the hanging wall of the megasplay, but  
454 normal faulting appears to be the dominant pattern. The second similarity is that both  
455 margins can be divided into inner and outer wedges separated by a regionally significant  
456 normal fault or a complex system of normal and oblique slip faults. At Tohoku, a  
457 landward dipping normal fault with significant offset separates a deep-sea terrace from  
458 the upper, middle and low slope that define the accretionary wedge. At Nankai, the  
459 seaward edge of the forearc basin is marked by relatively intricate set of normal faults  
460 associated with a graben-like structure that marks shelf edge. Some of the normal faults  
461 may also have oblique slip that accommodate strike-parallel motion related to  
462 moderately oblique plate convergence (Martin et al., 2010). Finally, one critical  
463 difference appears to be the presence of a megasplay in the accretionary prism of the  
464 Nankai margin and the apparent absence of similar structures along the Tohoku margin.

465 Interestingly, the similarities of the two margins are also the primary  
466 characteristics of margins that typically produce tsunami earthquakes (Tsuji et al., 2013;  
467 McKenzie and Jackson, 2012). For example, recent theoretical studies (McKenzie and

468 Jackson, 2012) as well as recent observations from Tohoku (Tsuji et al., 2013) suggest  
469 tsunami genic earthquakes result from the simultaneous slip along the décollement and  
470 a landward-dipping normal fault or a suite of normal faults that separate the inner and  
471 outer wedges. McKenzie and Jackson (2012) also propose that displacements on these  
472 regional-scale faults and the seaward motion of the outer wedge is driven by the release  
473 of gravitational potential energy as well as elastic strain. Although McKenzie and Jackson  
474 (2012) do not address what processes cause the décollement and the normal fault to fail  
475 simultaneously, Kimura et al. (2012) suggest that progressive dewatering of underthrust  
476 sediments along the Tohoku margin lead to failure and “runaway” slip along the  
477 décollement probably weakened by over pore pressure (e.g. Tobin and Saffer, 2009;  
478 Kitajima et al., 2012; Hashimoto et al., 2013; Tsuji et al., 2014). Tsuji et al. (2013), based  
479 on sea floor observations of extension cracks and heat flow anomalies, also propose that  
480 normal faulting in the hanging wall occurred simultaneously with slip on the  
481 décollement. Along the Nankai margin, the décollement is also interpreted to be  
482 anomalously weak and the seaward edge of the Kumano Basin is deformed exclusively  
483 by normal faults, suggesting a tectonic setting similar to Tohoku. One possibility,  
484 therefore, is that during a historic great earthquake, which also produced a tsunami

485 along southwest Japan, slip occurred simultaneously on normal faults in the hanging  
486 wall and along the décollement.

487         A complication to this interpretation is that models of the 1944 tsunami suggest  
488 that a significant amount of the coseismic slip occurred on the megasplay rather than the  
489 décollement (Tanioka and Satake, 2001; Cummins et al., 2002). However, Sakaguchi et al.  
490 (2011a), based on observations from Site C0007 which is near the toe of the prism, show  
491 that the décollement also moved co-seismically, although the timing of co-seismic slip is  
492 unknown. If the model proposed for Tohoku (McKenzie and Jackson, 2012) also applies  
493 to the 1944 event along the Kumano transect, then movement along both the megasplay  
494 and the décollement must have driven forward motion of the accretionary wedge.

495         We therefore propose that the two margins represent similar states between  
496 tsunami earthquakes, although there are differences. Following this interpretation, the  
497 stress state of the accretionary wedge, including the frontal plate interface builds up  
498 from a normal faulting stress regime just after a large earthquake to a reverse faulting  
499 regime before the next earthquake. In other words, the tectonic horizontal stress caused  
500 by plate convergence gradually builds up during the interseismic period and dynamically  
501 drops during an earthquake consistent with the conventional stress accumulation  
502 fundamental model (e.g. see Kanamori and Brodsky, 2001). Following this interpretation,

503 both Sites C0006 (Nankai) and Site C0019 (Tohoku) appear to be in the early stages of  
504 the interseismic cycle with  $\sigma_1$  is vertical and that  $S_{Hmax}$  (interpreted to be  $\sigma_2$ ) is generally  
505 parallel to the plate convergence vector (Fig. 6). In Nankai margin, more than 60 years  
506 have passed from the previous M8-class earthquake propagated through the megasplay  
507 fault to the time of drilling at C0006 (2007), but the time length from the previous great  
508 earthquake occurred on the décollement and propagated to C0006 is unknown.  
509 Hypothetically, the stress state may indicate that in Nankai margin, it is still in an early  
510 stage of the interseismic cycle of a great earthquake which occurs on the décollement  
511 and propagates to the toe, even cuts the seafloor.

512

513

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852 **Table and Figures' captions**

853

854 Table 1 Specifications of the stress measurement related boreholes in NanTroSEIZE and  
855 JFAST drilling sites. For example, C0002 denotes the drilling site; whereas C0002A is  
856 the name of the borehole “A” located at Site C0002. Usually, multi boreholes were  
857 drilled for different operations within a narrow area (e.g. a few tens meters) in a site in  
858 IODP.

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860 Fig. 1 (1.5-column fitting) Nankai and Japan Trench subduction zones and plates around  
861 Japan islands. Red stars and numbers show the epicenters of the earthquakes and  
862 its occurrence year; the red frames are the area of rupture zones during the  
863 earthquakes. White arrows and numbers show directions and rates of plate motion,  
864 respectively (Sella et al., 2002; Apel et al., 2006; Loveless and Meade, 2010; Ozawa  
865 et al., 2011).

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867 Fig. 2 (2-column fitting) Distributions of semi three-dimensional stress state in  
868 NanTroSEIZE transect. Codes (e.g. C0009) are the number of drilling sites. Red,  
869 black and light blue arrows are the orientations of the maximum, intermediate and  
870 minimum principal stresses, respectively. Two pair arrows in the same light blue  
871 color in the deeper part of C0009, C0002 and C0012 mean that the intermediate  
872 and minimum principal stresses are nearly equal each other, or the intermediate  
873 and minimum principal stresses are highly variable.

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875 Fig. 3 (2-column fitting) Seismic reflection section of NanTroSEIZE transect (modified  
876 from Saito et al., 2009). Depths denote the depth below sea level. The gray overlay  
877 shows the predicted area of horizontal  $\sigma_1$  (the maximum principal stress). Around  
878 megasplay site C0004 and the frontal thrust site C0006, two patterns of  $\sigma_1$   
879 distribution are considered to be possible. The first one is a gradual change: but the  
880 other shows a drastic change around the decollement and the megasplay suggested  
881 from the observations at ODP Site 808 and Alaska (Lallemant et al., 1993 and Byrne  
882 & Fisher, 1990).

883

884 Fig. 4 (2-column fitting) The maximum horizontal stress ( $S_{Hmax}$ ) orientations in SW and  
885 NE Japan subduction zones. Red bars at the drilling sites show the representative  
886  $S_{Hmax}$  orientations in the sites. Two rad rectangles in inset shows locations of figures  
887 (a) and (b), respectively. (a) Stress orientations at Site C0009 compiled from Lin et

888 al. (2010a) and Wu et al., (2012); C0002, C0001, C0004 and C0006 from Chang et al.  
889 (2010), C0011 from Expedition 322 Scientists (2010), C0012 from Yamamoto et al.  
890 (2013), and at ODP Site 808 from McNeill et al. (2004) and Ienaga et al. (2006).  
891 Yellow arrows show the far-field convergence vectors between the Philippine Sea  
892 plate and Japan (Heki and Miyazaki, 2001; Miyazaki and Heki, 2001). (b) Location of  
893 JFAST Site C0019 and  $S_{Hmax}$  orientation in the deep part of the borehole (Lin et al.,  
894 2013). Red solid and dashed lines show the mean  $S_{Hmax}$  orientation and one  
895 standard deviation (SD), respectively, determined in 2012 after the 2011 Tohoku  
896 earthquake. Green circles and lines show ODP sites drilled in 1999 and their  $S_{Hmax}$   
897 orientations prior to the 2011 earthquake (Lin et al., 2011). The gray arrow shows  
898 relative plate motion around Site C0019 (Argus et al., 2011). The white numbers  
899 and the contour lines show water depths.

900

901 Fig. 5 (2-column fitting) A comparison of seismic reflection profiles of NanTroSEIZE  
902 transect and around JFAST drilling site in the same scale (modified from Moore et al.,  
903 2009 and Kodaira et al., 2012 respectively) shows the overall similar structures. The  
904 five structure horizontal areas, the deep sea terrace, the upper, middle and lower  
905 slopes and the trench axis were defined by Kodaira et al. (2012). Site C0006 in the  
906 Nankai subduction zone is at the similar location as Site C0019 in the Japan Trench.  
907 At exact location of C0019 no wider seismic profile available, thus we used this  
908 profile locating just 15 km north of C0019.

909

910 Fig. 6 (2-column fitting) A comparison of stress states in the hanging wall of the frontal  
911 plate-interfaces in toe of Nankai and Japan Trench subduction zones revealed from  
912 Sites C0006 and C0019. (a) Possible stress state at 476 mbsf in borehole C0006B  
913 constrained from breakout width and assumed wall rock unconfined compressive  
914 strength (UCS) locates in the area of normal faulting stress regime (Wu et al., 2013).  
915 (b) Stress state at 468 mbsf in borehole C0006F determined from ASR  
916 measurements is of normal faulting stress regime being consistent with that from  
917 breakouts in C0006B (Byrne et al., 2009). (c) Possible stress state at 720 mbsf in  
918 borehole C0019B constrained from breakout width and measured UCS 3.8 MPa  
919 locates in the area of normal faulting stress regime (Lin et al., 2013). (d) Schematic  
920 of the current common stress state in the hanging wall of the frontal plate-interfaces  
921 in both Sites C0006 and C0019.

922

923 Fig. 7 (1.5-column fitting) Schematic of inferred coseismic three-dimensional stress state

924 change from a reverse faulting regime before the Tohoku-oki earthquake (a) to a  
925 normal faulting regime after the earthquake (b) in the lower portion of the frontal  
926 prism in Japan Trench subduction zone obtained from JFAST (Modified from Lin et  
927 al., 2013). NAP denotes North American Plate. Red arrows indicate the maximum  
928 principal stress ( $\sigma_1$ ); blue arrows: the intermediate principal stress ( $\sigma_2$ ); black  
929 arrows: the minimum principal stress ( $\sigma_3$ ). Because the static vertical stress ( $\sigma_v$ ) is  
930 under a mechanical equilibrium state with the overburden pressure (the gravity of  
931 the formations above the depth), the magnitude of  $\sigma_v$  may not change before and  
932 after the earthquake; however was the  $\sigma_3$  before the earthquake, the  $\sigma_1$  after the  
933 earthquake according to the changes of horizontal stress magnitudes during the  
934 earthquake.  
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Table 1 Specifications of the stress measurement related boreholes in NanTroSEIZE and JFAST drilling sites. For example, C0002 denotes the drilling site; whereas C0002A is the name of the borehole “A” located at Site C0002. Usually, multi boreholes were drilled for different operations within a narrow area (e.g. a few tens meters) in a site in IODP.

Holes (stress related operations)	Location		Water depth m	Total depth mbsf	Source of data
	Latitude	Longitude			
C0009A (WL&C*)	33°27.47'N	136°32.15'E	2054	1604	Exp 319 Summary
C0002A (LWD**)	33°18.02'N	136°38.18'E	1936	1402	Exp 314 Summary
C0002B (Coring)	33°17.99'N	136°38.20'E	1938	1057	Exp 315 Summary
C0001D (LWD)	33°14.33'N	136°42.70'E	2198	976	Exp 314 Summary
C0001E (Coring)	33°14.34'N	136°42.69'E	2198	118	Exp 315 Summary
C0001F (Coring)	33°14.34'N	136°42.71'E	2197	249	Exp 315 Summary
C0004B (LWD)	33°13.23'N	136°43.35'E	2637	400	Exp 314 Summary
C0010A (LWD)	33°12.60'N	136°41.12'E	2524	555	Exp 319 Summary
C0006B (LWD)	33°01.64'N	136°47.64'E	3872	886	Exp 314 Summary
C0006E (Coring)	33°01.64'N	136°47.63'E	3876	409	Exp 316 Summary
C0011A (LWD)	32°49.73'N	136°52.89'E	4049	952	Exp 319 Summary
C0012A (Coring)	32°44.89'N	136°55.02'E	3511	576	Exp 322 Summary
C0019B (LWD)	37°56.34'N	143°54.81'E	6890	851	Exp 343 Summary

871 \*WL&C: Wireline logging and coring

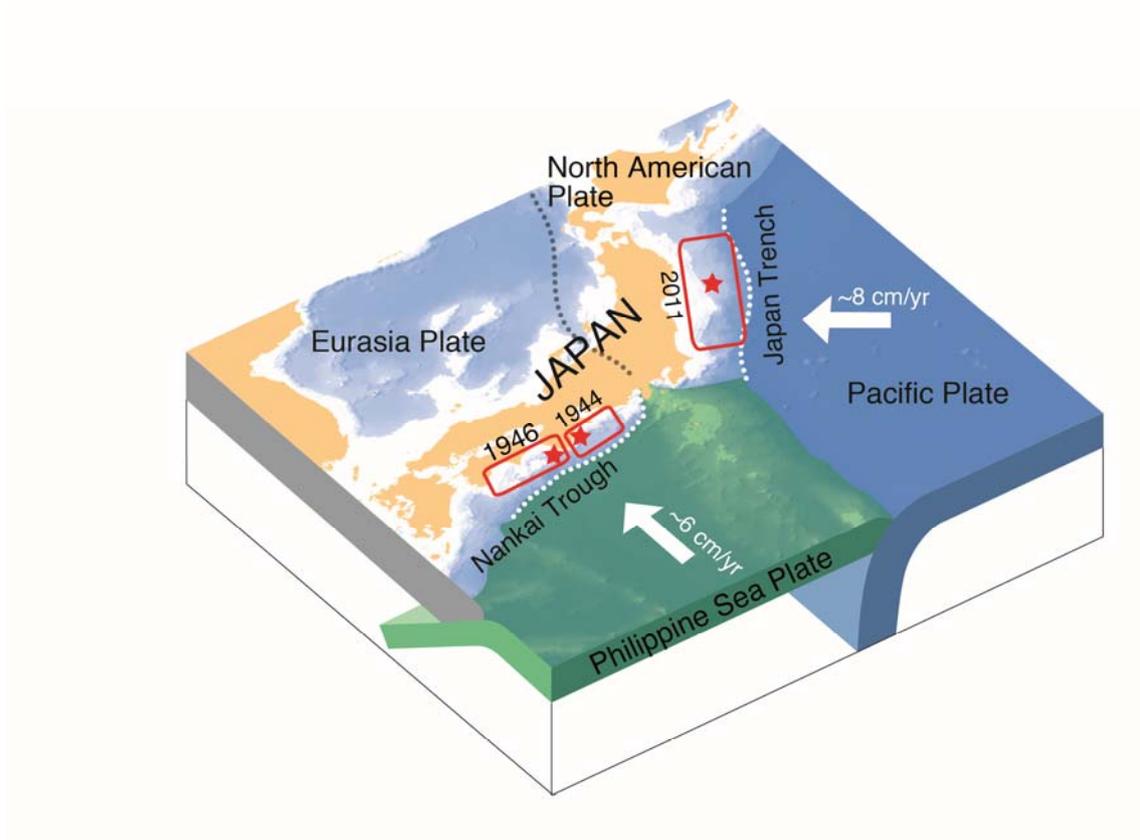
872 \*\*LWD: Logging While Drilling

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875 **Figures and their captions**

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879 Fig. 1 (1.5-column fitting) Nankai and Japan Trench subduction zones and plates around  
880 Japan islands. Red stars and numbers show the epicenters of the earthquakes and  
881 its occurrence year; the red frames are the area of rupture zones during the  
882 earthquakes. White arrows and numbers show directions and rates of plate motion,  
883 respectively (Sella et al., 2002; Apel et al., 2006; Loveless and Meade, 2010; Ozawa  
884 et al., 2011).

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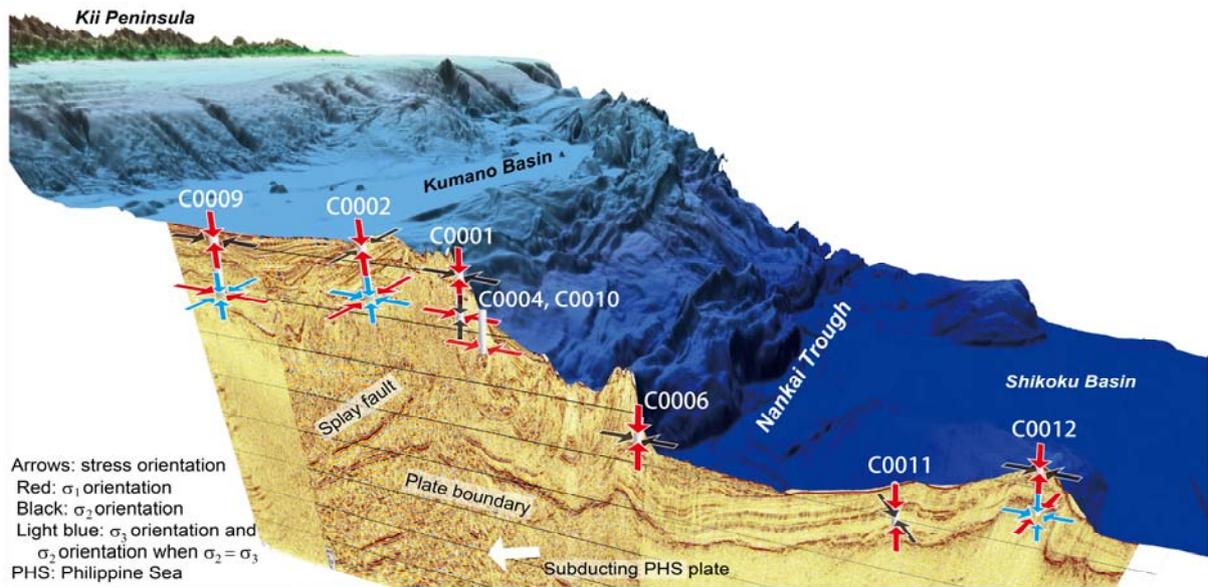


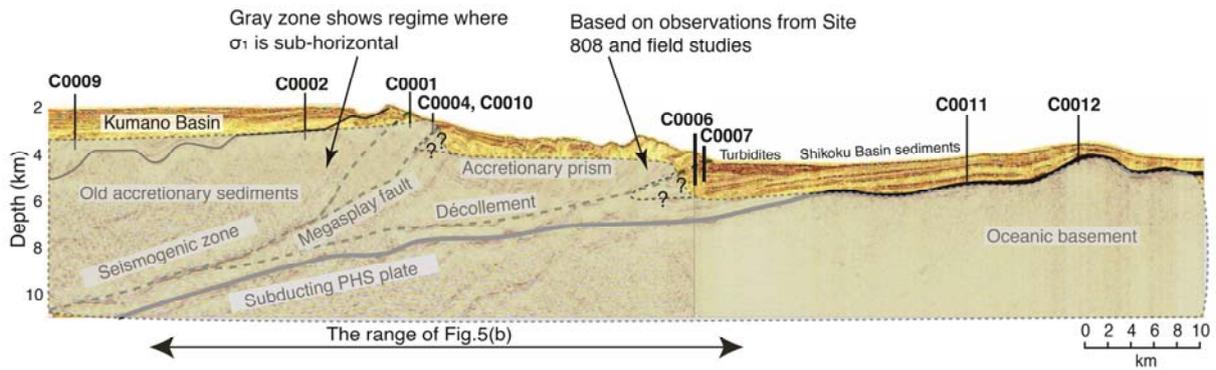
Figure 2 (2-column fitting)

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888 Fig. 2 (2-column fitting) Distributions of semi three-dimensional stress state in  
 889 NanTroSEIZE transect. Codes (e.g. C0009) are the number of drilling sites. Red,  
 890 black and light blue arrows are the orientations of the maximum, intermediate and  
 891 minimum principal stresses, respectively. Two pair arrows in the same light blue  
 892 color in the deeper part of C0009, C0002 and C0012 mean that the intermediate  
 893 and minimum principal stresses are nearly equal each other, or the intermediate  
 894 and minimum principal stresses are highly variable.

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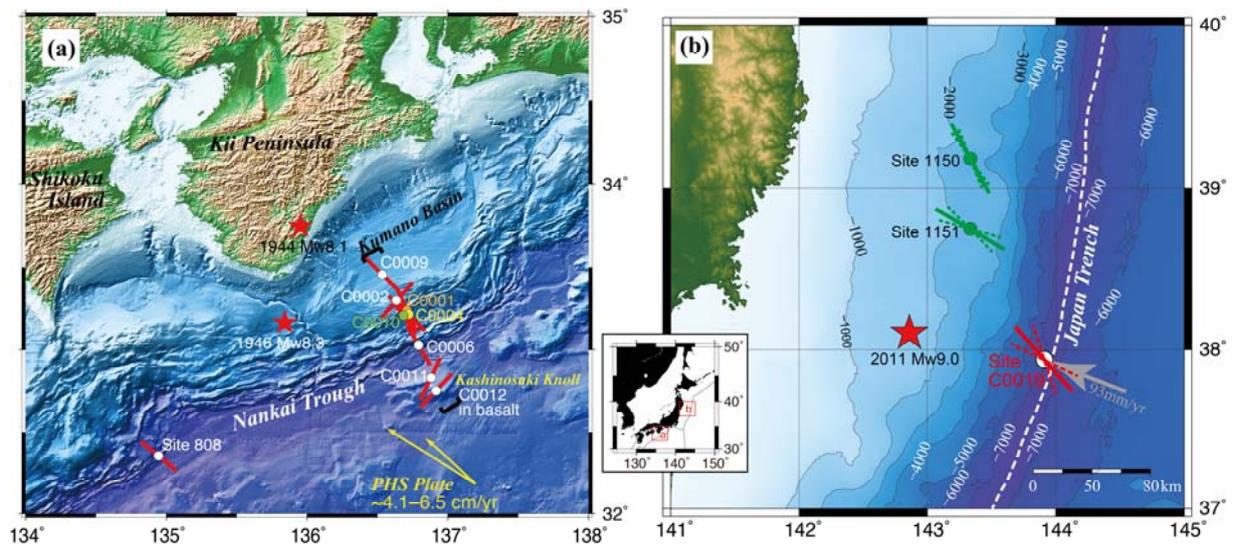
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899 Fig. 3 (2-column fitting) Seismic reflection section of NanTroSEIZE transect (modified  
900 from Saito et al., 2009). Depths denote the depth below sea level. The gray overlay  
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902 megasplay site C0004 and the frontal thrust site C0006, two patterns of  $\sigma_1$   
903 distribution are considered to be possible. The first one is a gradual change: but the  
904 other shows a drastic change around the decollement and the megasplay suggested  
905 from the observations at ODP Site 808 and Alaska (Lallemant-Lallemant et al., 1993  
906 and Byrne & Fisher, 1990).

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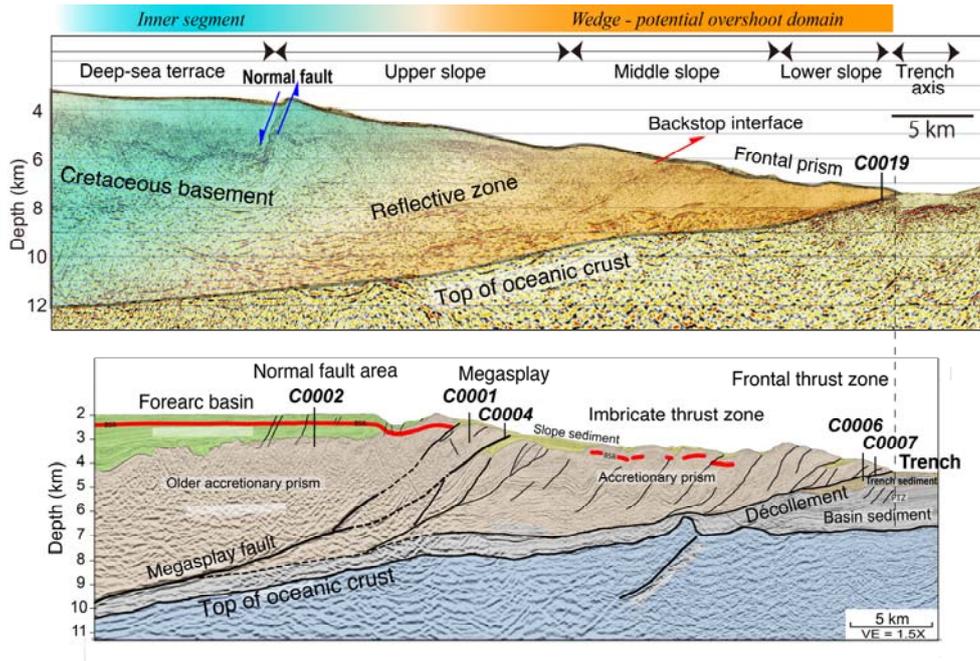
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912 Fig. 4 (2-column fitting) The maximum horizontal stress ( $S_{Hmax}$ ) orientations in SW and  
 913 NE Japan subduction zones. Red bars at the drilling sites show the representative  
 914  $S_{Hmax}$  orientations in the sites. Two red rectangles in inset shows locations of figures  
 915 (a) and (b), respectively. (a) Stress orientations at Site C0009 compiled from Lin et  
 916 al. (2010a) and Wu et al., (2012); C0002, C0001, C0004 and C0006 from Chang et al.  
 917 (2010), C0011 from Expedition 322 Scientists (2010), C0012 from Yamamoto et al.  
 918 (2013), and at ODP Site 808 from McNeill et al. (2004) and Ienaga et al. (2006).  
 919 Yellow arrows show the far-field convergence vectors between the Philippine Sea  
 920 plate and Japan (Heki and Miyazaki, 2001; Miyazaki and Heki, 2001). (b) Location of  
 921 JFAST Site C0019 and  $S_{Hmax}$  orientation in the deep part of the borehole (Lin et al.,  
 922 2013). Red solid and dashed lines show the mean  $S_{Hmax}$  orientation and one  
 923 standard deviation (SD), respectively, determined in 2012 after the 2011 Tohoku  
 924 earthquake. Green circles and lines show ODP sites drilled in 1999 and their  $S_{Hmax}$   
 925 orientations prior to the 2011 earthquake (Lin et al., 2011). The gray arrow shows  
 926 relative plate motion around Site C0019 (Argus et al., 2011). The white numbers  
 927 and the contour lines show water depths.

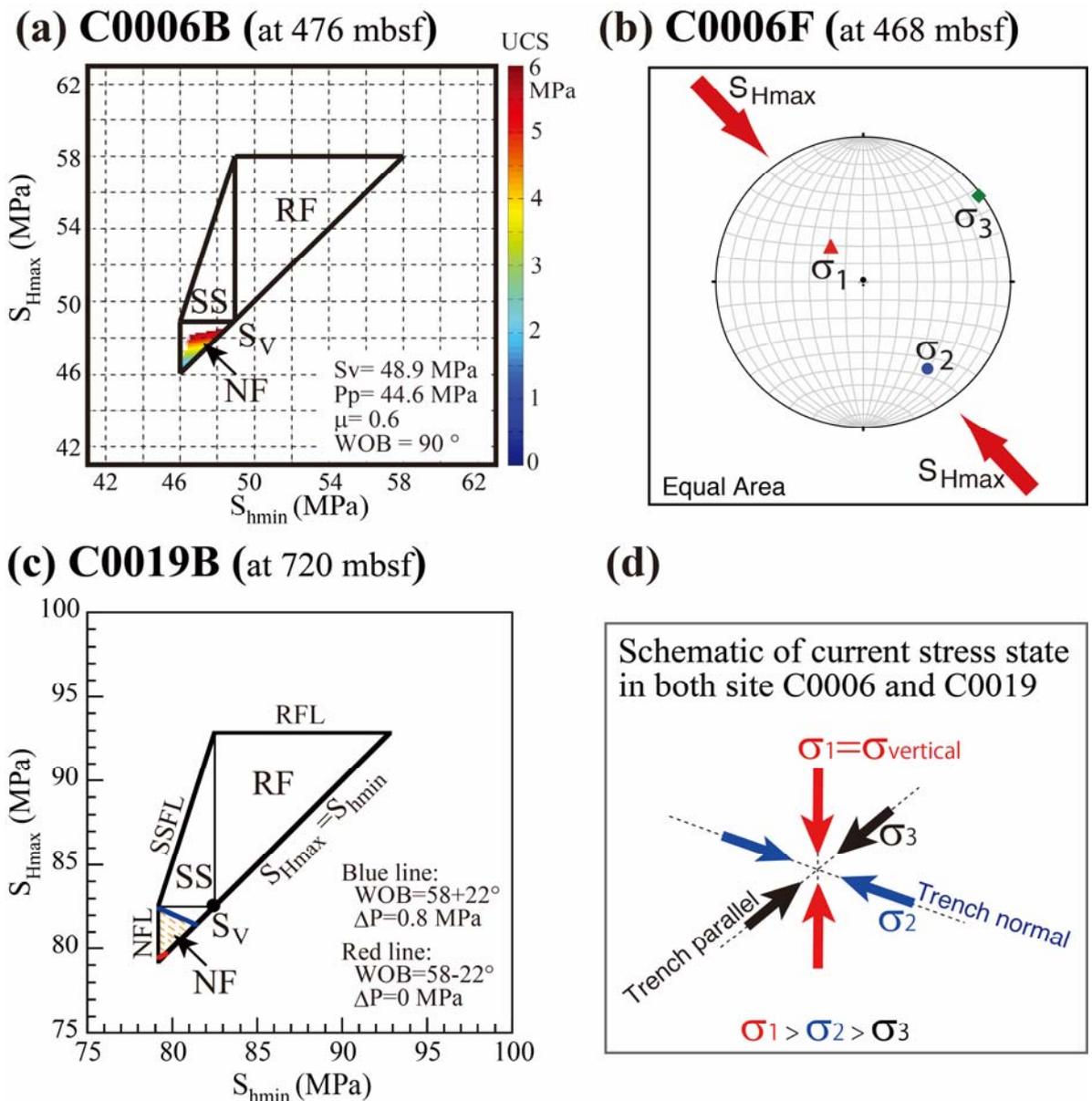
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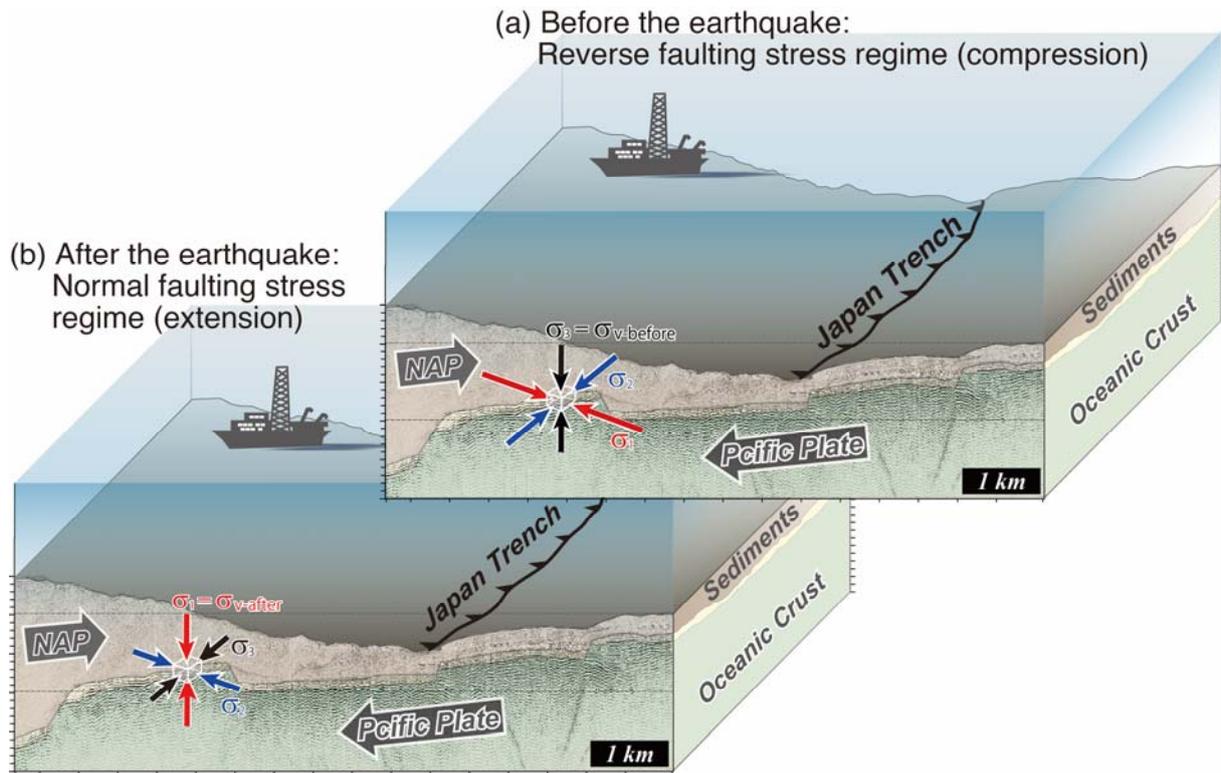
Fig. 5 (2-column fitting) A comparison of seismic reflection profiles of NanTroSEIZE transect and around JFAST drilling site in the same scale (modified from Moore et al., 2009 and Kodaira et al., 2012 respectively) shows the overall similar structures. The five structure horizontal areas, the deep sea terrace, the upper, middle and lower slopes and the trench axis were defined by Kodaira et al. (2012). Site C0006 in the Nankai subduction zone is at the similar location as Site C0019 in the Japan Trench. At exact location of C0019 no wider seismic profile available, thus we used this profile locating just 15 km north of C0019.



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943 Fig. 6 (2-column fitting) A comparison of stress states in the hanging wall of the frontal  
 944 plate-interfaces in toe of Nankai and Japan Trench subduction zones revealed from  
 945 Sites C0006 and C0019. (a) Possible stress state at 476 mbsf in borehole C0006B  
 946 constrained from breakout width and assumed wall rock unconfined compressive  
 947 strength (UCS) locates in the area of normal faulting stress regime (Wu et al., 2013).  
 948 (b) Stress state at 468 mbsf in borehole C0006F determined from ASR  
 949 measurements is of normal faulting stress regime being consistent with that from  
 950 breakouts in C0006B (Byrne et al., 2009). (c) Possible stress state at 720 mbsf in  
 951 borehole C0019B constrained from breakout width and measured UCS 3.8 MPa  
 952 locates in the area of normal faulting stress regime (Lin et al., 2013). (d) Schematic  
 953 of the current common stress state in the hanging wall of the frontal plate-interfaces  
 954 in both Sites C0006 and C0019.

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Fig. 7 (1.5-column fitting) Schematic of inferred coseismic three-dimensional stress state change from a reverse faulting regime before the Tohoku-oki earthquake (a) to a normal faulting regime after the earthquake (b) in the lower portion of the frontal prism in Japan Trench subduction zone obtained from JFAST (Modified from Lin et al., 2013). NAP denotes North American Plate. Red arrows indicate the maximum principal stress ( $\sigma_1$ ); blue arrows: the intermediate principal stress ( $\sigma_2$ ); black arrows: the minimum principal stress ( $\sigma_3$ ). Because the static vertical stress ( $\sigma_v$ ) is under a mechanical equilibrium state with the overburden pressure (the gravity of the formations above the depth), the magnitude of  $\sigma_v$  may not change before and after the earthquake; however was the  $\sigma_3$  before the earthquake, the  $\sigma_1$  after the earthquake according to the changes of horizontal stress magnitudes during the earthquake.