A Whole Mantle Attenuation Tomography based on the ISC Amplitude Data Analysis

by

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Abstract

A whole mantle P-wave attenuation structure was obtained by using the amplitude data reported by the International Seismological Center (ISC). Since the ISC amplitudes are measured for short-period body waves, they are likely to be affected strongly by site effects and the other factors. Therefore I analyzed amplitude fluctuations of the data before the inversion process.

The amplitudes from 3,445 events ($m_b < 7.0$) for 718 ISC stations in the world were analyzed from the ISC CD-ROMs. To eliminate various complicating effects, I have included only events that had at least 15 amplitudes at periods of 0.5 to 3.0 seconds and epicentral distances between 28 and 89 degrees. Data associated with travel paths that bottom in the lowermost mantle (>2700 km depth) are excluded to avoid the diffraction effect of the D" layer. Hypocenter parameters were obtained from the database improved by Engdahl et al. [1998], and source mechanism are taken from Harvard and USGS moment tensor solutions. Average station terms and azimuth-independent station terms and first and second azimuthdependent station terms were calculated for relative log-scaled amplitude and relative travel time residuals. The average terms and the azimuth-independent terms for amplitudes of stations in the central part of old continents, such as Eurasia and North America, are generally large, while small for stations around the Pacific Ocean and the southern Europe. These station anomalies seem to have a only weak correlation with the type of crustal structure. The first azimuthal terms have more complex distributions and do not show an obvious global tendency. The second-azimuthal terms are distributed systematically in an E-W direction in the western Pacific Ocean, in a N-S direction in North America, and mixed directions in Europe. The travel time residuals show the results that are similar to Dziewonski and Anderson [1983]. The second azimuthal terms show a relation to the S-wave polarization anisotropy.

The whole mantle three-dimensional structure of P-wave attenuation was then obtained by applying a tomographic method to the amplitude data of the ISC Bulletin. A grid

modeling tomographic method was developed and applied to the data. The simultaneous inversion technique determined source amplitudes and a one-dimensional attenuation structure down to 2,700 km depth, then three-dimensional perturbations from the 1-D model were obtained. The attenuation in the upper mantle is stronger than that in the lower mantle. Such tendency is also seen in the various standard Earth models obtained from free-oscillation analyses. The long-wavelength lateral variations in attenuation show similar patterns to previous P-wave velocity studies. A major high attenuation zone appears to be located in the central Pacific in the middle to lower mantle, while there is low-attenuation spreading beneath the Eurasia continental shield in the upper to middle mantle. There exists some remarkably high attenuation zones through the upper and lower mantle. Hotspots are located around these regions, therefore, the high attenuation may be due to upwelling flow.

This study presents the first model of whole mantle attenuation heterogeneity for short-period body waves. This new information will contribute valuable information for investigations about geothermal and geodynamical features of the Earth.

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-4-

Note

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This thesis is based on the following papers:

- Amplitude and travel time fluctuations for the ISC stations, submitted to Journal of Geophysical Research, by Hiroaki Negishi
- A whole mantle attenuation tomography based on the ISC amplitude analysis, to be submitted to Geophysical Journal International, by Hiroaki Negishi
- Amplitude and arrival time fluctuations of teleseismic P waves observed in northern part of Tohoku region, Japan, Journal of Seismological Society of Japan, **46**, 297 - 308, 1993, by Hiroaki Negishi and Tamao Sato.
- The three-dimensional attenuation structure beneath the Philippine archipelago based on seismic intensity data inversion, Earth and Planetary Science Letters, **151**, 1 11, 1997, by Glenda M. Besana, Hiroaki Negishi and Masataka Ando.
- The 1995 Kobe earthquake: Seismic image of the source zone and its implications for the rupture nucleation, Journal of Geophysical Research, **103**, 9967 9986, 1998, by Dapeng Zhao and Hiroaki Negishi.

-5-

Table of Contents

		page
Abstract		2
Acknowledg	ments	4
Note		5
Chapter 1.	General Introduction	9
Figure	es	13
Chapter 2.	Amplitude and travel time fluctuations for P waves at	
	teleseismic distances	16
2.1	Introduction	17
2.2	Dataset and other settings	. 18
	2.2.1 ISC Bulletin	18
	2.2.2 P phase amplitude data	19
	2.2.3 Earth model of velocity structure	20
	2.2.4 Hypocentral parameters	21
	2.2.5 Source mechanisms and geometrical spreading	22
2.3	Relative log-scaled amplitude analysis	23
2.4	Results of amplitude analysis	25
2.5	Travel time data analysis	27
2.6	Discussion	29

	2.6.1 Correlation between amplitude and travel time	29
	2.6.2 Crustal structure and amplitude	30
Figures		
Chapter 3.	A whole mantle P wave attenuation structure obtained from	
	ISC amplitude data	65
3.1	Introduction	66
3.2	Methodology of grid model attenuation tomography	67
	3.2.1 Basic theory of attenuation tomography	67
	3.2.2 Grid modeling formulation	68
	3.2.3 Smoothness constraint	72
	3.2.4 LSQR inversion algorithm	74
	3.2.5 Resolution	75
3.3	One-dimensional attenuation structure and setting for	
	tomographic inversion	77
	3.3.1 Setting of data and modeling space	77
	3.3.2 Results of one-dimensional inversion	79
	3.3.3 Setting and conducting the tomographic inversion	80
	3.3.4 Checkerboard resolution test	81
3.4	Tomographic result	82
3.5	Discussion	86

Tables	5	89
Figures		91
Chapter 4.	General Conclusion	170
Bibliography		173
Appendix A.	Azimuthal variation of log-amplitude anomaly and	
	relative travel time residuals.	183
A-1	Azimuthal variation of log-amplitude	184
A-2	Azimuthal variation of travel time	206
Appendix B.	Amplitude and travel time station corrections for ISC stations.	228
B-1	Amplitude station corrections	229
B-2	Travel time station corrections	234
Appendix C.	The whole-mantle P-wave attenuation structure : QPB3DV2	240

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Chapter 1. General Introduction

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Studying of the Earth's deep interior is one of the basic problems in Earth and planetary sciences. The seismic and volcanic activity of the planetary Earth is mainly due to the dynamics of the mantle and core. Seismological data have provided us with much information about the internal structure of the Earth, and have brought great help to understanding the Earth's dynamics, thermal structure, and origin. Particularly, arrival time data of various seismic phases are most important and useful information. Hypocenter distributions which are determined by many arrival times have cleared the images of subducted plates, active faults and thermal boundaries in the crust and mantle. In the 1930's, a spherically symmetric Earth model was constructed by Jeffreys and Bullen [1940] by analyzing arrival times of the world-wide data. This new information shed light onto the Earth. After the discovery of plate tectonics, there was considerable interest in the large-scale heterogeneity of the mantle. Many studies have been carried out to map the global variations of the upper mantle structure by using surface wave analysis, because surface waves can sample the entire globe rather uniformly in spite of a non-uniform distribution of earthquakes and seismic stations [Inoue, 1993].

Many heterogeneous images have been obtained for the Earth's interior by using travel time analysis, starting from the pioneering studies of Aki and Lee [1976] and Aki *et al.* [1977]. Their method has been improved and applied to local and regional studies (*e.g.*, Hirahara *et al.* [1989], Thurber [1983], Zhao *et al.* [1992], Negishi [1996], Zhao *et al.* [1996], Zhao and Negishi [1998]). Arrival times of short-period body waves can be used for not only regional studies but also global studies. Particularly, telescismic P-phases enable study of the deeper parts of the Earth because of clear phase and ray bottoming depths, while surface waves have much less information about the lower mantle. Cleary and Hales [1966] first analyzed the travel times of telescismic P-phases to calculate a world-wide distribution of station anomalies, and they found earlier arrivals of P phases in shield and the Western Pacific areas and later arrivals in the active tectonic regions. In 1980's, some investigators tried to image the whole mantle elastic structure. Dziewonski [1984] inverted 500,000 telescismic P arrivals from 5,000 shallow events to obtain a model of lower mantle heterogeneity (Fig. 1.1). The upper mantle heterogeneity was assumed to be incorporated in adjustments of hypocenter and

azimuth-dependent station corrections obtained by Dziewonski and Anderson [1983]. Negishi and Sato [1993] applied this method to the amplitude and arrival time data observed in northern part of Tohoku region, Japan. I use the same method in Chapter 2 of this thesis. Inoue *et al.* [1990] inverted over 2,000,000 arrivals of P-waves to obtain a three-dimensional P-wave velocity structure for the whole mantle of the Earth. This was the first study which delineated the entire mantle structure with reliability mapping (Fig. 1.2). With improvements of computer algorithms and developments in computer power, investigators have applied tomographic techniques to huge data sets of arrival times and constructed not only P-wave velocity but also S-wave velocity and bulk sound structure of the Earth (*e.g.*, Pulliam *et al.* [1993], van der Hilst *et al.* [1997], Kennett *et al.* [1998]). We can say that we already have a general image of the "elastic Earth".

On the other hand, do we have a general image of the "anelastic Earth" as well ?

Anelasticity of the Earth reflects the thermal state and the other physical properties more sensitively than elasticity. The attenuation of seismic waves is one of the parameters that represents the Earth's anelasticity. The attenuation of seismic waves, which can be specified by the quality factor Q, has an important bearing on the physical state of the Earth's deep interior, such as the temperature, the degree of partial melting, and so forth. Hence, extensive investigations of variations of attenuation are particularly important for better understanding of the dynamics of the Earth's interior. The attenuation structure of the Earth has been studied by using mainly long-period seismic data, free oscillation of the Earth and long-period surface waves. In the 1960's and 1970's, some depth-dependent Q models were established on the basis of such long-period data (e.g., MM8 by Anderson et al. [1965], Model G by Teng [1968], SL8 by Anderson and Hart [1978]). Dziewonski and Anderson [1981] analyzed a large data set of body waves, surface waves and free oscillations of the Earth, and obtained the radial model of velocity, Q, density, and the other physical parameters. This model, Preliminary Reference Earth Model (PREM), is still used by many geoscientists. This attenuation model was recently improved by Montagner and Kennett [1996] with a more recent velocity structure, and they established a new standard Earth model, named AK135. Tomographic studies of global attenuation heterogeneity have also

been done using long-period surface waves and free oscillations of the Earth (*e.g.*, Suda *et al.* [1991], Durek *et al.* [1993], Romanowicz [1995]). These investigations, however, resolved only the upper mantle. The whole mantle image of attenuation heterogeneity is not yet clear.

Recently I took notice of the amplitude data reported in the Bulletin of the International Seismological Center. The International Seismological Center (ISC) have compiled vast amounts of P-, S- and some later phase data from 1964 to the present. Many investigators have used the data to obtain regional to global scale heterogeneous structures of the Earth. The compiled data include not only arrival time but also amplitude of the first-arrival phase in order to determine magnitude, m_b . These data, however, have seldom been used for structural investigations because seismologists have considered the amplitude values unreliable, because of contamination by uncertainty factors (*e.g.*, site effects due to local geology, ground noise, picking error). However, I thought that the structural information can be resolved from the data by applying appropriate corrections. Statistical characteristics of short-period amplitudes of P-waves have been analyzed by several investigators (Stewart [1981], Nakanishi and Motoya [1990], Negishi and Sato [1993]). They found that the teleseismic amplitude data of short-period P-waves include not only site effects, such as local geology, but also the effects of lateral heterogeneity in the crust and the upper mantle.

In this thesis, I applied a tomographic approach to obtain a whole mantle attenuation structure, using the ISC amplitude data. In Chapter 2, I analyzed the fluctuations of the ISC amplitude based on the statistical method of Negishi and Sato [1993], and defined station corrections of amplitude, "relative log-scaled amplitude anomaly". This parameter corresponds to the travel time station corrections defined by Dziewonski and Anderson [1983]. In Chapter 3, a whole mantle P-wave attenuation structure was obtained by using the ISC amplitude data, with application of the amplitude station corrections obtained in the previous chapter. A grid model attenuation tomographic method, which is one of an approach for representing the three-dimensional attenuation heterogeneity, was adopted. This model is clearly very preliminary and the details of the patterns will likely change as our ability to gain resolution increases in the future. But this is the first model which delineates the whole mantle attenuation structure including the lower mantle.

Figure Captions

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- Fig. 1.1 Maps of the P-wave velocity heterogeneity at six different depths in the lower mantle. Black and white patterns indicate faster and slower anomalies than the average velocity at each depth, respectively. The indicated rage is ± 1 % for the depth of 670 km, and ± 0.5 % for the other depths (after Dziewonski [1984]).
- Fig. 1.2 P-wave velocity heterogeneity in the whole mantle. Slowness perturbations from the averages at each depth are shown. Fast and slow anomalies are indicated by cross and circles, respectively. The size of the symbols is proportional to the square root of the perturbation (after Inoue *et al.* [1990]).





Figure 1.2

Chapter 2.

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Amplitude and travel time fluctuations for P waves at teleseismic distances

2.1 Introduction

The arrival time data of the International Seismological Center Bulletin (ISCB) have been used for various seismological investigations of the Earth's deep interior. Dziewonski and Anderson [1981] used a very large set of the data for the years 1964 to 1975 to obtain a travel time curve which, together with other subsets of data, was used to derive the Preliminary Reference Earth Model (PREM). Recently some heterogeneous whole mantle images have been derived by applying tomographic methods to more than two million and even more arrival times of the ISCB. These models shed light on the study of mantle dynamics and understanding the Earth's global tectonics, such as slab penetration into the lower mantle (*e.g.*, Fukao *et al.* [1992], Kennett *et al.* [1998]).

On the other hand, amplitude and period data around the first arrival phase have also been reported in the same bulletin in order to determine magnitude, m_b . These data, however, have rarely been used in any structural studies because even the fundamental nature of the ISC short-period amplitudes is not well known and seismologists have considered amplitude values unreliable for analysis, because of contamination by uncertainty factors at each site, such as local geology, ground noise, and picking error. However, this means that the ISC amplitude data may become usable by applying suitable correction for the characteristic values of various site effects. Since amplitudes are sensitive to partial derivatives of velocity and to anelasticity more detailed structures may be resolved by combining amplitudes with the travel time data (Thomson and Gubbins [1982]). For example, Haddon and Husebye [1978] used amplitude data to investigate the velocity heterogeneity beneath the Norwegian Seismic Array (NORSAR) in conjunction with the travel times.

Dziewonski and Anderson [1983] investigated the fluctuations of P wave travel times of the ISCB and obtained station residuals, including azimuthal effects, for 994 seismic stations. They found that the azimuthally station corrections exhibit general consistency over broad geographic areas. It is expected that a significant part of the effect of velocity anomalies in the upper mantle can be accommodated by the static and azimuthal dependent station corrections. They applied these station corrections to the tomographic study (Dziewonski [1984]) and succeeded in deriving three-dimensional model of lateral variations of the P-wave velocity in the lower mantle. Such azimuthal station corrections can provide great help toward understanding the Earth's heterogeneity.

From the above view point, I tried to clarify the fundamental characteristics of the ISC amplitude and travel time data. First, relative log-scaled amplitude anomalies were obtained by statistical analysis. The azimuthally dependent station corrections were also estimated by using the new data base which includes events relocated with the AK135 model (Kennett *et al.* [1995]), generalized by Engdahl *et al.* [1998]. Correlation between relative log-scaled amplitude anomalies and relative travel time residuals are then discussed for each station to conclude whether the amplitude is more affected by the heterogeneity of velocity (focusing or defocusing) or the attenuation.

2.2 Dataset and other settings

2.2.1 ISC Bulletin

The ISC has been compiling data reported from a large number of seismograph stations all over the world. The ISC Bulletin has long been utilized by seismologists as an invaluable data source for studying world seismicity and structure of the Earth's interior. All the arrival time data and hypocenter locations reported from local agencies are compiled by the ISC and re-determined from the first P-wave arrivals using the Jeffreys-Bullen travel time tables (Jeffreys and Bullen [1940]) and the Earth's ellipticity correction suggested by Gutenberg and Richter [1933]. The database contains numerous kinds of earthquake information, such as hypocentral parameters, processed data of various seismic phases, and disaster information. These data are published as printed and machine-readable bulletins with a typical delay of two vears. Figure 2.1 shows an example of the printed book page. Adherence to this rather conservative manner of processing has resulted in the uniformity and reliability of the database. The detailed procedure of the analysis by the ISC is given in Adams *et al.* [1982].

2.2.2 P phase amplitude data

The ISC Bulletin have reported unified magnitudes, m_b , following the procedure outlined by Gutenberg and Richter [1956] for P waves of period shorter than 3 seconds. These amplitudes and periods are measured on short-period vertical instruments. If Q denotes the depth-distance factor, A the amplitude in nanometers and T the period in seconds for the i-th station, then for N observations

$$m_b = \frac{1}{N} \sum_{i=1}^{N} \left[\mathcal{Q}(\Delta_i, h) + \log 10 \left(\frac{A_i}{T_i}\right) \right] - 3$$
(2.2.1)

In this equation, $Q(\Delta_i, h)$ includes structural effects of the Earth's interior, so it is possible that the fluctuations of m_b are related to variations in attenuation along the ray path. Stewart [1981] tried to delineate P-wave attenuation anomalies in the lower mantle under the North Atlantic by assuming that body-wave magnitude residuals are due to structure near the bottoming-points of the rays.

The ISC Bulletin have been issued from 1964 in the form of bulletin books and CD-ROMs, but the data prior to 1983 cannot be used for the present investigation since only the log10(Amplitude/Period) value had been reported. Most of the ISC data are for small events with relatively few reports by individual stations and such events have to be omitted, because they do not provide enough statistical information. I excluded the events greater than magnitude 7, since the effects of source directivity and complexity of the source process could not be ignored for body wave amplitudes in such larger event (Mikumo [1969]). I included events that had at least 15 amplitude data with periods between 0.5 and 3.0 seconds at epicentral distances of 28° and 89°. In this range of epicentral distance, the first arrival phase is direct-P and no other phases are included in the 3 second time window after the P-phase in the AK135 velocity model (Kennett *et al.* [1995]) which I used here. Figures 2.2 (a) and (b) show the WKBJ synthetic record section as a function of epicentral distance and their

amplitudes, respectively. The P-wave amplitudes decay gradually with distance, but being to grow in amplitude at farther than about 90 degree. This is due to the diffraction effect in the lowermost mantle layer, called the D" layer. Therefore, the data associated with rays bottoming in the lower mantle (>2,700 km depth) are excluded to eliminate diffraction effect for the D" layer. To avoid contamination from depth phases, event shallower than 10 km were omitted. Using the constraints stated above, 155,778 amplitudes data, observed at 718 stations from 3,445 events, remained for use in the present study. Figures 2.3 and 2.4 show the epicentral distribution of the events and locations of the stations, respectively.

2.2.3 Earth model of velocity structure

Following the pioneering study of Jeffreys and Bullen [1940], investigators produced radial velocity models using a wide variety of different techniques and different data (e.g., Herrin et al. [1968], Dziewonski and Anderson [1981], Kennett and Engdahl [1991]). The locations provided by the ISC are determined using the Jeffreys and Bullen [1940] travel time tables. It has been recognized for many years that there was a baseline problem with the tables, because events with independently determined locations show origin-time errors of the order of 2 seconds. A major effort to improve P-wave travel time tables was made in 1968 (Herrin et al. [1968]), but the absence of S-phase arrival times limited the usefulness of this set of tables. An initiative by the International Association of Seismology and Physics of the Earth's Interior (IASPEI) to improve earthquake locations led to the construction of the IASP91 model (Kennett and Engdahl [1991]) and the SP6 model (Morelli and Dziewonski [1993]). From these models, travel times can be calculated for the full range of seismic phases; the main phases have been tabulated (Kennett [1991]) and the same material is available in computational form. The P-wave travel times for these two models are in very close agreement to distances of 80 degrees, and both models indicate an average offset of 1.7 seconds from the Jeffreys and Bullen tables, which is likely to be manifest in the ISC event parameters. Recently, Kennett et al. [1995] refined the IASP91 model by relocating events using the IASP91 model, depth phases and re-associating phase picks. The new preferred model, AK135 (shown in Fig. 2.5), gives a significantly better fit to a broad range of phases

than that is provided by the IASP91 and SP6 models (Kennett *et al.* [1995]). I used this AK135 model for calculating geometrical spreading and ray tracing in this study.

2.2.4 Hypocentral parameters

The ISC uses a standard least-squares procedure based on Jeffreys' method of uniform reduction (Jeffreys [1932, 1939], Adams *et al.* [1982]) to obtain hypocenters. The location parameters are determined by using only first-arriving P-wave travel times, which for most events do not include P-wave arrivals corresponding to upgoing ray paths. The distribution of earthquakes is highly heterogeneous on a global scale, and most earthquakes occur in or near subduction zones where lateral variations in seismic velocities of 4 to 8% are not uncommon (Engdahl *et al.* [1998]). Seismological stations are also heterogeneous, mostly located in continental areas and on some islands in oceanic region. Such biased distribution of events and stations lead to large shifts of hypocenter and origin time. Hence, many ISC hypocenters are poorly constrained. It is well known that such mislocation of hypocenters masks structural signals. For example, Davies [1992] showed that mislocation contributes up to 35 % to the travel-time variance signal at teleseismic distances for earthquakes.

Recently Engdahl *et al.* [1998] relocated nearly 100,000 events that occurred during the period from 1964 to 1995 and are well-constrained teleseismically by arrival-time data reported to the ISC and to the USGS-NEIC (National Earthquake Information Center). Their data set of relocated hypocenters, named EHB, is calculated by using not only the P phases but some other phases, S, PKiKP, PKPdf and the teleseismic depth phases pP, pwP, and sP. These source parameters were determined by the new standard model AK135 (Kennett *et al.* [1995]) and ellipticity corrections (Kennett and Gudmundsson [1996]). Figure 2.6 shows an example of the EHB epicenter relocation vectors relative to the ISC epicenters (Engdahl *et al.* [1998]). The largest difference is over 30 km, which corresponds to a travel-time difference of about 4 seconds. This difference cannot be ignored for velocity and attenuation analysis. These hypocentral parameters were used in this study.

2.2.5 Source mechanisms and geometrical spreading

Focal mechanism solutions are also needed to remove the effects of radiation pattern. A double-couple mechanism was assumed here. Figure 2.7 shows the definition of the fault-orientation parameters and the definition of ray propagation directions. We can obtain the radiation pattern from a double-couple point source for P-waves, R, as

$$R = \cos \lambda \sin \delta \sin^{2} i_{\xi} \sin 2(\phi - \phi_{s}) - \cos \lambda \cos \delta \sin 2i_{\xi} \cos(\phi - \phi_{s}) + \sin \lambda \sin 2\delta \left\{ \cos^{2} i_{\xi} - \sin^{2} i_{\xi} \sin^{2}(\phi - \phi_{s}) \right\}$$

$$+ \sin \lambda \cos 2\delta \sin 2i_{\xi} \sin(\phi - \phi_{s})$$

$$(2.2.2)$$

where $(\phi_s, \lambda, \delta)$ are fault orientation parameters (strike, dip, rake) and (i_{ξ}, ϕ) are angular ray coordinates (emergence angle from down, azimuth from North), respectively (Aki and Richards [1980]). Figure 2.8 shows the radiation pattern from a point source double couple (Kennett [1983]). The observed amplitude should be divided by this factor to correct for the radiation pattern. The data that emerges near nodal planes (sin theta < 0.1) are excluded. I used the USGS-NEIC and Harvard centroid moment tensor solutions for correction of the radiation pattern for all of events used in this study.

The body wave amplitude from a point source is proportional to the inverse of the hypocentral distance in a homogeneous non-attenuate ($Q=\infty$) media. In a laterally-homogeneous spherical Earth, the geometrical spreading for a seismic wave amplitude can be expressed by (*e.g.*, Aki and Richards [1980])

$$G = \frac{1}{R_0} \sqrt{\frac{\rho_0 V_0}{\rho_s V_s} \frac{\sin \theta}{\sin \Delta \cos i_0} \frac{d\theta}{d\Delta}}$$
(2.2.3)

where R_0 is the radius of the Earth, ρ_0 and V_0 the density and the velocity at the surface, ρ_s and V_s the density and the velocity at the source, Δ the angular epicentral distance, θ the emergence angle measured from vertical, and i_0 the incident angle measure from vertical, as shown in Figure 2.9. I applied these corrections to the observed amplitude data by using the AK135 velocity and density model.

2.3 Relative log-scaled amplitude analysis

Body-wave amplitudes from a teleseismic event are controlled by various effects, such as source magnitude, geometrical spreading, structural effects, and source mechanism. Therefore, these effects have to be corrected before carrying out statistical analyses of amplitudes from a large number of teleseismic events. The amplitude that is recorded at the jth station from the i-th event in a certain frequency range can be expressed by the following equation;

$$A_{ij} = M_i \cdot R_{ij} \cdot G_{ij} \cdot X_{ij} \cdot C_j \tag{2.3.1}$$

where A_{ij} is the amplitude observed at the j-th station from the i-th event, M_i is the source amplitude of i-th event, R_{ij} is the effect of radiation pattern, G_{ij} is the geometrical spreading and attenuation effects in spherical homogeneous structure, X_{ij} indicates the effects of the lateral heterogeneity of velocity and attenuation in the mantle, and C_j is the site effect at the j-th station. When we already know (or suppose) the spherical structure, hypocenter locations, and source mechanisms for all events, the equation for the average of the commonlogarithm of (2.3.1) for each event is,

$$\frac{1}{N_i} \sum_{j} \left(\log A_{ij} \right) = \frac{1}{N_i} \left[\sum_{j} \left(\log C_j \right) + \sum_{j} \left(\log X_{ij} \right) \right] + \log M_i$$
(2.3.2)

where N_i indicates the number of data for i-th event. We should assume one-dimensional structures for both velocity and attenuation to estimate G_{ij} . Figure 2.10 (a) shows the WKBJ synthetic seismograms for vertical components at the surface from a 10 km deep source, displayed with a reduction slowness of 7.0 seconds per degree. The amplitude variations of the figure (a) is shown in Figure 2.10 (b). The seismograms were calculated using a non-attenuating AK135 model (left), and an attenuation-included model (Montagner and Kennett [1996]) (right). The amplitudes are normalized by the maximum trace in each figure. The absolute values of each amplitude are much different, but the amplitude variation shows same

pattern between non-attenuated seismograms and attenuated traces. This indicates that the 1-D attenuation effect can be excluded if we analyze relative amplitude variations for each event, so only the 1-D velocity structure is used for estimating G_{ij} . Substitution of (2.3.2) from the logarithm of (2.3.1) becomes,

$$R(\log A)_{ij} = R(\log C)_{j} + R(\log X)_{ij}$$
(2.3.3)

where

$$R(\log A)_{ij} = \log A_{ij} - \frac{1}{N_i} \sum_{j} (\log A_{ij})$$

$$R(\log C)_j = \log C_j - \frac{1}{N_i} \sum_{j} (\log C_j)$$

$$R(\log X)_{ij} = \log X_{ij} - \frac{1}{N_i} \sum_{j} (\log X_{ij})$$
(2.3.4)

Here we call $R(\log A)_{ij}$ the "Relative log-scaled amplitude anomaly (hereinafter referred to as log-amplitude anomaly)" (Negishi and Sato [1993]). We can obtain the lateral heterogeneity term X_{ij} directly when C_j is already known. The estimation of the site effect is, however, so difficult that usually we do not know them. But if we suppose that

$$\sum_{j} \left(\log C_j \right) = 0 \tag{2.3.5}$$

and the following relation is satisfied for each station,

$$\sum_{i} \left\{ R(\log X)_{ij} \right\} = 0 \tag{2.3.6}$$

the site effect term can be written as

$$\log C_j = \frac{1}{K_j} \sum_{i} \left\{ R(\log A)_{ij} \right\}$$
(2.3.7)

where K_j is the number of the event recorded at the j-th station. Therefore, we can obtain the site effect term by averaging the log-amplitude anomaly for each station. Figure 2.11 shows examples of histogram of relative log-amplitude anomalies (left-side of the equation (2.3.3)) at each station. The amplitude data have a lognormal distribution, the same tendency as

observed by Ringdal [1976, 1977]. This indicates that the log-amplitude fluctuation can be expressed by the combination of the station bias, $R(log C)_j$, and the lognormal-distributed components, that include the effects of heterogeneous structure and random noise. So the assumption of equations (2.3.5) and (2.3.6) are appropriate here.

2.4 Results of amplitude analysis

Figure 2.12 shows the spatial distribution of the site effect terms (right-hand side of the equation (2.3.7)). Open circles and diamonds indicate larger and smaller amplitudes, respectively. The sizes of the symbols are proportional to the anomaly according to the indicated scale. The site effect terms show an obvious geographical variation as can be seen in the figure. The amplitudes are systematically large for stations in the central and southern part of the Eurasia continent, such as China, India and Russia, while stations with small amplitude are concentrated in the Circum-Pacific belt, such as western North America, East-and Southeast-Asia, and Australia. These patterns seems to reflect the differences of the crust and the uppermost mantle structure beneath old continental shield and tectonically-active zones. On the other hand, amplitudes are medium scale for most of the stations in central North America, and a mixture of larger and smaller amplitudes are observed in Europe.

I applied the azimuthal dependency approach (Cleary and Hales [1966], Dziewonski and Anderson [1983]) to the log-amplitude anomalies. Because the azimuthal distribution of events with respect to the station tends to be uneven, azimuthal fluctuations of amplitude anomalies were obtained by the following procedure. The full azimuth range is divided into 18 windows, 20 degree wide. An average of log-amplitude anomalies is calculated if there are at least three data in each given window. These averages are treated with equal weight to reduce the bias due to unequal distribution of events (Dziewonski and Anderson [1983]). Then, the

-25-

least squares approach is used to determine azimuthal fluctuations of the amplitude anomaly for each station in the equation,

$$R(\log A)_{ij} = A_0 + A_1 \cos\left(\theta_{ij} - \theta_1\right) + A_2 \cos\left(\theta_{ij} - \theta_2\right)$$
(2.4.1)

where A_0 , A_1 and A_2 are the azimuth-independent term, first azimuthal dependent term, and second azimuthal dependent term, respectively. θ_{ij} is the azimuth viewed from the j-th station to the i-th event. θ_1 and θ_2 denote the direction of largest amplitude for the first and second azimuthally dependent terms, respectively. We can easily see that the azimuthindependent term (A_0) corresponds to $R(\log C)_i$, and the azimuth-dependent terms $(A_1$ and A_2) are the same as $R(\log X)_{ij}$ in the equation (2.3.3). A_0 becomes equal to the site effect term, $\log C_j$, when the conditions (2.3.5) and (2.3.6) are satisfied. These five parameters characterize station corrections for the ISC amplitudes for direct-P waves at teleseismic distances including the effects of the crust and the upper mantle. Figure 2.13 is an example of log-amplitude anomalies as a function of azimuth viewed from station to event. The solid curve and horizontal line are the least squares fit to the equation (2.4.1) and the constant term A_0 , respectively. The figures of log-amplitude anomalies as a function of azimuth for all station analyzed here are shown in Appendix A. Appendix B lists the resultant five parameters of azimuthal station corrections. The standard deviation before (sd_1) and after (sd_2) the fitting and the variance reduction, which indicates the goodness of fit, are also listed. The variance reduction (vr) is defined as

$$vr = \left[1 - \left(\frac{sd_2}{sd_1}\right)^2\right] \times 100 \qquad (\%) \tag{2.4.2}$$

Figure 2.14 shows the geographical distribution for the world of the A_0 , A_1 and A_2 terms in equation (2.4.1), and Figures 2.15, 2.16 and 2.17 are the expanded views of North America, Europe, and Asia-Oceania, respectively. The sizes of the symbols are proportional to the anomaly according to the indicated scale. The arrow points toward the largest-amplitude direction for A_1 , and the bar is parallel to the largest direction for A_2 . The azimuth-independent terms show similar pattern as the site effect terms shown in Figure 2.12. This indicates that the assumptions of the equations (2.3.5) and (2.3.6) are satisfied well. The

first-azimuthal terms have more complex distributions and do not show an obvious global tendency. This might be due to local effects around each station because the first azimuthal term reflects major structures in the crust and the upper mantle (Dziewonski and Anderson [1983]). The second-azimuthal terms, on the other hand, can be divided into characteristic regions, showing east-west directions, north-south directions, and complex distributions. The large-amplitude direction aligns in mainly an east-west direction around the western side of the Circum-Pacific zone. However, on the eastern side of the Pacific Ocean, such as the western part of North America, the large direction is parallel to the coast line. This suggests that deeper structure effects the second azimuthal term more than the first azimuthal term.

2.5 Travel time data analysis

The same analysis procedure was applied to the travel time data for comparison with the amplitude fluctuations. The relative travel time residuals were calculated using the AK135 velocity model and the ellipticity correction of Kennett and Gudmundsson [1996]. Then the station corrections for travel time and their azimuthal dependency were obtained by applying equations (2.3.7) and (2.4.1). For travel times, θ_1 and θ_2 denote the direction of latest phase arrival for the first and second azimuth-dependent terms, respectively. Figure 2.18 is an example of travel time anomalies as a function of azimuth viewed from station to event. Figures 2.19 and 2.20 show the spatial distribution of the site effect terms for travel time and the geographical distribution for the world of the terms of equation (2.4.1). Figures 2.21, 2.22 and 2.23 are the same maps as Figures 2.15, 2.16 and 2.17 but for travel time residuals. These results are generally consistent with Dziewonski and Anderson [1983], despite the fact that their data set is completely independent from the data of this study.

The azimuth-independent terms show almost the same pattern as the distribution of the site effect terms for amplitude, except for some faster stations in the Siberia and India regions and slower stations of Southeast Asia. This systematic distribution of travel time anomalies, the shields are fast and tectonically active regions are slow, was pointed out by Cleary and Hales [1966]. For the first azimuthal term, there is a tendency among the coastal stations for the slow direction to point toward the sea (for example east- and west coasts of North America, southeastern Asia, and South Africa). This is also pointed out by Dziewonski and Anderson [1983]. They suggested that this tendency might be associated with the relative slowness of the downdip propagation of the waves that encounter the thickening crust and possible depression of the upper mantle iso-velocity surfaces. On the other hand, the fast directions point opposite to the direction of the sea in Alaska. This area is characterized by the Pacific plate subducting toward the north beneath the North America plate (Zhao *et al.* [1995]). The larger amplitude (see Figure 2.15) and the faster arrivals from north might be caused by ray-guiding within the subducted high-velocity slab. The most striking feature in Europe is the cluster of the north-direction arrows in the central region. These are pointing away from the Alpine belt.

The second term of relative travel time residuals seems to have clusters of stations that show similar pattern. There is a great deal of regional consistency over a large part of North America. Most stations have NS slower directions in the western part of the United States, Canada and Alaska. In East Asia, in and around China and Japan, the dominant slower direction is E-W or WNW-ESE. The slower directions in these clusters and other stations are roughly consistent with the results of S-wave splitting analysis. It is easy to imagine that these second azimuthal terms correlate with the velocity anisotropy. Figure 2.24 has maps showing the faster split shear wave polarization directions from an ScS study (after Ando [1984]) and from SKS study (after Silver and Chan [1991]). If we assume the origin of the Pwave velocity anisotropy is same as that of the S-wave polarization, the second azimuthal dependency term for travel times should be orthogonal to the fastest direction of S-wave splitting. Comparing the second azimuthal term and shear-wave splitting, good agreements can be seen in some places, e.g. west and east coasts of North America, East Europe, and around China and Japan. For example, the slow directions of the second azimuthal term are roughly parallel with the direction of greatest principal compression in the United States (Zoback and Zoback [1980]). Seismic anisotropy represents dynamics of the Earth's interior, directly reflecting the instantaneous stress in the mantle (Kaneshima [1991]). Previously, analyses of shear-wave splitting have been the main method to determine the anisotropy. This work shows that an azimuthally dependent analysis of P-waves is also a useful tool to clarify the stress field in the Earth's interior.

2.6 Discussion

2.6.1 Correlation between amplitude and travel time

Lateral fluctuations of travel time residuals reflect lateral variations of velocity structure in the Earth's interior. On the other hand, amplitudes of seismic rays are affected by both velocity heterogeneity and attenuation structure. In general, regional low- and highvelocity anomalies cause focusing or defocusing of rays, in consequence ray amplitudes become larger or smaller, respectively. If larger travel time residuals and larger amplitude are observed at one station, it is possible that the large amplitude is caused by focusing of lowvelocity heterogeneity somewhere on the raypath, while early arrival and small amplitude indicate defocusing along the ray path. Therefore the positive correlations indicate that large amplitudes may be caused by focusing with low velocity anomalies. On the other hand, negative correlations between travel times and amplitudes can be caused by not only attenuation effects but also focusing effects by the low-velocity structure, when the lowvelocity body exists at deep position and the focus is not near the surface (Haddon and Husebye [1978], Ødegaard and Doornbos [1993]). Ødegaard and Doornbos [1993] investigated the NORSAR (Norwegian Seismic Array) data and found that there is a clear relation between large-amplitude arrivals tend to be late, but late arrivals do not necessarily have large amplitude. Figure 2.25 shows the spatial distribution of correlation coefficients between relative travel time residuals and log-amplitude anomalies at each station. There exist systematic clusters of negative correlation with early arrivals in southern Eurasia (western China and India) and late arrivals in the southern part of Southeast Asia (Malaysia, Singapore and Indonesia). This suggests that large amplitude observations are due to low attenuation in the crust and the upper mantle in southern Eurasia, while the high attenuation area or the deep low-velocity body may exists just beneath the southeastern Asia region. The other regions seem to have no systematics in general.

2.6.2 Crustal structure and amplitude

Amplitudes of seismic rays are affected by not only velocity and attenuation structure in the mantle but by crustal structure and local geology. I compare the log-amplitude anomalies to a new global model for the Earth's crust named CRUST5.1, presented by Mooney *et al.* [1998]. They constructed a global model which consists of 2,592 tiles on a 5° x 5° scale in which the crust and the uppermost mantle are described by eight layers: ice, water, soft sediment, hard sediment, crystalline upper crust, same type middle crust, same lower crust, and uppermost mantle. All of the tiles are classified into 14 primary crustal types. Figure 2.26 shows the primary crustal types showing P-wave velocities and the global distribution of the crustal types used to construct the model CRUST5.1 (Mooney *et al.* [1998]). The final classification has 139 structure types (84 continental, 26 oceanic, 23 shelf and six unique types for portions of the Red Sea, Black Sea and Caspian Depression) with differences in thickness, density, P- and S-wave velocities for each layer.

Figure 2.27 is a scatter diagram of the site effect term (equation (2.3.7)) for amplitude versus predicted site amplification from CRUST5.1. The predicted amplification factors, PP', were calculated by P-SV scattering matrix assuming vertical incident P-waves as

$$PP = 2^{n} \prod_{k=2}^{n} \left(\frac{\rho_{k} V p_{k}}{\rho_{k-1} V p_{k-1} + \rho_{k} V p_{k}} \right)$$
(2.6.1)

where n is the number of layers (from bottom to surface), ρ_k is the density at the k-th layer, and Vp_k is the P-wave velocity at the k-th layer (Aki and Richards [1980]). As shown in Figure 2.27, most of the stations are separated into three ranges of amplification., continental shell ($PP \sim 2$ to 3), active tectonic region ($PP \sim 4$) and islands ($PP \sim 6$ to 7). The site effect terms have large fluctuations with relation to the predicted site amplification, and there seems to be only a slight positive correlation. Figure 2.28 is a plot of the site effect terms for amplitude versus primary crustal types. There are some differences for each crust type. For example, station amplitudes are relatively small in Phanerozoic and forearc regions, while Platform and late Proterozoic regions have a tendency for larger amplitude observations. It seems that generally the old continents have relatively larger amplitudes, while active tectonic regions have smaller amplitude. Such tendencies can be seen in other teleseismic amplitude studies (e.g., Nakanishi and Motoya [1990], Negishi and Sato [1993]). The fluctuation of the site effect terms for amplitude, however, is so large that it cannot be explained by only the differences of the crustal type. This indicates that the site effect terms for amplitude are affected mainly by local effects, and the elastic structure of the crust and the uppermost mantle hardly affects them. Moreover, it is difficult to explain the fluctuations of site effect terms by the differences of the impedance beneath the seismometers, because the seismic observatory is seldom installed in the sedimentary place. The difference of the site effect term for amplitude may reflects much more local influences, such as local geology and instrumental origin.

Figure Captions

- Fig. 2.1 A page of the ISC printed book. The seismic database contains hypocentral parameters, source mechanism, phase-picking data, and disaster information. The main part of this page is about the 1995 Kobe Earthquake.
- Fig. 2.2 (a) WKBJ synthetic seismograms plotted as a function of epicentral distance.
 AK135 velocity model (Kennett *et al.* [1995]) was used. Only the time window around the direct P-phase was calculated. The source depth is 10 km.

(b) Amplitude variations of the figure (a) as a function of epicentral distances. Amplitude value is normalized by the source amplitude.

- Fig. 2.3 Map showing locations of 3,445 epicenters that occurred during the period from 1984 to 1995 used in this study. The location parameters of each event were taken from the relocated hypocenters data base named EHB (Engdahl *et al.* [1998]). The events that has more than 15 amplitude data were used. The minimum and maximum body-wave magnitude are 4.4 and 6.9.
- Fig. 2.4 Map showing locations of 718 stations used in this study. Totally 155,778 amplitude data observed these stations were used in this study.
- Fig. 2.5 AK135 one-dimensional Earth model (Kennett *et al.* [1995]) in the crust and mantle. P-wave velocity (thick solid lien) and density (thin solid line) structure of this model were used for the calculation of geometrical spreading and ray tracing. The effects of one-dimensional attenuation was not included in this study.
- Fig. 2.6 EHB epicenter relocation vectors relative to the ISC epicenters (after Engdahl *et al.* [1998]). The largest difference is over 30 km around the subduction region of the southwest Pacific, which corresponds to a arrival time difference of about 4 seconds.

- Fig. 2.7 Definition of the fault parameters and ray parameters used to obtain the radiation pattern. 3 fault parameters (strike, dip and rake angles) and 2 ray parameters (azimuth and emergent angle) are used for the source mechanism correction.
- Fig. 2.8 Radiation patterns for double-couple point source in a uniform medium. Left: 31 double couple force, mid: radiation pattern for P-waves, right: radiation pattern for S-waves. (after Kennett [1983]).
- Fig. 2.9 Geometries and coordinates that using for calculating the geometrical spreading $(R_0:$ the radius of the Earth, $\rho_0:$ the density at the surface, $V_0:$ the velocity at the surface, $\rho_s:$ the density at the hypocenter, $V_s:$ the velocity at the source, $\Delta:$ the angular epicentral distance, $\theta:$ the emergence angle measured from vertical, $i_0:$ the incident angle measure from vertical).
- Fig. 2.10 (a) (left) WKBJ seismograms using a non-attenuating AK135 model. Each trace was normalized by the maximum amplitude for all traces. (right) WKBJ seismograms using a AK135 model with attenuation shown in Fig. 2.5 (Montagner and Kennett [1996]). The difference of the amplitude variation between these figures cannot be seen. This indicates that the 1-D attenuation effect can be excluded if we analyze relative amplitude variations for each event.

(b) Amplitude variations of figures (a) as a function of epicentral distances. The absolute values of each amplitude are much different.

- Fig. 2.11 Examples of histogram of the relative log-scaled amplitude residual (referred to as log-amplitude anomaly) for each station (IMA: Indian Mountain, PMR: Paimer, SPA: South Pole, WRA: Warramunga, MAT: Matsushiro, MAI: Maizuru). The log-amplitude anomalies have a log-normal distribution.
- Fig. 2.12 Geographical distribution of the average log-amplitude anomalies (site effect terms). The size of the symbols is proportional to the anomaly according to the indicated scale. Circle and diamond indicate larger and smaller amplitude, respectively.

- Fig. 2.13 Log-amplitude anomaly fluctuation as a function of back azimuth viewed from station to event. The vertical axis is the common-logarithm of amplitude anomaly. Back azimuth is measured clockwise from North. Solid curve is the least-squares fit of equation (2.4.1). The horizontal line shows the constant term A₀. Vertical thin lines indicate one-sigma standard deviations for each 20 degrees azimuth window. The same figures for all station analyzed here are shown in Appendix A-1.
- Fig. 2.14 Geographical distribution of the terms A₀, A₁ and A₂ in equation (2.4.1). The size of the symbols are proportional to the anomaly according to the indicated scale. Circle and diamond indicate larger and smaller amplitude for A₀, respectively. The arrow points toward the largest direction for A₁, and the bar is parallel to the largest direction for A₂. These coefficients are listed in Appendix B-1.
- Fig. 2.15 Geographical distribution of the terms A_0 , A_1 and A_2 in equation (2.4.1) in North America. Other details are same as Fig. 2.14.
- Fig. 2.16 Geographical distribution of the terms A₀, A₁ and A₂ in equation (2.4.1) in Europe. Other details are same as Fig. 2.14.
- Fig. 2.17 Geographical distribution of the terms A₀, A₁ and A₂ in equation (2.4.1) in Asia-Oceania. Other details are same as Fig. 2.14.
- Fig. 2.18 Relative travel time residual fluctuation as a function of back azimuth viewed from station to event. The vertical axis is the relative travel time residual in second. The same figures for all station analyzed here are shown in Appendix A-2. Other details are same as Fig. 2.13.
- Fig. 2.19 Geographical distribution of the relative travel time residuals. Circle and diamond indicate late and early P-wave arrivals for A₀, respectively. The arrow points toward the latest arrival direction for A₁, and the bar is parallel to the latest

direction for A₂. These coefficients are listed in Appendix B-2. Other details are same as Fig. 2.12.

- Fig. 2.20 Geographical distribution of the terms A₀, A₁ and A₂ for the relative travel time residuals in equation (2.4.1) for the world. Other details area same as Fig. 2.12.
- Fig. 2.21 Geographical distribution of the terms A₀, A₁ and A₂ for the relative travel time residual in North America. Other details area same as Fig. 2.14.
- Fig. 2.22 Geographical distribution of the terms A₀, A₁ and A₂ for the relative travel time residual in Europe. Other details area same as Fig. 2.14.
- Fig. 2.23 Geographical distribution of the terms A₀, A₁ and A₂ for the relative travel time residual in Asia-Oceania. Other details area same as Fig. 2.14.
- Fig. 2.24 (upper) Map showing faster direction of shear wave splitting obtained from ScS (solid lines) study (after Ando [1984]). The length of the lines are proportional to the time difference between the two sprit waves. The dashed lines with a small code show the linear particle motions possibly representing no splitting of shear waves.

(lower) Faster shear wave splitting obtained from SKS analysis (after Silver and Chan [1991]). The bar is parallel to the fastest polarization directions, and the time difference between the split waves is indicated by the size of solid circle.

- Fig. 2.25 Geographical distribution of the correlation coefficients between the relative logamplitude anomaly and the relative travel time residual. Circle indicates positive correlation (larger amplitudes and late arrivals were observed) and diamond indicates negative correlation (large amplitudes and fast arrivals). The size of symbols are proportional to the correlation coefficients.
- Fig. 2.26 (upper) Crustal types used to construct the global crustal model CRUST5.1 (after Mooney *et al.* [1998]). Each crustal type has seven crustal layers. The crustal layers are ice, water, soft sediments, hard sediments, and the upper, middle and

lower crystalline crust. Only P-wave velocity is shown here, but the other parameters, such as S-wave velocity and density are also specified.

(lower) Global distributions of CRUST 5.1 types shown in the upper figure. The crustal structure in unmeasured regions has been extrapolated using statistical averages of regions of similar tectonic setting. (after Mooney *et al.* [1998])

- Fig. 2.27 Scatter diagram of the site effect term for amplitude station corrections (Averaged log-amplitude anomalies, equation (2.3.7)) versus the predicted site amplifications of CRUST5.1. The predicted amplifications were calculated by P-SV scattering matrix assuming vertical incident P-waves to each crustal structure type. Almost of the plots cam be divided to three ranges of the calculated site amplification, continental shell (~ 2.5), active tectonic region (~ 4) and islands (~ 6 to 7).
- Fig. 2.28 (upper) The site effect terms for amplitude versus the primary crustal types of CRUST5.1. Station amplitudes are relatively small in Phanerozoic and forearc regions, while Platform and late Proterozoic regions have a tendency for larger amplitude observations. The fluctuation of the site effect terms for amplitude, however, is so large that it cannot be explained by only the differences of the crustal type.

(lower) P-wave velocity structure of the primary types of CRUST5.1 (after Mooney *et al.* [1998]).
ASAR Alice Springs Ar. 84.53 221 P	18 54 47.4 (1.2) -0.9
ASPA Alice Springs 84.54 221 T/P BOB Boburget 84.55 254 P	18 54 48.3 (1.3) 0.0
BDI Bagni Di Lucca 84.56 352 P	18 54 48.1 +0.2
SFI Santa Sofia 84.58 351 P FIN Finale Ligure 84.61 353 P	18 54 50.2 +2.2
STV St Anna Valdieri 84.63 354 P	18 54 47.0 -1.3
PGD Poggio Sodo 84.64 351 P ENR Entracque 84.64 354 P	18 54 49.1 +0.8 18 54 46 9 -1.4
CRE Caprese Michel 84.86 351 P	18 54 50.7 +1.3
AUTH L'Aution 84.87 354 P	18 54 50.9 +1.4 18 54 50.9 +1.4
PII Pisa 84.90 352 P	18 54 49.6 0.0
IMI Imperia 84.93 354 P	18 54 48.7 -1.0
POO Poona 84.94 293 1/P AURE Auriera 84.99 354 D	18 54 49.0 (2.0) -1.4
MVIF Mont Vial 84.99 354 P	18 54 51.2 ÷1.1
SBF Sospel 85.00 354 eP REVF Reverse 85.13 354 P	18 54 50.9 +0.8 18 54 51 8 +1.0
CALN Calern 85.15 354 P	18 54 52.1 +1.2
CDR Cadarache 85.29 355 @P ASS Assisi 85.34 350 P	18 54 51.7 +0.1 18 54 52 0 +0.2
FRF La Foret Royale 85.36 355 eP	18 54 51.5 (1.5) -0.4
LRG Lorgues 85.48 355 eP VAY Valandovo 85.58 343 eP	18 54 53.2 (1.3) +0.7 18 54 54 0 -0 0
LMR La Mourre 85.59 355 eP	18 54 53.9 (1.6) +0.8
AQU l'Aquila 85.96 349 P MNS Montasola 86.01 350 P	18 54 57.1 +2.1
EPF Esparros 86.10 359 eP	18 54 55.8 (.8) +0.2
SDI San Donato 86.20 353 eP	18 54 56.7 (1.8) +0.6 18 54 57.6 -0.3
GBA Gauribidanur Ar. 86.70 288 P	18 54 57.0 -2.2
MGR Morigerati 87.88 347 P	.18 55 05.9 +1.8 18 55 04.1 -0.2
STKA Stephens Creek 89.13 211 T/P	18 55 10.8 (1.2) +0.3
BWA Boorowa 89.49 205 eP	18 55 13.2 +1.0
CAN Canberra 90.18 204 eP SDV Santo Domingo 95.46 69 eP	18 55 16.4 +1.0
SHRA Al Sharaya 99.21 322 LeP	18 55 58.0 +1.1
BGCA Bogoin 121.42 337 ePKP	18 56 02.3 +3.4 19 01 07.0
DBIC Dimbokro 122.22 5 ePKP	19 01 08.5 -0.7
KIC Kosan Boka 122.53 5 PKP	19 01 10.6 (7.1) +1.4
ITR Itaparica 127.59 50 ePKP	19 01 20.7 +1.1
BAO Brasilia Array 128.33 64 PKP	19 01 22.1 (3,1) +1.2 19 01 13.5 -7.4
VNDA Vanda 128.94 185 PKP	19 01 21.8 +1.2
VTY Vatovaky 130.36 292 PKP	19 01 27.8 (.7). +3.1
VDA Vodivohitra 130.69 293 PKP ABM Ambohimiarambe 131.01 292 PKP	19 01 28.7 +3.3
PTZ Petauke 134.92 313 T/PKP	19 01 36.0 +2.6
SPA South Pole 141 05 180 ePKP	19 01 49.0
BUL Bulawayo 141.31 312 PKP	19 01 46.3 (1.7) +1.4
BFT Belfast (SA) 145.29 306 J/PKP MAW Mawson 145.60 217 PKP	19 01 52.5 +0.9
POG Pongola 145.83 302 L/PKP	19 01 53.5 (2.3) +1.0
SLR Silverton 146.22 308 J/PKP SLR [.23um.0#8:1]	19 01 54.5 +1.3
KSR Koster 147.01 310 L/PKP	19 01 58.0 (2.1) +3.5
WIN Windhoek 148.16 327 ePKP	19 02 01.9 (2.3) 46.0 19 01 55.0 (2.3) -1.4
BLF Bloemfontein 150.04 307 J/PKP BOSA Boshof 150.10 200 T/PKP	19 02 05.7 (2.6) +6.4
FRS Fauresmith 151.00 308 T/PKP	19 02 06.7 (2.0) +5.3
HVD K Verwoerl Dam 151 61 one Trours	10 00 00 1
GRM Grahametown 153 18 201 UDVD	19 02 50.1 +48.5
GRM Grahamstown 153.18 301 J/PKP GRM [96nm,170:1]	19 02 50.1 +48.5 19 02 15.0 +11.3
GRM Grahamstown 153.18 301 J/PKP GRM [96nm,170:1] POF Poladder 153.19 317 J/PKP SYO Syowa Base 153.88 212 LePKP	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.1 19 02 12.3 +8.7
GRM Grahamstown 153.18 301 J/PKP GRM [96nm,1#0:1] POF Pofadder 153.18 317 J/PKP SYO Syowa Base 153.88 212 JePKP CER Ceres 156.87 313 J/PKP	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.1 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7
GRM Grahamstown 151.01 300 [JPKP GRM [96nm,180:1] POP Potadder SYO Syowa Base 153.18 301 JPKP SYO Syowa Base 153.18 212 JePKP CER Ceres 156.87 313 JPKP EIDC 16/18/142/m 2349, 6:66Nx73:19W,	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.1 19 02 15.0 +11.1 19 02 15.0 +16.7 19 01 14.0 (2.1) -54.7 h162km Mb4.3/3 -54.7 -54.7
GRM Grahamstown 13.01 3006 (JPKP GRM (Jachamstown 153.19 301 JPKP GRM (Jachamstown 153.19 317 JPKP SYO Syows Base 153.88 212 JepKP CER Ceres 156.87 313 J/PKP EIDC 16/ 16/ 42m 2349, 5:566/k-73119/W, ISC 16/ 16/ 42m 2349, 5:566/k-73119/W, ISC 16/ 16/ 42m 2349, 5:566/k-73119/W,	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.1 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mb4.3/3 73108₩21092,
GRM Grahamstown 151.01 300 (JPKP GRM [95nm, 160:1) POP Pofadder 153.19 317 LiPKP SYO Syows Base 153.88 212 LePKP CER Ceres 156.87 313 LiPKP EIDC 164 18h 42m 2349, 5:66N-73159V, ISC 164 18h 42m 2349, 5:66N-73159V, ISC 164 18h 42m 2349, 5:76N±1099- h161tms14km, n19, 01113/16, MB4 Colombia	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.3 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162 ^{km} Mbd.3/3 73:08₩±092, .5/4, 3C-4D, Northern
Certain and the second	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.3 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mb4.3/3 73'06W±'052, 5/4, 3C-4D, Northern
GRM Grahamstown 151.01 300 J/FKP GRM Grahamstown 153.19 301 J/FKP GRM J95mn, 190:11 POF Poladder 153.19 317 J/FKP SYO Syowa Base 153.88 212 JePKP CER Ceres 156.87 313 J/FKP EIDC 164 169 42m 2349, 5*66Nx73*19W, ISC 164 189 50m 4340, 4278Nx135*, Mbd Colombia ROM 164 169 50m 4340, 4278Nx13*15, Mbd ISC 164 189 50m 444*, 189, 4278Nx13*15, Mbd	19 02 15.0 +11.3 19 02 15.0 +11.3 19 02 15.0 +11.1 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mb4.3/3 73108W±7092, 54.4 3C-40, Northern 5km, Mb2.6 372E=±18, h5km, n5,
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GRM Grahamstown 131.01 300 (JPKP GRM Grahamstown 133.18 301 JPKP GRM (96nm, 160.1) POP Potadder 153.19 317 JPKP SY0 Syowe Base 153.88 212 JepKP SYO Syowe Base 153.88 212 JepKP SY0 Syowe Base 153.88 212 JepKP SY0 Syowe Base 153.88 212 JepKP EIDC 16/ 18h 42m 23+9, 6:66Nx.73:19W, ISC 166 18h 42m 22+142, 6:75Nx:109N-h161Km, 14km, n19, 01913/16, MbA Colombia SY0 16h 16h 56m 4340, 42*8Nx-13:15, https://doi.org/10.1000/11.5000000000000000000000000000	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.3 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 h162km, Mb4.3/3 73108W±'092, 5/4, 30-4D, Northern 5/m, Mb2.6 3*2E±'18, h5km, n5, 5. h0km, Mb4.6/4 , h3%m, o1461, Mb4.6/2,
GRM Grahamstown 151.01 300 J/FKP GRM Grahamstown 153.19 301 J/FKP GRM JS6m, 190.1] POP Foldeder 153.19 317 J/FKP SYO Syowa Base 153.82 312 JepKP CER Gerea 156.87 313 J/FKP EDC 164 19h 42m 23h, 6:r56N,731;9W, ISC 164 19h 43m 23h, 0;42;8N,713h, MB4 Colombia ROM 164 19h 55m 43h, 148, 42;8N,8:11,11 GOE 164 19h 55m 43h, 24;8N,8:11,11 GOE 164 19h 55m 50h, 51:13N,1792051 LIDC 164 19h 55m 50h, 51:13N,1792051 LIDS 164 19h 50m 51a, 147, 51:14a, 148,144	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.1 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mb4.3/3 73'08W2'092, 54.3 52-40, Northern 5km, M02.6 3*25±2*18, h5km, n5, 5. Nokm, Mb4.6/4 5. Nokm, Mb4.6/4 5. Nokm, m161, Mb4.6/2, 79*15±*13, h41km_15km,
GRM Grahamstown 131.01 300 J/FKP GRM Grahamstown 153.19 301 J/FKP GRM JBGnn, 190:11 POF Poladder 153.19 317 J/FKP SVO Syowa Base 153.19 317 J/FKP EIDC 16/16/16/2002 916, 5660/kr73:19/W, ISC 16/18/14/2002 916, 5660/kr73:19/W, ISC 16/18/14/2002 916, 5660/kr73:19/W, ISC 16/18/14/2002 917, 507 Amou 16/18/14/00 42/70/kr13:16, 104 Colombia ROM 16/18/50/00 42/20/kr13:16, 104 Colombia FIDC 16/18/150/00 42/20/kr13:16, 104 EIDC 16/18/150/00 50/2 511:37/kr179:052 FIDC 16/18/150/00 512/51137/kr179:052 Less reliable solution, ISC 16/18/150/00 512/5173/14/2/1541 n17, 01952/16, Mb4.1/4, Rat Island	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.1 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mbd.3/3 73108W±1092, 54.4 3C-40, Northern 5km, Mb2.6 32E±2:18, h5km, n5, 5. h0km, Mb4.6/4 5. h0km, Mb4.6/4 5. h0km, Mb4.6/4 5. h39m, 01461, Mb4.6/2, 79:1E±13, h41km±15km, is
GRM Grahamstown 131.01 300 J/FKP GRM Grahamstown 131.01 300 J/FKP GRM JBGrm, 160.11 POF Poladder 153.19 317 J/FKP SV0 Syowa Base 153.82 312 JepKP CER Ceres 156.87 313 J/FKP EIDC 16/16/142m 2349, 6:66/N:73*19W, ISC 16/18/142m 2349, 6:66/N:73*19W, ISC 16/18/142m 2349, 6:56/N:73*19W, ISC 16/18/142m 2349, 6:76/N:735*0, M16/16/16/16/144 Colombia ROM 16/16/56m 434-148, 42:80N:11x1 c0971/5, Central taly EIDC 16/16/59m 50/2 51:37N:178*132 Less reliable solution. ISC 16/18/59m 51:27, 51:31N:179*05L NEIC 16/18/59m 50:25:137N:178*131 Less reliable solution. ISC 16/18/59m 50:25:137N:14:15x1 n17, 01*52/16, Mb4:1/4, Rat Island JMA 16/19h 03m 03:32:0F6, 43:49N:204 M3.5, n31, Kurlf Islands	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.1 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mb4.3/3 73'08W±'092, 5/4, 3C-4D, Northern 5/m, Mb2.6 3'22E_a'18, h5km, n5, 2'22E_a'18, h5km, n5, 5, 33''m, 6161, Mb4.6/2, 78''1E_a'13, h41km_15km, 15 at 17'55E_a'05, h24km,
GRM Grahamstown 131.01 300 J/FKP GRM Grahamstown 131.01 300 J/FKP GRM (J66nn, 160.1) POF Poladder 153.19 317 J/FKP SV0 Syowa Base 153.82 312 JepKP CER Ceres 153.18 301 J/FKP EIDC 160 16h 42m 2349, 6:66N+73119W, ISC 166 16h 42m 2349, 6:66N+73119W, ISC 166 16h 50m 4349, 42:8N+73116, Mb4 Colombia ROM 160 16h 56m 4340, 42:8N+13116, Mb4 Colombia BCD 160 16h 56m 4349, 42:8N+13116, Mb4 Colombia BCD 160 16h 56m 4349, 42:8N+1316, Mb4 Colombia COV71/S, Central taly EIDC 160 16h 55m 4696, 51:13N+179:032 Less reliable solution. ISC 166 16h 59m 50:51:37N+179:032 Less reliable solution. ISC 166 16h 90 50m 0243:2066, 43:49N+204 M3.5, n31, Kurli talands IGO 160 19h 02m 0243:2066, 43:49N+204	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.1 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mb4.3/3 73'08W±'092, 5/4, 3C-4D, Northern 5km, Mb2.6 3*2E±2*18, h5km, n5, 5. h0km, Mb4.6/4 c, h39km, of 1661, Mb4.6/2, 79'15±13, h41km_15km, is x147:555±2*05, h24km, Dim Ado 2 2
GRM Grahamstown 131.01 300 J/PKP GRM Grahamstown 133.18 301 J/PKP GRM (j66nn, 160.1) POP Potadder 153.19 317 J/PKP SYO Syowa Base 153.18 301 J/PKP SYO Syowa Base 153.18 301 J/PKP EIDC 16/16/142/m 2349, 6:66/Nx73119/W, ISC 166 18/142/m 224-182, 6:75Nx12095- h1811/m, 144/m, 14/9, 01413/16, Mb4 Colombia ROM 16/18/56/m 4390, 42:80/x1311c, http://doi.org/11/5. ISC 166 18/16/56/m 4390, 42:80/x1311c, http://doi.org/11/5. ISC 166 18/16/56/m 4390, 42:80/x1311c, http://doi.org/11/5. FEIDC 16/18/56/m 4390, 42:80/x1311c, http://doi.org/11/5. ISC 166 18/16/56/5. 51:131Nx179:052/ NEIC 16/18/16/55 19/131Nx179:052/ NEIC 16/18/16/55 19/131Nx179:052/ NEIC 16/18/16/59/m 40:65, 51:131Nx179:052/ NEIC 16/18/16/50 m 03:73, 0:66, 43:48Nx104 M3.5, n31, Kuril Islands JMA 16/19/00 03:73,096, 43:49Nx:04 M3.5, n31, Kuril Islands IGO 16/19/13/m 21*11,115x78/22W, A33, 15C 164 19/13/22x=113, 11085x:058X	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.1 19 02 12.3 +8.7 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mb4.3/3 73'08Ws''092, 54.4 3C-4D, Northern 54.4 3C-4D, Northern 54.4 3C-4D, Northern 54.5 + 13. h5km, n5, 5. h0km, Mb4.6/4 5. h0km, d16.4 , Mb4.6/2, 79'112:13, h41km_15km, 15 *147:555±2.505, h24km, 94.7 78'12:14, h39km, n10,
 Carla amateum 131.01 300 [JPKP GRM (Js6nm, 160.1) GPOP Potadder 153.19 317 L/PKP SYO Syows Base 153.18 201 L/PKP SYO Syows Base 153.18 212 LepKP. CER Ceres 156.87 313 L/PKP EIDC 16/18/h 42m 23+9, 6:66Nx73*19W, ISC 16/18/h 42m 23+9, 6:66Nx73*19W, ISC 16/18/h 42m 23+9, 6:760Nx73*15H, h 16/14/h 16/h 5/m 43+0, 42*8Nx13*15H, ISC 16/18/h 56m 43+0, 42*8Nx13*15H, ISC 16/18/h 56m 43+0, 42*8Nx13*15H, ISC 16/18/h 56m 43+0, 42*8Nx13*15H, ISC 16/18/h 56m 43+0, 5:113/Nx179*13H, NEIC 16/18/h 56m 43+0, 5:113/Nx179*13H, NEIC 16/18/h 56m 43+0, 5:113/Nx179*13H, Less reliable solution. ISC 16/18/h 50m 51+2:147, 51*2Nx2*15H, 1n17, 01*52/15, Mbx114, Rat Lalanc JMA 16/19/h 03m 03+32+046, 43*49Nx*04 M3.5, n31, Kuril Islands IGO 16/19/h 13m 22+131, 11*55x76*2W, n33. ISC 16/19/h 13m 22+131, 11*55x76*2W, n33. 	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.1 19 02 12.3 +8.7 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mb4.3/3 73108W±*092, .5/4, 3C-4D, Northern Skm, Mo2.6 3*2E±*18, h5km, n5, . h0km, Mb4.6/4 . h38m, o1461, Mb4.6/2, 79*1E±*13, h41km±15km, is x147*55E±*05, h24km, pkm, Mo3.2 78*1W±*14, h39km, n10,
GRM Grahamstown 151.01 300 J/FKP GRM Grahamstown 151.01 300 J/FKP GRM JS6nn, 160:11 POP Foldeder 153.19 317 J/FKP SYO Syowa Base 153.88 211 JepKP CER Cares 156.18 313 J/FKP EIOC 164 169 42m 239, 6:66Av.731:9W, ISC 164 169 42m 239, 6:766Av.731:9W, ISC 164 169 42m 239, 6:766Av.731:9W, ISC 164 169 4390, 42:8W-131:16, Mbd Colombia POM 164 169 55m 4390, 42:8W-131:16, Mbd Colombia ISC 164 169 55m 4390, 42:8W-131:16, Mbd Colombia ISC 164 169 55m 4390, 42:8W-131:16, Mbd Colombia ISC 164 169 55m 4390, 42:8W-131:17, 17:132 LICS 164 169 55m 50%, 51:137N-179:132 LICS 164 169 55m 50%, 51:13N-179:132 LICS 164 169 55m 50%, 51:13N-179:132 LICS 164 169 55m 60%, 51:13N-179:132 LICS 164 169 55m 60%, 51:13N-179:132 LICS 164 169 50m 160; 50% 60%, 51:37N+179:132 LICS 164 169 100 2007, 14:32/16, Mbd-114, Rat Islands ISC 164 169 100 2007, 17:14 Islands ISC 164 169 100 207, 17:15, 2008-2005 C0160 169 109 100 2141, 11:15, 11098-20505	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.3 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mbd.3/3 73'08Wa'062.6
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GRM Grahamstown 131.01 300 //FKP GRM Grahamstown 131.01 300 //FKP GRM (j66m, 160.1) POF Poladder 153.19 317 //FKP SVO Syowa Base 153.89 317 //FKP SVO Syowa Base 153.88 211 //FKP EIDC 16/16/16/207 2349, 6:560N:73119W, ISC 16/18/142m 224:142, 6:770N:2059- h1511m, 144m, n149, 0113316, Mb4 Colombia ROM 16/16/50m 4390, 42:80N:13116, Mb4 Colombia ROM 16/16/50m 4390, 42:80N:1316, Mb4 Colombia ROM 16/16/50m 4390, 42:80N:1316, Mb4 Colombia Colombia Bib 50m 444-118, 42:80N:1316, Mb4 Colombia SC 16/16/50m 509, 51:37N:179:05L Less reliable solution. ISC 16/18/50m 4342, 014, 43:484.15x1 ISC 16/18/50m 0343,2006, 43:49N-204 MA 16/19/03m 0343,2006, 43:49N-204 MA 16/19/13m 0241,115x1 ISC 16/19/13m 0241,115x1 ISC 16/19/13m 0241,115x1 ISC 16/19/13m 0241,115x1 ISC 16/19/13m 0247,175:20N-123:768 CO 16/10/13-1202,114,1148-148 ISC 16/19/13m 0247,175:20N-123:768 Less reliable soluti	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.1 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 h162km, Mbd.3/3 73'08W±'092, 5/4, 3C-4D, Northern 5/m, Mb2.6 372'E±18, h5km, n5, 5/m, Mb3.6/4 5, n39m, o1461, Mb4.6/2, 79'1'E±'13, h41km±15km, 15 16, n39m, o1461, Mb4.6/2, 79'1'E±'13, h41km±15km, 15 17'1'W±'14, h39km, n10, , h10km, o0672, Mb4.5/20, , n0km, Mb4.4/5 91x1237E±41, h10km, 01 Savema 2 Samture
 Christmatter, 13.10, 13.00, 1/FKP GRM (js6m, 160.1) GRM Grahamstown 153.19, 301 /JFKP GRM (js6m, 160.1) POP Potadder, 153.19, 317 /JFKP SYO Syowa Base, 153.88, 212 / ΔρFKP CER Ceres, 156.87, 313 /JFKP EIDC 16/18/h 42m 2349, 6:66/h,r3:19/W, ISC 166 18/h 42m 2349, 6:66/h,r3:19/W, ISC 166 18/h 42m 2349, 6:76/h,r3:16, Ihd Colombia ROM 16/18/h 56m 4340, 42:80/h,13:16, Ihd Colombia EIDC 16/18/h 56m 4340, 42:80/h,13:16, Ihd Less reliable solution. ISC 16/18/h 59m 50:55, 51:37/N,179:05L Less reliable solution. ISC 16/18/h 30m 03432046, 43:49Na;104 M3.5, n31, Kurli Islande ISC 16/18/h 30m 03432046, 43:49Na;104 M3.5, n31, Kurli Islande ISC 16/19/h 20m 2347, 79:20N,123:756E Less reliable solution. EIDC 16/19/h 20m 2347, 79:20N,123:7576 Less reliable solution. EIDC 16/19/h 20m 2347, 79:20N,123:7576 Less reliable solution. EIDC 16/19/h 20m 2347, 79:20N,123:7576 Less reliable solution. EIDC 16/19/h 20m 2347, 79:20N,123:7576 ISC 16/h 20m 2347, 79:20N,123:7576 ISC 16/h 20m 2347, 79:20N,123:7576 ISC 16/h 20m 2347, 79:20N,123:7576 	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.1 19 02 12.3 +8.7 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mb4.3/3 73'08Wa''092, 5/4, 3C-4D, Northern 5km, Mb2.6 5th, Mb4.6/4 5, h39km, of 161, Mb4.6/2, 79'154:13, h41km_15km, is x147'5554:05, h24km, 78'11Wa''14, h39km, n10, 5, h0km, of 72, Mb4.5/20, 5, h0km, db4.4/5, h10km, of Severnaya Zemiya
 Christian Bell, 191, 201, 2010, JFRCP GRM. (JsGnm, 180:1) GRM. Grahamstown 153, 18 301 JFRCP GRM. (JsGnm, 180:1) POP Potadder 153, 19 317 J. (JPKCP SYO Syows Base 153, 38 212 J. 24 PKC CER. Ceres 156, 187 313 J. (JPKCP SYO Syows Base 153, 38 212 J. 24 PKC CER. Ceres 156, 193, 212 J. 24 PKC CER. Ceres 156, 193, 214, 214, 214, 214, 214, 214, 214, 214	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.1 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mbd.323 73108W.2092, 5.4, 3C-40, Northern 5km, Mb2.6 3*2E_±18, h5km, n5, 5. h0km, Mb4.6/4 5. h0km, Mb4.6/4 5. h0km, Mb4.6/4 5. h0km, Mb4.6/2 78*1E_±13, h41km_15km, 147*55E_±05, h24km, 5. h0km, d04.5/20, . h0km, Mb4.4/5 91*12378E_±1, h10km, of Severnaya Zemiya h10km, d0499, Single
 Carla and Semi 13-101 300 [JFKP GRM Grahamstown 13-101 300 [JFKP GRM (J66m, 160:1) GPOF Polader 153.19 317 J.PKP SYO Syowa Base 153.88 213 J.epKP SYO Syowa Base 153.88 213 J.epKP EIDC 164 169 42m 23r9, 6:560 J.epKP ISC 164 189 56m 43r4, 188, 42:80 J.ext ISC 164 189 56m 43r4, 188, 42:80 J.ext ISC 164 189 56m 43r4, 189, 42:80 J.ext ISC 164 189 56m 50r42, 51:37N-179:051 Less reliable solution. JSC 164 189 56m 50r42, 51:37N-179:051 Less reliable solution. JSC 164 189 56m 303r2.066, 43:48N ±:04 M3.5, n31, Kurll Islands IGC 164 199 13m 21r1, 1:15x78:2W, h33 ISC 164 199 13m 22ra, 1v3, 1:0953:0054 .co58:001, 3C-20, Ecuador NEIC 164 199 20m 2397, 79:20N-123:756 Less reliable solution. IEC 164 19n 20m 2397, 79:24N-123:37E ISC 164 19n 20m 2397, 79:24N-123:37E	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.1 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mb4.3/3 73108W±7092, 54.3 52.40, Northern 5km, Mb2.6 372E_±718, h5km, n5, 5. h0km, Mb4.6/4 5. h0km, Mb4.6/4 5. h0km, Mb4.6/4 7871E_±714, h39km, n10, 5. h0km, mb4.4/5 91x1237E_±741, h10km, 01 Severnaya Zemlya h10km, o0#99, Single h15km
 Carl Anamatown 131-01 300 [JFKP GRM Grahamatown 153.19 301 JFKP GRM [96m, 1907] GRM Grahamatown 153.19 317 JFKP GPOF Poladier 153.19 317 JFKP SYO Syowa Base 153.88 211 JePKP SYO Syowa Base 153.88 211 JePKP EIDC 164 16h 42m 234.9, 6766/Nr73*19W, ISC 164 16h 42m 234.9, 6766/Nr73*19W, ISC 164 16h 42m 234.9, 6778.Nr 2098- h1611ms, 144m, n14, 0 4113/16, Mod Colombia ROM 164 16h 55m 4340, 4228Nr 113:1 oOP71/5, Central Italy EIDC 164 16h 55m 4646, 51113Nr 179:05L NEIC 164 18h 55m 4646, 51113Nr 179:05L NEIC 164 18h 55m 502, 51137Nr 179:134 Less reliable solution. ISC 166 18h 55m 514-187, 5114Nr 179:05L 165 164 18h 30m 3032-006, 43249Nr 304 M3.5, 731, Kurll Islands IGO 164 19h 13m 2141, 115S-762W, A3 ISC 164 19h 20m 2347, 79720Nr 30 Co 16710, 35-20, Ecuador NEIC 164 19h 20m 2347, 79720Nr 123:37E ISC 164 19h 20m 2347, 79720Nr 123:37E ISC 164 19h 20m 2347, 79720Nr 123:37E ISC 164 19h 21m 3249, 3255S-71:67W, network solution. NEIC 164 19h 21m 334, 3255S-71:67W, ISC 164 19h 21m 334, 3255S-71:67W, 	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.1 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 15 01 14.0 (2.1) -54.7 16 01 14.0 (2.1) -54.7 17 10 14.0 (2.1) -54.7 16 01 14.0 (2.1) -54.7 17 10 14.0 (2.1) -54.7 16 01 14.0 (2.1) -54.7 17 10 14.0 (2.1) -54.7 18 14.0 (2.1) -54.7 1
 Carl Animettown 131-01 3000 [JFKP GRM Grahamatown 131-01 3000 [JFKP GRM [96m, 190:1] GRM Grahamatown 153.19 301 JFKP GRM [96m, 190:1] POF Poladder 153.19 317 JFKP SYO Syowa Base 153.88 212 JepKP SYO Syowa Base 153.88 212 JepKP EIDC 16/18h 42m 2349, 6:560N,73119W, ISC 16/18h 56m 4349, 42:80N,13116, Mod Colombia ROM 16/18h 56m 4349, 42:80N,13116, Mod Colombia ROM 16/18h 56m 444-1184, 42:80N,13116, Mod Colombia GO 16/18h 56m 444-1184, 42:80N,13116, Mod Colombia EIDC 16/18h 56m 444-1184, 42:80N,131178/132 Less reliable solution. ISC 164 18h 56m 444-1184, 42:80N,132/154 In17, 01+52/16, Mbd.114, Rat Island MA 16/18h 02m 03432066, 43:49N-304 M3.5, n31, Kuril Islands ISC 164 19h 30m 2347, 79:20N,123/156 Less reliable solution. ISC 164 19h 20m 2347, 29:2355, 71:68W, Nelwork solution. ISC 164 19h 21m 334, 32:555, 71:68W, Nelwork solution. ISC 164 19h 21m 334, 32:555, 71:68W, Nelwork solution. ISC 164 19h 21m 334, 32:555, 71:68W, NelWork 11, Near coast of Central Cl ISC 164 19h 21m 334, 24:352, 71:68W, NelWork 11, Near coast of Central Cl 	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.1 19 02 12.3 +8.7 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mb4.3/3 73'08W±'092, 5/4, 3C-4D, Northern 5/4, 3C-4D, Northern 5/m, Mb2.6 3/22E_2'18, h5km, n5, 5/m, Mb4.6/4 5, n0km, Mb4.6/4 5, n0km, d18, h41km_15km, 18 147'55E_2'05, h24km, 19 172'5E_2'13, h41km_15km, 18 147'55E_2'05, h24km, 19 1123'26E_2'41, h10km, 01 Severnaya Zemlya h10km, d0999, Single h15km 177'W±26, h10km, n11, 116
 Charles and States and States	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.1 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mb4.3/3 73108W.2092, 54.3 C-40, Northern 5km, Mb2.6 5:252±2:18, h5km, n5, 5: h0km, Mb4.6/4 5: h3%m, d1461, Mb4.6/2, 78:12±2:13, h41km_15km, 15 147:555±2:05, h24km, 147:555±2:05, h24km, 16 17 Ma3.2 78:1W±114, h39km, n10, 5: h10km, d0#92, Single h10km, d0#93, Single h10km, d0#94, Single Sing
 Carl Andream Semi 13-101 300 [JFKP GRM Grahamstown 13-101 300 [JFKP GRM [96nn; 10:1] GRM Grahamstown 153.19 317 [JFKP OPP Foldeder 153.19 317 JFKP SYD Syowa Base 153.88 211 [46]FKP SYD Syowa Base 153.88 211 [46]FKP IDC 164 169 4300 [42:80k-131:16, Mb4 Colombia ROM 164 169 550 40:60, 511 [30k-137]FKP IDC 164 169 550 40:60, 511 [30k-137]FKP IDC 164 169 550 40:60, 511 [30k-179] [30k- IDC 164 169 500 40:60, 511 [30k-179] [30k- IDC 164 169 500 40:50, 513 [30k-179] [30k- IDC 164 169 10] [30k-206, 43:49N-104] MAI 164 169 10] [30k-216, Mat Islands IDC 164 169 10] [30k-216, Mat Islands IDC 164 169 10] [30k-216, Mat Islands IDC 164 169 10] [30k-228, 103, 1109S-1068] [SC 164 169 10] [30k-228, 104, 105S-1068] [SC 164 169 10] [30k-228, 104, 107, 105S-1058] [SC 164 169 10] [30k-228, 104, 107, 105S-1058] [SC 164 169 10] [30k-228, 104, 227558, 11577] [SC 164 169 10] [30k-228, 104, 107, 105S-10577] [SC 164 169 10] [30k-228, 104, 107, 10578-10] [SC 164 169 10] [30k-228, 104, 107, 10578-10] [19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.3 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 10 54.7 (3.4) (3.4) 11 555 (3.4) (3.4) 12 54.7 (1.6) (1.6) 14 7155 (2.5) (2.4) 10 54.7 (3.4) (3.4) 11 70 57 (2.1) (3.4) 12 74.1 (1.6) (1.6) 14 7155 (2.1) (3.4) 14 7155 (3.4) (3.4) 10
 Carla and Semi 13-101 300 [JFKP GRM Grahamstown 13-101 300 [JFKP GRM (J66m, 160:1) GRM Grahamstown 153.19 301 JFKP GRM (J66m, 160:1) FOP Foldeder 153.19 317 JFKP SYO Syowa Base 153.88 213 JePKP SYO Syowa Base 153.88 213 JePKP SYO Syowa Base 153.88 213 JePKP ELDC 164 16h 42m 23+9, 5:66Nx73:19W, ISC 164 18h 42m 23+9, 5:76Nx1098- h1611m, 144m, 181, 0;1813116, M64 Colombia ROM 164 16h 55m 43+2184, 42:80x+11x1 d0V7175, Central Raly ELDC 164 18h 55m 44+2;184, 42:80x+11x1 d0V7175, Central Raly ELDC 164 18h 55m 44+2;184, 42:80x+11x1 d0V7175, Central Raly ELDC 164 19h 55m 50x 51:13Nx.179:05L Less reliable solution. ISC 164 18h 55m 51+2;17, 51:14x-115x1 n17, 01*52176, M64;144, Rat Islande IGO 164 19h 13m 22x+133, 1:1085x:058x- d0980(10), SC-20, Ecuador NEIC 164 19h 20m 2397, 79:20Nx123:37E Less reliable solution. IEDC 164 19h 21m 32e, 32:55Sx:14:57T, network solution. IEDC 164 19h 21m 32e, 32:35Sx:11:67W, network reliable solution. IEDC 164 19h 22m 2741, 44:77Nx6:72E, h LDG 164 19h 23m 2741, 44:77Nx6:72E, h 	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.1 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 15 02 12.3 15 02 1
 Christmattown 131-01 300 [JFKP GRM Grahamstown 131-01 300 [JFKP GRM [96m, 160:1] GRM Grahamstown 153.19 301 JFKP GPOF Poladier 153.19 317 JFKP SYO Syowa Base 153.88 211 JePKP SYO Syowa Base 153.88 211 JePKP EIDC 16/16/16/42m 2349, 6:560Nx73:19W, ISC 16/16/16/42m 2349, 6:560Nx73:19W, ISC 16/16/16/50m 4390, 42:80Nx13:15, Int Colombia ROM 16/16/16/50m 4390, 42:80Nx13:15, Int GPT1/5, Central Italy EIDC 16/16/16/50m 4502, 51:137Nx179:05L NEIC 16/16/16/50m 5022, 51:137Nx179:05L NEIC 16/16/16/50m 502, 51:137Nx179:05L NEIC 16/16/16/50m 502, 51:137Nx179:05L Less reliable solution. ISC 16/18/90m 33420H6, 43:49Nx:04 M335, n31, Kurli Italands IGO 16/19/13/m 2141, 1:15x78:2W, N3; ISC 16/19/13/m 2141, 1:15x78:2W, N3; ISC 16/19/13/m 2141, 1:15x78:2W, N3; ISC 16/19/13/m 2141, 1:15x78:2W, N3; ISC 16/19/13/m 2141, 2:15x78:2W, N3; ISC 16/19/13/m 2147, 79:20Nx:00 n27, 0:0487/27, Mb4.5/20, 1C, East NEIC 16/19/20/m 2397, 79:20Nx123:756 Less reliable solution. NEIC 16/19/20/m 2397, 79:20Nx123:756W, ISC 16/19/21/m 3346, 32:555X71;67W, network solution. NEIC 16/19/21/m 3346, 32:555X71;67W, ISC 16/19/22m 274, 44/30Nc54E, 70 ISC 16/19/22m 274, 44/30Nc54E, 70 ISC 16/19/22m 274, 44/30Nc54E, 70 ISC 16/19/22m 274, 44/30Nc54E, 70 ISC 16/19/22m 274, 54, 54, 550, 752, 750, 752, 750, 72, 74, 750, 750, 752, 74, 750, 752, 74, 750, 752, 74, 750, 752, 74, 750, 752, 74, 750, 752, 74, 750, 752, 74, 750, 752, 74, 750, 750, 74, 740, 750, 745, 750, 745, 740, 750, 747, 740, 750, 746, 746, 750, 747, 740, 750, 746, 750, 747, 740, 750, 746, 740, 740, 740, 740, 740, 740, 750, 740, 740, 740, 740, 740, 740, 740, 750, 740, 740, 740, 740, 740, 740, 740, 74	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.3 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 10 01.2 17 01.0 (2.1) -54.7 10 01.2 17 02 12.3 1.5 0.7 1.5
 Carl Animettown 131-01 3000 [JFKP GRM Grahamstown 131-01 3000 [JFKP GRM [96m, 190:1] GRM Grahamstown 153.19 301 JFKP GRM [96m, 190:1] SVO Syowa Base 153.88 211 JepKP SVO Syowa Base 153.88 211 JepKP EIDC 16/16/16/42m 2349, 6:560N+73:19W, ISC 16/16/16/42m 2349, 6:560N+73:19W, ISC 16/16/16/50m 4340, 42:80N+73:15, https://doi.org/10.1001	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.3 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mb4.3/3 73'08W±'092, 5/4, 3C-4D, Northern 5/4, 3C-4D, Northern 5/4, 3C-4D, Northern 5/m, Mb2.6 3/22E_2'18, h5km, n5, 5/m, Mb4.6/4 5, n0km, Mb4.6/4 5, n0km, Mb4.6/4 5, n0km, Mb4.6/2 78'1W±'14, h39km, n10, 5/n0km, d09.72, Mb4.5/20, 10km, d09.99, Single h10km, d09.99, Single h10km, d09.93, kg2.4(GEN). m, Mb2.2 30x8'89E_2'090, h5km, 11:0E±.728, h49km, n5,
 Carl Anamatown 151.01 300 [JFKP GRM Grahamatown 151.01 300 [JFKP GRM [95m, 160.1] GRM Grahamatown 153.19 317 [JFKP GPOF Poladier 153.19 317 JFKP SYD Sydowa Base 153.88 211 [46]FKP SYD Sydowa Base 153.88 211 [46]FKP ISC 164 169 42m 23#, 6756M-73719W, ISC 164 169 42m 23#, 6756M-73719W, ISC 164 169 45m 43#, 188, 4238M-211x1 order1715, Central haly EIDC 164 169 55m 43#, 189, 4238M-211x1 order1715, Central haly EIDC 164 169 55m 50F2, 5113M-175138 Less reliable solvion. ISC 164 169 55m 50F2, 5113M-175138 Less reliable solvion. ISC 164 169 55m 50F2, 5113M-175138 Less reliable solvion. ISC 164 169 50m 51#, 187, 514M-215.41 n17, o1#52/16, Mb4.1/4, Rat Island MA 164 19h 02m 0273.2066, 43749M-204 M3.5, n31, Kurli Islands ISC 164 19h 20m 23#7, 79:20M-123726 Less reliable solvion. EIDC 167 19h 20m 23#3, 432585, 57:1567W, network solvion. EIDC 167 19h 20m 23#3, 432585, 71:567W, network solvion. EIDC 167 19h 22m 2714, 4477M-6778E, he ISC 164 19h 23m 7544, 4475M-6784, h	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.3 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mb4.323 73708W, 47092, 54.3 3C-40, Northern 5km, Mb2.6 3*25±18, h5km, n5, 5. h0km, Mb4.6/4 5. h0km, Mb4.6/4 5. h0km, d1461, Mb4.6/2, 78*15±13, h41km_15km, 15 m, Mb2.2 78*1W±14, h39km, n10, 78*1W±14, h39km, n10, 78*255, h10km, o0\$*99, Single h15km 177W±26, h10km, n11, hie 5km, o0\$*99, single h15km 177W±26, h10km, n5, 147*285±04, h52km
GRM Grahamstown 151.01 300 J/FKP GRM Grahamstown 151.01 300 J/FKP GRM Grahamstown 153.19 317 J/FKP GRM Grahamstown 153.19 317 J/FKP GRM Grahamstown 153.19 317 J/FKP SYO Syowa Base 153.88 201 J/FKP SYO Syowa Base 153.88 201 J/FKP EIOC 164 16h 42m 23h, 6:66Av.73:19W, ISC 164 16h 43m 22h, 6:76Av.73:19W, ISC 164 16h 43m 22h, 6:76Av.73:19W, ISC 164 16h 56m 44h, 149, 0:113116, Mbd Colombia ROM 164 16h 55m 40h, 149, 0:113116, Mbd Colombia ROM 164 16h 55m 40h, 149, 0:113116, Mbd Colombia ISC 164 16h 56m 44h, 149, 0:113116, Mbd Colombia ROM 164 16h 55m 40h, 214, 137147, 137152 EIOC 164 16h 55m 40h, 214, 173174, 137151 EIOC 164 16h 55m 40h, 214, 175, 174179:152 EIOC 164 16h 55m 40h, 214, 175, 174179:152 EIOC 164 16h 55m 40h, 214, 174, 184 Islands ISC 164 18h 19m 23t1, 1;15, 1541, 12082;0563, 153, 1548, 21545, 101, 0:1182;056, 152, 1542, 103, 10982;0563 ISC 164 18h 13m 23t2, 145, 110982;0563, 150;056, 150, 150;056, 150, 100, 102, 0:20, Eculador ISC 164 19h 12m 23h, 214, 177, 1572,	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.3 19 02 15.0 +11.3 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 14.0 (2.1) -54.7 15 37252±2:18, h5km, n5, -54.7 15 392m, o1461, MD4.6/2, -79:112:112, h3km, n10, 5 4.13252±2:05, h24km, -90.7 5 4.147:1555±2:05, h24km, n10, -78:114, h39km, n10, 5 4.1232±2:134, h41km±15km, -10, 5 78:1104.1, h39km, n10, -78:112312±2:41, h10, 5 79:1232±2:141, h10, h32km, -10, 1 10 52:015, h02, h24, h32km, -11, 11e -58m, o0493, A82.4(GEN). 0 50:65792±2:090, h5km, -11, 11:0 <td< td=""></td<>
 Carla amatemi 13-101 300 [JFKP GRM Grahamatewn 13-101 300 [JFKP GRM [96m, 160:1] GRM Grahamatewn 153.19 317 J.PKP GRM [96m, 160:1] FOP Foldeder 153.19 317 J.PKP SYO Syowa Base 153.88 213 JapKP EUC 164 16h 42m 23+9, 5:66Nx73:19W, ISC 164 18h 42m 23+9, 5:66Nx73:19W, ISC 164 18h 42m 23+9, 5:75Nx1709- h1611m, 14km, n19, 0113116, Mb4 Colombia ROM 164 16h 56m 44+2, 184, 42:80x+11x1 d0V7175, Central Raly EUC 164 18h 56m 44+2, 184, 42:80x+11x1 d0V7175, Central Raly EUC 164 18h 56m 44+2, 184, 42:80x+11x1 d0V7175, Central Raly EUC 164 18h 56m 44+2, 184, 3:280x+11x1 d0V7175, Central Raly EUC 164 18h 56m 44+2, 184, 3:280x+11x1 d0V7175, Central Raly EUC 164 18h 59m 51+2, 17; 371x1x-115x1 n17, 01*52/15, Mb4,174, Rat Island ISC 164 18h 19h 03m 0393-066, 43:49Nx:04 M3.5, n31, Kurll Islande IGO 164 19h 13m 21x1, 115x7572W, h33 ISC 164 19h 13m 21x1, 115x7572W, h33 ISC 164 19h 13m 22x, 193, 11095x:069x d0V6101, 3:C-20, Ecuador NEIC 164 19h 20m 2397, 79:20Nx123:37E ISC 164 19h 20m 274, 44'70Nx637E, h LDG 104 19h 20m 274-335, 34'55Nx255, 34'55Nx151x1 c0443/5, 014 ast coast coast coast coast coast 104 19h 20m 274-335, 34'55Nx151x1 c0443/5, 014 ast coast coast coast coast 104 19h 20m 274-335, 34'55Nx151x1 c0443/5, 014 ast coast coast coast cof 100xh J	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.1 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 15 02 12.3 14.3 C-40.1 Northern 54.3 C-40.1 Northern 55. Northern 14.1 C-40.1 Northern 15. North, and 15. 14.1 C-40.1 Northern 15. North, and 10. 14.1 C-40.1 Northern 15. Northern 14.1 C-40.1 Northern 15. Northern 14.1 C-20.3 Ads/mm 15. Northern 15. Northern 14.1 C-20.3 Ads/mm 15. Northern 15. North
 Charlane toem 131-01 300 [JFKP GRM Grahamstown 153.19 301 JFKP GRM [96m, 160:1] GRM Grahamstown 153.19 317 JFKP GPOF Poladier 153.19 317 JFKP SYO Syows Base 153.88 211 JePKP SYO Syows Base 153.88 211 JePKP EIDC 16/16/16/42m 2349, 6:560Nx73:19W, ISC 16/16/16/42m 2349, 6:560Nx73:19W, ISC 16/16/16/50m 4390, 42:80Nx13:15, htt Colombia ROM 16/16/50m 4390, 42:80Nx13:15, htt Colombia ROM 16/16/50m 4390, 42:80Nx13:15, htt Colombia EIDC 16/16/50m 4390, 42:80Nx13:15, htt Colombia EIDC 16/16/50m 4502, 51:137Nx179:05L HEIC 16/16/50m 502, 51:137Nx179:05L HEIC 16/16/50m 502, 51:137Nx179:05L Less reliable solution. ISC 16/18/50m 03:43:046, 43:48Nx:04 M3.5, n31, Kurli Islands IGO 16/19/19/19/277, 79:20Nx123:756 Less reliable solution. IEC 16/19/20m 2347, 79:20Nx123:756 Less reliable solution. IEC 16/19/21m 2349, 32:555x.71:67W, network solution. IEC 16/19/21m 2349, 32:555x.71:67W, NEIC 16/19/21m 2344, 32:555, 34:	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.3 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mbd.3/3 73108W±1092, 54.3 32-40, Northern 5km, Mb2.6 372E.s.18, h5km, n5, 5. h0km, Mb4.6/4 5. h0km, Mb4.6/4 5. h0km, Mb4.6/4 5. h0km, Mb4.6/4 78:11W.s.114, h39km, n10, 5. h10km, c0#72, Mb4.5/20, 5. h0km, Mb4.4/5 91x12378E.s'41, h10km, of Severnaya Zemlya h10km, c0#99, Single h15km 177W.s26, h10km, n11, nle 5km, c0#93, kg2.4(GEN), m, M.2.2 30x659E.s:090, h5km, 1110E.s'28, h49km, n5, 1147:28E.s'04, h52km, h5km, c0#42, Single h5km
 Carl Andrew Bell 131.01 300 [JFKP GRM Grahamstown 131.01 300 [JFKP GRM [96m, 1901] GRM Grahamstown 153.19 317 J.PKP POF Poladier 153.19 317 J.PKP SYO Syowa Base 153.88 212 J.epFKP SYO Syowa Base 153.88 212 J.epFKP EIDC 16/16/16/950/04.2780,47311.91/ ISC 16/16/16/50m 4390,42280,41311, oOP71/5, Central Italy EIDC 16/16/50m 4645,51113N,179055 EIDC 16/16/50m 4645,51113N,179055 EIDC 16/16/50m 4645,51113N,179055 EIDC 16/16/50m 4645,51113N,179055 EIDC 16/16/50m 4034,2006,43240H,2131 Less reliable solution. ISC 164 18/50m 4343,2006,43240H,2131 ISC 164 18/50m 0343,2006,43240H,2131 ISC 164 18/50m 0343,2006,43240H,204 MA 16/19/10 20171,1155,7572W,103 ISC 164 19/13m 2141,1155,7572W,103 ISC 164 19/13m 2141,1155,7572W,103 ISC 164 19/13m 2347,7920N-123736 Less reliable solution. IEC 16/19/20m 2347,79220N-123736 IEC 16/19/20m 2347,79220N-123736 IEC 16/19/21m 2349,32555,7156W, network solution. IEC 16/19/21m 3346,32555,7156W, ISC 164 19/13m 2741,4477NA657EE. In LEG 16/19/23m 2741,4477NA657EE.102 ISC 164 19/13m 754,942555,77576W, NEIC 16/19/23m 2741,4477NA657E.102 ISC 164 19/13m 354,32555,7156W, ISC 164 19/13m 354,32555,77576W, ISC 164 19/13m 356,92044,4475NA53114,775 ISC 164 19/13m 356,920454,4475NA5314,775 CHEC 16/19/23m 2741,4477NA657EE.102 ISC 164 19/13m 564920476,4475NA530, ISC 164 19/13m 385692044,43729N,33455N255,7057W, N24,705421,France JMA 164 19/13m 564920476,44375N,33455N2,7057W, M34,725,7074480,34755,70577W, M55 18/19/43m 4478,3470252707W, M55 18/19/43m 4478,3470252707W, M55 18/19/43m 4478,3470252707W, M55 18/19/43m 4478,3470252707W, M55 18/19/43m 4478,3470252707W, 	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 12.3 +11.3 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mb4.3/3 73'08W±'092, 5/4, 3C-4D, Northern 5/4, 3
 Carl Andrew Bern 151.01 300 [JFKP GRM Grahamstown 151.01 300 [JFKP GRM [95m, 160:1] GPOF Poladier 153.19 317 [JFKP POF Poladier 153.19 317 JFKP STO Syowa Base 153.88 211 [46]KP CER Carea 156.87 313 JFKP EUC 164 169 42m 23e, 6:56N-73:19W, ISC 164 169 42m 23e, 6:56N-73:19W, ISC 164 169 45m 23e, 6:26N-73:19W, ISC 164 169 55m 43e, 149, 0:113116, Mbd Colombia ROM 164 169 55m 43e, 149, 0:113116, Mbd Colombia ROM 164 169 55m 43e, 149, 0:113116, Mbd Colombia ISC 164 169 55m 43e, 149, 0:113117 or0e71/5, Central Italy EUC 164 169 55m 507, 5:113N-1792130 Less reliable solution, ISC 164 169 55m 507, 5:113N-1792130 (JSC 164 169 55m 507, 5:113N-1792130) ISC 164 169 55m 507, 5:113N-1792130 (JSC 164 169 55m 507, 5:113N-1792130) ISC 164 169 55m 507, 5:113N-1792130 (JSC 164 169 55m 507, 5:113N-1792050, M3-5, n31, Kuril Islands ISC 164 169 169 02 00:32506, 43:49N-204 (M3-5, n31, Kuril Islands ISC 164 169 169 02 00:327, 79:20N-102:3766 (JSC 169 169 120 02:387, 79:20N-122:3766 (JSC 169 169 120 02:387, 79:20N-122:3766 (JSC 169 169 20 02:387, 79:20N-122:3767 (JSC 169 169 20 02:387, 79:20N-122:3767 (JSC 169 169 20 02:385, 345, 32:55, 71:57W, network solution, SC 164 169 22 00 07:44, 07:3, 34:55N-351, 71 (JSC 164 19h 23 00 7:44, 07:3, 34:55N-351, 72 (JSC 164 1	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.3 19 02 15.0 +11.3 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 14.0 (2.1) -54.7 15.7 54.3C-40, Northern 54.3C-40, Northern 5.4.3C-40, Northern 55.7 55.7 147:5555±10, h4.0 10.4.6/2 79:15.7 78:17W±14, h39km, n10,
 Charlane Semi 131-01 300 [JFKP GRM Grahamstown 131-01 300 [JFKP GRM (J66m, 160:1) GRM Grahamstown 153.19 301 JFKP GRM (J66m, 160:1) FOP Foldeder 153.19 317 JFKP SYO Syowa Base 153.88 213 JepKP SYO Syowa Base 153.88 213 JepKP SYO Syowa Base 153.88 213 JepKP EIOC 164 16h 42m 23r9, 6:66N-73:19W, ISC 164 16h 42m 23r9, 6:766N-73:19W, ISC 164 16h 45m 23r9, 6:766N-73:19W, ISC 164 16h 45m 42r4, 189, 4:278N-8:115x1 or07175, Central Italy FIDC 164 16h 55m 444-198, 4:278N-8:115x1 or07175, Central Italy FIDC 164 16h 55m 50r2, 51:37N-179153 EIOC 164 16h 55m 50r2, 51:37N-179153 EIOC 164 16h 55m 50r2, 51:37N-179153 Lass reliable solution, ISC 164 18h 55m 50r2, 51:37N-179153 Lass reliable solution, ISC 164 18h 50m 51:4-17, 51:4N-8:15x1 n17, 01*52/16, Mb4.114, Rat Island MA 164 19h 03m 03:32-066, 43:49N-204 M3.5, n31, Kurll Islands IGO 164 10h 10m 23r7, 75:20N-123:756 Lass reliable solution, CIO 164 19h 20m 23r7, 75:20N-123:756 Lass reliable solution, CIO 164 19h 20m 23r7, 75:20N-123:756 Lass reliable solution, CIO 164 19h 20m 23r7, 75:20N-123:756 Lass reliable solution, CIO 164 19h 21m 33r6, 32:5558,71:57W, network solution, CIO 164 19h 21m 33r6, 32:558,21:477, CIO 495/11, Near coast of Central CI NEIC 164 19h 22m 27r4, 44:07N-45720, FC, Lass NEIC 164 19h 22m 27r4, 44:07N-4578, 50 LDS 164 19h 22m 27r4, 50, 54:50N-55N-50 SC 164 19h 32m 57r4, 54, 54:50N-50 SC 164 19h 32m	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.3 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 13 252 18.1 19.7 13 252 19.8 19.8 1417555 19.8 10.8 11 10 27 19.8 10.8 11 10 27 10.8 10.8 11 10 27 10.8 11.1 11 10 27 10.8 11.1 11 10 27 10.8 11.1 11 10 27 10.8 10.9 11 10 27
 Charlane Stein 131-01 300 [JFKP GRM Grahamstown 131-01 300 [JFKP GRM (J96m, 180:1) GRM Grahamstown 153.19 301 JFKP GRM (J96m, 180:1) FOP Foldeder 153.19 317 JFKP SYO Syowa Base 153.88 211 JePKP SYO Syowa Base 153.88 211 JePKP EIDC 164 16h 42m 234,9,6 7560 Ar3:19W, ISC 164 16h 42m 234,9,6 7560 Ar3:19W, ISC 164 18h 42m 234,9,6 7578 Ar309, h161 Hm, 144m, n14, 01413116, M04 Colombia ROM 164 16h 56m 444-118, 4228 Ar111x1 oOV7175, Central Raiy EIDC 164 16h 56m 444-118, 4228 Ar111x1 oOV7175, Central Raiy EIDC 164 16h 56m 444-118, 4228 Ar113r1 oOV7175, Central Raiy EIDC 164 16h 59m 504-2173 Nr.179:054 Less reliable solution. ISC 164 18h 59m 514-217, 5174 Ar2:15x1 n17, 01452176, Mb4.174, Rat Islande IGO 164 19h 13m 2141, 115x-78:2W, A3 ISC 164 19h 13m 2141, 2153-2056, central Bradow 304/50, 05, 3249Ar204 (M3.5, n3), Kuril Islande IGO 167 19h 13m 2141, 115x-78:2W, A3 ISC 164 19h 20m 2347, 79:20Ar205, 21555, 21567, central Bradow 304/50, 05, 05, 05, 05, 05, 05, 05, 05, 05,	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.3 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mbd.3/3 73108W±7092, 54.3 52-40, Northern 5km, Mb2.6 372E±18, h5km, n5, 5. h0km, Mb4.6/4 5. h0km, Mb4.6/4 5. h0km, Mb4.6/4 79:1E±13, h41km±15km, 15 141755E±205, h24km, 15 h10km, c0#972, Mb4.5/20, 10km, d0#972, Mb4.5/20, 10km, c0#972, Mb4.5/20, 10km, c0#972, Mb4.5/20, 10km, c0#972, Mb4.5/20, 10km, c0#972, Mb4.5/20, 10km, c0#972, Mb4.5/20, 10km, c0#99, Single h15km 17728±26, h10km, n11, h1e 5km, c0#93, k2.4(GEN), m, Mb2.2 30x6595±2090, h5km, 1417015±203, h49km, n5, 141728±204, h52km, 1105±203, h7km±15km, t14728±204, h52km, 14304±2, 5ingle h2km 14304±2, 203, h0km, M3.0 14304±203, h7km±15km, t14304±24, h0km, n13, 14304±203, h7km±15km, t14304±2, 203, h0km, M3.0 14304±2, 203, h0km, M3.0
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 Charlane Stein 151.01 300 [JFKP GRM (JS6m, 160.1]) GRM (JS6m, 160.1]) GRM (JS6m, 160.1]) GRM (JS6m, 160.1]) FOP Folder 153.19 317 [JFKP SY0 Syowa Base 153.88 211 [JSFR] GRM (JS6m, 160.1]) FOF Folder 153.19 317 [JFKP SY0 Syowa Base 153.88 211 [JSFR] ELCC 164 169 42m 23e, 6:56N, 731.9W, ISC 164 169 42m 23e, 6:42, 6:75N, 159N, 159N, h161tm, 149n, 119, 01413116, Mb4 Colombia ROM 164 169 55m 43eQ, 42:8N, 1371, 15, Mb4 (JSC 164 169 55m 43eQ, 42:8N, 1371, 157131 (JSC 164 169 55m 5072, 51137N, 179131) (JSC 164 169 50m 51e, 187, 514N, 15, 1 n17, 01452/16, Mb4, 1/4, Rat Island (JAA 164 19h 02m 0273, 2066, 43749N, 204 (M3.5, n31, Kurli Islands ISC 164 19h 12m 23a, 79:20N, 123726 (JSC 164 19h 12m 23a, 1508, 5060, 00460/10, 3C-2D, Ecuador NEC 167 19h 20m 2347, 79:20N, 123726 (JSC 164 19h 23m 744, 413N, 44:7N, 65726, 14 (JSC 164 19h 23m 744, 413N, 44:7N, 65726, 15 (SC 164 19h 23m 744, 413N, 44:7N, 557, 75774, 7578, 75	19 02 50.1 +48.5 19 02 50.1 +11.3 19 02 15.0 +11.3 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mb4.3/3 73'08W2'092, 54.3 C-40, Northern 5km, Mb4.6/4 5, h39km, of 461, Mb4.6/2, 78'182.13, h41km_15km, is 147'5555.105, h24km, 0'm, Mb4.4/5 9'm, Mb3.2 78'11Wa114, h39km, n10, 78'11Wa114, h39km, n10, 78'11Wa114, h39km, n10, 78'11Wa114, h39km, n10, 78'11Wa124, h39km, n10, 78'11Wa124, h39km, n10, 78'11Wa124, h39km, n10, 78'11Wa124, h39km, n10, 78'11Wa125, h10km, n11, hile 5km, o0993, kg2.4(GEN), m, ML22 30x8'5955.105km, 141'0152.703, h49km, 110'123, h7km, 15km, r region 143'0452.703, h0km, M3.0, 143'0452, 103, h0km, m6,
 C. T. Harmsteven 13-1.01 300 [JFKP GRM (JS6nn, 160:1) GRM Grahamsteven 153.19 301 JFKP GRM (JS6nn, 160:1) FOP Foldeder 153.19 317 JFKP SYO Syowa Base 153.88 201 JepKP SYO Syowa Base 153.89 201 JepKP HIG 161 Bh 42m 22*2, 157, 157, 157, 157, 157, 157, 157, 157	9 02 50.1 +48.5 19 02 15.0 +11.3 19 02 15.0 +11.3 19 02 15.0 +11.3 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 1417:555=2:05, h24km, n5, 10.4 -7 11.1 10.8 -7 1417:555=2:05, h24km, n10, -7 -7 11.10km, d04.4/5 11.1 10.8 110km, d04.4/5 11.1 11.1
 Charlane Semi 131-01 300 [JFKP GRM (JSGnn, 180:1) GRM Grahamstown 153.19 301 JFKP GRM (JSGnn, 180:1) FOP Foldeder 153.19 317 JFKP SYO Syowa Base 153.88 211 JepKP SYO Syowa Base 153.88 211 JepKP EIDC 164 18h 42m 224-142, 675N4.1095- h1610m, 144m, 181, 01413116, Mb4 Colombia ROM 164 18h 56m 44-2189, 4220N4:1111 d097115, Central Italy EIDC 164 18h 56m 44-2189, 4220N4:1111 d097115, Central Italy EIDC 164 18h 56m 44-2189, 4220N4:1111 d097115, Central Italy EIDC 164 18h 56m 44-2189, 4220N4:1111 Cld 18h 56m 4646, 51113N4, 179:0521 Less reliable solution. ISC 164 18h 56m 514-317, 5174N4:11541 n17, 01452116, Mb4,114, Rat Islande IGO 164 19h 13m 224; 143, 11058-1068- uess reliable solution. EIDC 164 19h 20m 2397, 797:20N4:123:37E ISC 164 19h 20m 2397, 797:20N4:123:37E ISC 164 19h 20m 2397, 797:20N4:123:37E ISC 164 19h 21m 3296, 327:358-71:66W, network solution. IEIC 164 19h 21m 3296, 327:358-71:66W, ISC 164 19h 21m 3296, 327:358-71:66W, ISC 164 19h 21m 3296, 327:358-71:66W, ISC 164 19h 22m 2714, 44:77NA6:78E, h LDG 167 19h 22m 2714, 44:77NA6:78E, h LDG 167 19h 22m 2714, 44:77NA6:78E, h LDG 167 19h 22m 274, 44:8075, 44:75NA:20 n21, 0048422, France JMA 161 19h 32m 56:99_04, 43:29A:200 n21, 0048422, France JMA 161 19h 32m 56:99_04, 43:29A:200 n21, 0048424, Chile-Argentina bord n44, hc2, Swith East 054 104 105522 10:07 N, 180 1164 19h 32m 56:99_04, 43:29A:200 n21, 004842, Chile-Argentina bord n44, hc2, Swith East 054 104 noshi JMA 164 19h 32m 56:99_04, 43:19A:200 JMA 164 20h 08m 21:3,003, 40:071M-101, ISC 164 20h 08m 21:3,003, 40:071M-101, ISC 164 20h 07m 194-276, 33:19A:1111 004375, 011, Pyremese JMA 164 19h 32m 56:92_042, 35:1N4:111 004375, 011 sest 00544, 34,014,014,014,014,014,014,014,014,014,01	19 02 50.1 +48.5 19 02 50.1 +11.3 19 02 15.0 +11.3 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 19 01 14.0 (2.1) -54.7 10 01 14.0 (2.1) -54.7 10 01 14.0 (2.1) -54.7 10 01 14.0 (2.1) -54.7 11 02 ^{km} , MD4.3/3 3721084:10, Northern 5 ^{km} , MD2.6 37228.218, h5km, n5, 5 ^{km} , MD2.6 57218.218, h5km, n10, 5 ^{km} , MD4.6/4 5 ^{km} , MD4.6/2 5 ^{km} , MD4.6/4 5 ^{km} , MD4.4/5 9 ^{km} , MD3.2 5 ^{km} , MD4.4/5 9 ^{km} , 208.92, Single h15 ^{km} 1774:228, h49 ^{km} , n5, 1471288.2090, h5 ^{km} , 140:05.218, h49 ^{km} , n5, 143:08.219, h5 ^{km} , M3.0 143:08.214, h0 ^{km} , m3, 006W.211, h10 ^{km} , m6, 140:578.201,
 Charlane toem 131-01 300 JFKP GRM (J96m, 160:1) GRM (J96m, 160:1) FOF Poladier 153.19 317 LiPKP POF Poladier 153.19 317 LiPKP SYO Syows Base 153.88 211 LePKP CER Ceres 156.87 313 LiPKP EIDC 16/16/16/207294, 5660N, 73:19W, ISC 16/16/16/207294, 5660N, 73:19W, ISC 16/16/16/207294, 5660N, 73:19W, ISC 16/16/16/16/207294, 5778N, 1098- h1611ms, 144m, n18, 01813116, M04 Colombia ROM 16/16/16/507 4676, 511:13N, 179:05L HIC 16/16/16/507 4676, 511:13N, 179:05L HIC 16/16/16/507 4676, 511:13N, 179:05L HIC 16/16/16/507 4676, 511:13N, 179:05L HIC 16/16/16/507 4676, 511:13N, 179:05L Less reliable solution. ISC 16/18/19/007 0343-006, 43:49N-104 M3.5, n31, Kurll Islands IGO 16/19/19/19/217, 179:20N-123:75E Less reliable solution. ISC 16/19/19/207/397, 79:20N-123:75E Less reliable solution. ISC 16/19/207/397, 79:20N-123:75E ISC 16/19/217/396, 32:55S, 71:57W, network solution. ISC 16/19/217/366, 32:55S, 71:57W, NEIC 16/19/27/396, 32:55S, 71:57W, NEIC 16/19/27/397, 744, 413Mbc*E, Lab SC 16/270 00F 711, 44777Nbc*E, Lab SC 16/270 01/19/27/35, 34:55N-200, NA 16/270 02F 713, 043, 40:705S, 72:704W, NEIC 16/19/397 07:44, 93, 30:705S, 72:704W, NEIC 16/19/397 07:44, 93, 30:705S, 72:704W, NEIC 16/19/397 07:44, 93, 30:705S, 72:704W, NEIC 16/19/397 07:44, 93, 40:705S, 72:704W, NEIC 16/19/397 07:42, 04:305, 72:704W, NEIC 16/19/397 07:42, 04:305, 72:704W, NEIC 16	19 02 50.1 +48.5 19 02 50.1 +11.3 19 02 15.0 +11.3 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mbd.3/3 73108W±1092, 54.3 52.4 0.0 Northern 5km, Mb2.6 372E±2.18, h5km, n5, 5. h0km, Mb4.6/4 5. h0km, Mb4.6/4 5. h0km, Mb4.6/4 5. h0km, Mb4.6/4 78:118, h41km±15km, 15 1407:52±205, h24km, 15 1407:52±205, h24km, 15 16 16 16 17 16 16 17 16 16 17 16 17 16 16 17 16 16 17 16 17 16 16 16 17 16 16 16 16 17 16 16 16 16 16 16 16 16 16 16
 Charles and Sense 11-101-3000 [JFKP GRM (J96m, 1907)] GRM (J96m, 1907)] FOF Poladier 153.19 317 LiPKP SYO Syows Base 153.88 211 LaPKP SYO Syows Base 153.88 211 LaPKP EIDC 16/18h 42m 224:18, 617 SYI 19W, ISC 16/18h 42m 224:18, 4278W-115:1 ISC 16/18h 55m 4646, 511:13N-179:05L NEIC 16/18h 55m 4646, 511:13N-179:05L NEIC 16/18h 55m 4646, 511:13N-179:05L NEIC 16/18h 55m 4646, 511:13N-179:05L NEIC 16/18h 55m 512, 51:37N-179:13L Lass reliable solution. ISC 16/18h 30m 03:43-016, 43:48N-104 M3.5, n31, Kurll Islands IGO 16/19h 13m 2141, 11:15S-76:2W, h31 ISC 16/19h 13m 2147, 179:20N-103 ISC 16/19h 13m 2141, 11:15S-76:2W, h31 ISC 16/19h 13m 2147, 179:20N-103 ISC 16/19h 13m 2147, 179:20N-103 ISC 16/19h 13m 2147, 179:20N-103 ISC 16/19h 13m 2147, 179:20N-103 ISC 16/19h 21m 3249, 32:55S-71:69W, ISC 16/19h 21m 3249, 32:55S-71:67W, network solution. NEIC 16/19h 21m 3249, 32:55S-71:67W, ISC 16/19h 21m 3346, 32:53S-71:67W, ISC 16/19h 21m 3346, 32:53S-71:67W, ISC 16/19h 21m 3346, 32:53S-71:67W, NEIC 16/19h 21m 249, 27:55S-71:67W, NEIC 16/19h 21m 249, 27:55S-7000W, NE	19 02 50.1 +48.5 19 02 15.0 +11.3 19 02 12.3 +8.7 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mbd.3/3 73108W±1092, 544.3C-40, Northern 5km, Mbd.6/4 5, A32m, Oktober 5, A32m, Oktob
 Charland Stein 131-01 300 [JFKP GRM (JS6m, 160:1) GRM (JS6m, 160:1) FOF Folder 153.19 317 [JFKP SY0 Syowa Base 153.88 211 [JSFR] GRM (JS6m, 160:1) FOF Folder 180 42m (23e, 6:56M, 731:30) ISC 161 180 42m (23e, 128, 5:78M, 209) ISC 161 180 42m (23e, 228M, 13t), MMA Colombia ROM (J61 18) 55m 430, 42:80M, 13t), MMA (SC 161 18) 55m 430, 42:80M, 13t, 15M GRM (J61 18) 55m 430, 42:80M, 13t, 15M CIC 161 18) 55m 507, 5:113M, 179:05t LICS 164 18) 55m 507, 5:113M, 179:05t LICS 164 18h 59m 514, 187, 5:14M, 175, 73t LICS 164 18h 59m 514, 187, 5:14M, 15M, 179:05t LISS 164 18h 50m 514, 187, 5:14M, 15M, 179:05t LISS 164 18h 120 (23e, 20e, 43:14M, 120; 184 JAA 164 19h 120 (23e, 20e, 43:14M, 120; 184 ISC 164 19h 120 (23e, 79:24M, 123; 131; 1058, 1660; 166:109, 120; 189, 120; 132e, 70e, 140; 120; 120; 1482/16, 149, 120; 132e, 70e, 140; 120; 120; 149, 120; 132e, 70e, 140; 120; 120; 149, 120; 132e, 70e, 140; 120; 140; 140; 140; 140; 140; 140; 140; 14	19 02 50.1 +48.5 19 02 50.1 +11.3 19 02 15.0 +11.3 19 02 12.3 +8.7 19 01 14.0 (2.1) -54.7 h162km, Mb4.3/3 73'08W2'092, 54.3 C-40, Northern 54.3 C-40, Northern 55. Notw, Mb4.6/4 5. Notw, Mb4.6/2 78'18.*14, h39km, n10, 5. Notw, Mb4.4/5 147'555.*105, h24km, 11.0km, c0#72, Mb4.5/20, 1. Notw, c0#72, Mb4.5/20, 1. Notw, c0#72, Mb4.5/20, 1. Notw, c0#93, Single h15km 11.23'26.541, h10km, n11, hie 5. Notw, c0#93, kg2.4(GEN). m, ML2 30.68'89E.*090, h5km, 1.41'101E.*03, h49km, 1.147'28E.*04, h52km, 1.43'06E.*03, h0km, M3.0, 1.43'06E.*03, h0km, M3.0, 1.43'06E.*03, h0km, M3.0, 1.43'06E.*11, h59km, 1.40'57E.*01, 1.84.140'6E.*11, h59km, 1.5km, c0%42, h5km, n7,

16d 18h

 EDC 16/20*46**50*3,34*53N*134*90E. nD***, Mb5.7/15 BVDS 16/20*46**51*3,34*564N*134*99E. n17***, Mb5.840, MS5 16/20*46**51*3,34*564N*134*99E. n17***, Mb5.840, MS5 Focal mechanism: C25,D15; NP1****,933*,547*,335* MVDS Focal mechanism: C25,D15; NP1****,933*,547*,335* MVDS Focal mechanism: C25,D15; NP1******* MVDS Focal mechanism: C25,D15; NP1******* MVDS Focal mechanism: C25,D15; NP1****** MVDS Focal mechanism: C25,D15; NP1******* MVDS Focal mechanism: C25,D15; NP1********** MVDS Focal mechanism: C25,D15; NP1************************************	S 2.86 75 dPn 3.02 253 Pn 3.03 47 dPn 3.09 68 dPn 3.12 242 eS 3.14 88 dPn 3.21 27 cPn 3.24 248 Pn 3.25 52 dPn 3.26 52 ePn 3.26 52 ePn 3.32 65 2 eS 3.27 65 dPn 3.32 66 dPn 3.33 2 dPn 3.37 57 eS 3.37 81 dPn 3.51 91 Pn 3.55 64 dPn 3.55 244 Pn 3.57 86 dPn 3.60 65 Pn 3.64 45 Pn 3.75 249 Pn 3.75 249 Pn 3.60 65 Pn 3.64 45 Pn 3.77 60 Pn 3.61 234 Pn 3.77 60 Pn 3.61 234 Pn 3.61 234 Pn 3.76 Pn 3.69 65 Pn 3.69 65 Pn 3.69 65 Pn 3.69 65 Pn
 MOS 162 CPR 5183, 34: 5M#138: 39E, IN 7PM, MDE 840, MS7, 2713 MOS Focal mechanism: C25, D19; NP1;eg3437, 347*, 345*, NP2; g3227, 865*3, 131*, Principal ares: T Plg52*, Azm185*, N MPG36*, Azm27*; P Plg10*, Azm289*, Mg=1, 1x:10¹⁹Mm (OBN), MS4 1560*, 327*, 857*,	3.02 253 Pn 3.03 47 dPn 3.09 58 dPn 3.12 242 eS 3.14 88 dPn 3.21 27 cPn 3.24 248 Pn 3.25 79 dPn 3.26 52 dPn 3.26 52 ePs 3.26 52 ePs 3.26 52 ePs 3.26 52 eS 3.37 57 eS 3.37 57 eS 3.37 57 eS 3.37 81 dPn 3.50 65 Pn 3.60 65 Pn 3.64 45 Pn 3.75 249 Pn 3.60 65 Pn 3.64 45 Pn 3.75 249 Pn 3.75 249 Pn 3.60 65 Pn 3.64 45 Pn 3.77 60 Pn 3.61 234 Pn 3.77 60 Pn 3.61 234 Pn 3.77 60 Pn 3.61 234 Pn 3.76 67 Pn
 MOS Focal mechanism: C25,D15; NP1:se333:347:J365; NP2:se333:347:J365; NP3:se333:347:J365; NP3:se3333:347:J365; NP3:se3333; NP3:Se333; NP3:Se333	3.09 68 dPn 3.12 242 eS 3.14 88 dPn 3.21 27 cPn 3.24 248 Pn 3.25 79 dPn 3.26 52 dPn 3.26 52 eS 3.26 52 eS 3.26 52 Pn 3.30 266 dPn 3.30 2017 dPn 3.31 82 dPn 3.32 50 dPn 3.37 57 eS 3.37 81 dPn 3.56 64 dPn 3.57 86 dPn 3.60 65 Pn 3.61 234 Pn 3.75 249 Pn 3.61 234 Pn 3.75 249 Pn 3.61 234 Pn 3.77 60 Pn 3.81 234 Pn 3.85 65 Pn
 PG36*Arm27*; P. PG10*Azm289*, Mg=1.1x10¹⁹Nm (OBN) JUS Usuki MAK Fél 20* 46% 5158.00: 35:04'E.200. MAK Fél LeVI J Sumoto, Köbe, V Toyo'oka, Hikone, Kyöto, IV: Nara, Kóchi, Totton. Tokushima, Okayama, Takamatsu, Mazuru, Himej, Wakayama, Okayama, Takamatsu, Mazuru, Himej, Wakayama, Okayama, Gilu, Fukuki, III Oita, Saigó, Hiroshima, Osayama, Ya MAT Matsushiro misaki, Owase, Nagoya, Kanazawa, Iida, Toyama, Wa MJ, Takayama, Karuzawa, Hamamatsu, Shizuoka, Kóti, Mishima, Nagano, Takada, Yokohama BJI 169 20* 46% 52*0, 34*651Ni 135*02E. 20% mMoč. 1, Ms7.3 NECI 169 20* 46% 52*0, 34*651Ni 135*02E. 20% mMoč. 1, Ms7.3 NECI 169 20* 46% 52*0, 34*651Ni 135*02E. 20% mMoč. 1, Ms7.3 NECI 169 20* 46% 52*0, 43*651Ni 135*02E. 20% mMoč. 1, Ms7.3 NECI 169 20* 46% 52*0, 34*651Ni 135*02E. 20% mMoč. 1, Ms7.3 NECI 169 20* 46% 52*0, 43*651Ni 135*02E. 20% mMoč. 1, Ms7.3 NECI 169 20* 46% 52*0, 44*651Ni 148*02 Mistorima, Nagano Livit Ji Inte Koba area and on Awaji-shima. Over 90 percent of the casualtes occurred along the southem coast of Honshu between Kobe and Nishinomya. At least 28 people were killed by a landskide at Nishinomya. At least 28 people were killed by a landskide at Nishinomya. At least 28 people were killed by a landskide of destroyet Numerous Tars, gas and water main breaks and power outages occurred in the epicentral area. Felt VIJ aton Shitonomia and in the lehnomotya area on Awaji-shima; VMM at Iwakuni, displacement of 1.2 to 1.5 meires in the northem part of melchinomya area on Awaji-shima; VMM at Iwakuni, the lehnomist ensor Solution: 31, scale 1018/m; Mud.09; KMG (1=1 JMA) NEC Radiated energy from the P-wave first-motion solution: 8.51.5k1014/1048 NEC Maciated energy from the P-wave first-motion solution: 8.55.1.5k1014/1048 NEC Maciated enema area on Awaji-shima; VMM at Nakuni, theathioj imin 145m; Ph	3.12 242 eS 3.14 88 dPn 3.21 27 cPn 1.25 79 dPn 3.26 52 dPn 3.26 52 ePn 3.26 52 ePn 3.26 52 ePn 3.32 65 2Pn 3.32 50 dPn 3.33 22 dPn 3.32 50 dPn 3.33 82 dPn 3.37 57 eS 3.7 81 dPn 3.50 65 Pn 3.60 65 Pn 3.61 234 Pn 3.75 249 Pn 3.60 Pn 3.67 6 Pn 3.89 76 Pn
 h16km-2em, M7.2 MAR Felt I-VI J Sumolo, Köbe, V Toyo'oka, Hikene, Kyöto, IV Nara, Köchi, Totton, Tokushima, Okayama, Takamatsu, Mazuru, Himej, Wakayama, Osaka, Tsu, Tsunga, Giu, Fukui, III Oita, Saigó, Hiroshima, Matsuyama, Murotomisaki, Yonago, Matsue, Shiono misaki, Owase, Nagoya, Kanazawa, Ida, Toyama, Wa jima, Takayama, Karuzawa, Hamamatsu, Shizuoka, Kötu, Mishima, Nagano, Takada, Yokohama BJI 169 20º 49m 52º0, 34º 531Ni 135'02E, I-26^{im}, Mb6 1, Ms7.3 NECI 169 20º 49m 52º1, 34º 580Ni 135'02E, I-26^{im}, Mb6 1, Ms7.3 NECI 169 20º 49m 52º1, 34º 580Ni 135'02E, I-26^{im}, Mb6 1, Ms7.3 NECI 169 20º 49m 52º1, 34º 580Ni 135'02E, I-26^{im}, Mb6 1, Ms7.3 NECI 169 20º 49m 52º1, 34º 580Ni 135'02E, I-26^{im}, Mb6 1, Ms7.3 NECI 169 20ⁱⁿ 49m 52ⁱⁿ, 34º 580Ni 135'02E, I-26^{im}, Mb6 1, Ms7.3 NECI 169 20ⁱⁿ 49m 52ⁱⁿ, 34º 580Ni 135'02E, I-26^{im}, Mb6 1, Ms7.3 NECI 169 20ⁱⁿ 49m 52ⁱⁿ, 34º 580Ni 135'02E, I-26^{im}, Mb6 1, Ms7.3 NEIC 169 20ⁱⁿ 49m 52ⁱⁿ, 34º 580Ni 135'02E, I-26^{im}, Mb6 1, Ms7.3 NEIC 169 20ⁱⁿ 49m 52ⁱⁿ, 34º 580Ni 135'02E, I-26^{im}, Mb6 1, Ms7.3 NEIC 169 20ⁱⁿ 49m 52ⁱⁿ, 34º 580Ni 135'02E, I-26^{im}, Mb6 1, Ms7.3 NEIC Mas 54 (ISS), Mw6 9(HRV), Casualites I-XII MM Nick Masababa, Alababa 1, 1000 people were killed by a landskide at Nishinomya, Al least 28 people were killed by a landskide at Nishinomya, Aloui 310,000 people were evacualed to temporary shelters. Over 200,000 buikdings were camaged or destroyed Numerous Tinss, gas and waler main breaks and power outages occurred in the epicentral area. Felt VI J atong a coasta strip extending from Suma Ward, Kobe to Nishinomiya and in the lehinomiya area on Awaji-shima; V MM at Iwakuni, KJ Kikija bahima area. Depth from broadband displacement seismogram	3.21 27 cPn eS 3.24 248 Pn 3.25 52 dPn 3.25 52 dPn 3.26 52 eS 3.26 52 eS 3.26 52 ePn 3.30 266 dPn 3.31 266 dPn 3.32 50 dPn 3.33 22 dPn 3.37 57 eS 3.51 91 Pn 3.55 64 dPn 3.55 64 dPn 3.57 86 dPn 3.56 45 Pn 3.57 249 Pn 3.57 249 Pn 3.64 45 Pn 3.57 249 Pn 3.57 249 Pn 3.61 234 Pn 3.57 60 Pn 3.89 76 Pn 8.89 76 Pn
 IV Nara, Kóchi, Totton, Tokushima, Okayama, Takamatsu, Mazuru, Himej, Wakayama, Osaka, Tsu, Tsunga, Giu, Fukui, III Oita, Saigó, Hindshima, Csaka, Tsu, Tsunga, Giu, Fukui, III Oita, Saigó, Hindshima, Candon, Tokada, Yonago, Matsus, Shinon misaki, Owase, Nagoya, Kanazawa, Ida, Toyama, IWa jima, II Miyazaki, Shimonoseki, Kumanoto, Saga, Uwa jima, Takayama, Karucawa, Hamamatsu, Shizuoka, Kótu, Mishima, Nagano, Takada, Yokohama BJI 169 209 49m 5291, 34:55Ni 135:702E, In26m, Mb61, Ms7.3 NECI 169 209 49m 5291, 34:55Ni 135:702E, In26m, Mb61, Ms7.3 NECI 169 209 49m 5291, 34:55Ni 135:702E, In26m, Mb61, Ms7.3 NECI 169 209 49m 5291, 34:55Ni 135:702E, In26m, Mb61, Ms7.3 NECI 169 209 49m 5291, 34:55Ni 135:702E, In26m, Mb61, Ms7.3 NECI 169 209 49m 5291, 34:55Ni 135:702E, In26m, Mb61, Ms7.3 NECI 169 209 49m 5291, 34:55Ni 135:702E, In26m, Mb61, Ms7.3 NECI 169 209 49m 5291, 34:55Ni 135:702E, In26m, Mb61, Ms7.3 NECI 169 520 49m 5291, 34:55Ni 135:702E, In26m, Mb61, Ms7.3 NECI 169 209 49m 5291, 34:55Ni 135:702E, In26m, Mb61, Ms7.3 NECI 169 209 49m 5291, 34:55Ni 157:702E, In26m, Mb61, Ms7.3 NECI 169 209 49m 5291, 34:55Ni 157:702E, In26m, Mb61, Ms7.3 NECI 169 200 49m 5291, 34:55Ni 157:702E, In26m, Mb61, Ms7.3 NECI Mataka Ma	3.24 2.48 Pn 3.25 79 dPn 3.26 52 dPn 3.26 52 eS 3.26 52 eS 3.26 52 eS 3.20 50 dPn 3.30 266 dPn 3.31 25 dPn 3.37 87 dS 3.50 65 Pn 3.50 65 Pn 3.60 P5 Pn 3.60 P5 Pn 3.60 P6 Pn
 Takaninato, macOut, Pintel, Yiakayanie, Osaka, Fab, Tisu, T	3.26 52 dPn 3.26 52 dPn eS 3.26 52 dPn 3.26 52 Pn 3.30 266 dPn 3.31 82 dPn 3.37 81 dPn 3.50 237 dPn 3.50 237 dPn 3.56 44 dPn 3.56 64 dPn 3.56 45 Pn 3.56 258 dPn 5 3.60 65 Pn 3.77 60 Pn 3.81 234 Pn 3.77 60 Pn 3.81 254 Pn 3.76 67 Pn
 Malsuyama, Murotomisaki, Yonago, Malsue, Shonoo misaki, Owase, Nagoya, Kanazawa, Iida, Toyama, Wa misaki, Owase, Nagoya, Kanazawa, Iida, Toyama, Wa misaki, Owase, Nagoya, Kanazawa, Iida, Toyama, Wa misaki, Magana, Takayama, Karuzawa, Hamamatsu, Shizuoka, Kóhi, Matkusahiro Malsusahiro Nere 100 percent of the casuahis occurred along the southern coast of Honshu between evacualed to temporary shelters. Over 200,000 peole were evacualed to temporary shelters. Over 200,000 pulkings water main breaks and power outges occurred in the epicentral area. Peht IVI J an elong a coastal strip extending from Suma Ward, Kobe to Nishinomiya and in the lehomomya area on Awajishima, Vienero Shironali Malsusahiro Malsusahiro, Alare Vienero Malsusahiro Malsusahirona Malsubahiro Malsusahiro Malsusahiro	eS 3.26 52 ePn 9.30 266 dPn 3.31 250 dPn 3.32 50 dPn 3.33 82 dPn 3.37 57 eS 3.37 87 eS 3.37 81 ePn 3.50 237 dPn 3.51 91 Pn 3.56 44 dPn 3.57 86 dPn 3.56 45 Pn 3.75 249 Pn 3.75 249 Pn 3.75 60 Pn 3.89 76 Pn 3.89 76 Pn
 jima, II. Miyazaki, Shimonoseki, Kumamoto, Saga, Uwa jima, II. Miyazaki, Shimonoseki, Kumamoto, Shizuoka, Kóhi, Mishima, Nagano, Takada, Yokohama BJI 69 20' 495 254', Shi 55 202E, h26^m, Mb6.1, Ms7.3 NECI 167 20' 495 724', Shi 55 202E, h26^m, Mb6.1, Ms7.3 NEIC 167 20' 495 724', Shi 55 202E, h26^m, Mb6.1, Ms7.3 NEIC 167 20' 495 724', Shi 55 202E, h26^m, Mb6.1, Ms7.3 NEIC 167 20' 495 724', Shi 55 202E, h26^m, Mb6.1, Ms7.3 NEIC 167 20' 495 724', Shi 55 202E, h26^m, Mb6.1, Mb7.3 NEIC 167 20' 495 724', Shi 55 202E, h26^m, Mb6.1, Mb7.3 NEIC MS 5.5 (BHK), Mo=6, Sat 10¹⁹ Am (PT), Five thousand in functed hvo people contimed killed, 36, 866 injured and extensive damage leVII J in the Koba area and on Awajishima. Over 90 percent of the casualities to CHLI Chichibu Chichibu Cost of destroyed. Numerous Environming and in the about 310,000 people were evacuated to temporary shelters. Over 200,000 buildings were damaged or destroyed. Numerous Environming and in the epicentral area. Felt VI J on Shiknou, Right-lateral surface faulting was observed to 9 kilometres with horizontal area. Depth from braadband displacement seismograms. NEIC Adiated energy from the P-wave first-motion solution: 8,51.5 k10¹⁴ MM7 NEIC Maitated bardiated action solution: 8,51.5 k10¹⁴ M47 NEIC Maitated energy from the P-wave first-motion solution: 8,51.5 k10¹⁴ M47 NEIC Maitated energy from the P-wave first-motion solution: 8,51.5 k10¹⁴ Mathright and the sect of 1.2 to 1.5 metres in the norther part of Numerous Environmal area. Depth from braadband displacement seismograms. NEIC Maitated energy from the P-wave first-motion solution: 8,51.5 k10¹⁴ M196 NEIC Maitated energy from the P-wave first-motion solution: 1,51.5 metres in the norther part 1,51.5 mit 10¹⁴ M196 NEIC Maitated energy from the P-wave fir	eS 3.26 52 Pn 3.30 266 dPn 3.32 50 dPn 3.33 82 dPn 3.37 57 eS 3.37 81 dPn 5.50 237 dPn 3.51 91 Pn 3.56 64 dPn 3.57 86 dPn 3.56 45 Pn 3.75 249 Pn 3.75 249 Pn 3.75 60 Pn 3.81 234 Pn 3.81 234 Pn 3.81 254 Pn 3.76 67 Pn
 Mishima, Nagano, Takada, Yokohama BJI 169 20° 495 20°, 43°53Ni 35°02E, 128°m, Mb6.1, Ms7.3 NECI 167 20° 495 52°1, 34°55Ni 35°02E, 128°m, Mb6.1, Mb7.3 NECI 167 20° 495 52°1, 34°55Ni 35°02E, 128°m, Mb6.1, Mb7.3 NEIC 165 20° 495 52°1, 34°55Ni 35°02E, 122°m, at60.1 NEIC MS 6.5 (BHK), Mo=6, 34:01°P/m (P7). Five thousand NEIC MS 6.5 (BHK), Mo=6, 34:01°P/m (P7). Five thousand All Ajiro All Ajiro All Ajiro All Ajiro All Ajiro Churded hvo people contirmed killed, 36,896 All Ajiro Churded and extensive damage I=VII J in the Kobe area and on Awaji-shima. Over 90 percent of the casualtes Cocurred along the southern coast of Honshu between Kobe and Nishinomiya. At least 28 people were killed by a landshde at Nishinomiya. Al least 28 people were killed by a landshde at Nishinomiya. Al least 28 people were killed by ware damaged or destroyed. Numerous Envis, gas and CHJ Chichibu CHJ Chichibu	3.30 256 dPn 3.32 250 dPn 3.33 82 dPn 3.37 57 eS 3.37 81 dPn 75 3.50 237 dPn 3.51 91 Pn 3.55 86 dPn 3.56 45 Pn 3.64 45 Pn 3.64 45 Pn 3.64 45 Pn 3.67 60 Pn 3.81 234 Pn 3.87 60 Pn 3.89 76 Pn
 NEIC 169 201 459 529 1; 34:5511/25 1:3250/25 1:3250/26 1:45299, MS6 8/52 M/s6 (S5) M/s6 5(HFY) C assumines 1/21 M/s (K1) Kamita 2 MS6 8/52 M/s6 (S5) M/s6 5(HFY) C assumines 1/21 M/s (K1) NEIC MS 6.5 (BHR), M/s6 3/510 P/T), Five thousand five hundred and hvo people confirmed killed, 36,896 injured and extensive damage 1=VII J in the Kobe area and on waji-shima. Over 90 percent of the casualtes occurred along the southern coast of Honshu between Kobe and Nishinomiya. At least 28 people were killed by a landshde at Nishinomiya. At least 28 people were killed by a landshde at Nishinomiya. At least 28 people were killed by a landshde at Nishinomiya. At least 28 people were killed by a landshde at Nishinomiya. At least 28 people were killed by a landshde at Nishinomiya. At least 28 people were killed by a landshde at Nishinomiya. At least 28 people were killed by a landshde at Nishinomiya. At least 28 people were killed by a landshde at Nishinomiya. At least 28 people were killed by a landshde at Nishinomiya. At least 28 people were killed by a landshde at Nishinomiya. At least 28 people were killed by a seat and power outages occurred in the epicentral area. Felt VI J ang a coastal strip extending from Suma Ward, Kobe to Nishinomiya and in the lehinomiya area on Awaji-shima; V MM at Iwakuni, Also felt IV J on Shikoku. Right-lateral surface faulting was observed for 9 kilometres with horizontal area. Depth from broadband displacement seismograms. NEIC Addiated energy from the P-wave first-motion solution: 8.51.6x1014/Mrg/8 NEIG Adment tensor solution: 31, scale 1019Nm; M/o.09; Mill maehtjöi jima thermoint tensor solution: 31, scale 1019Nm; M/o.09; Mill maehtjöi jima thermoint avace: 11 20 thin 24 min 162; N n 00;	3.33 82 dPh 3.37 57 eS 3.37 81 dPh 75 3.50 237 dPh 3.56 64 dPh 3.57 86 dPh 3.56 65 Ph 3.62 258 Ph 3.64 45 Ph 3.64 45 Ph 3.64 45 Ph 3.75 249 Ph 3.75 60 Ph 3.77 60 Ph 3.89 65 Ph
 NEIC MS 6.5. (BRR), Mo=6.3-r019Nm (PT), Five thousand five hundred and two people confirmed killed 36,896 Ajiro Aliro Alira Aliro Aliro	3.37 51 65 3.37 61 dPn 75 3.50 237 dPn 3.56 64 dPn 3.57 86 dPn 3.57 86 dPn 3.64 45 Pn 3.64 45 Pn 3.77 60 Pn 3.77 60 Pn 3.89 65 Pn 65 Pn 65 Pn 65 Pn
 Inter Information and Investment of Maleo, So,050 Inite Information and Investment of Maleo, So,050 Majir editates inverse damage I=VII J in the Kobe area and on Awaji-shima. Over 50 percent of the casualtes occurred along the southern coast of Honshu between Kobe and Nishinomya. At least 28 people were killed by a landside at Nishinomya. At least 28 people were killed by a landside at Nishinomya. At least 28 people were killed by a landside at Nishinomya. At least 28 people were killed by a landside at Nishinomya. At least 28 people were killed by a landside at Nishinomya. At least 28 people were killed by a landside at Nishinomya. At least 28 people were killed by a landside at Nishinomya. At least 28 people were killed by a landside at Nishinomya. At least 28 people were killed by a landside at Nishinomya. At least 28 people were killed by a landside at Nishinomya. At least 28 people were killed by water main breaks and power outages occurred in the epicentral area. Felt VI J and ga a coastal strip extending from Suma Ward, Kobe to Nishinomya and in the Ichinomya area on Awaji-shima; V MM at Iwakun, Also felt IV J on Shikoku. Right-Iateral surface faulting was observed for 9 kilometres with horizontal displacement of 1.2 to 1.5 metres in the northem part of Awaji-shima. Liquefaction also occurred in the epicentia area. Depit from breadband displacement seismograms. NEC Addiated energy from the P-wave first-motion solution: 8.51.6x10/14/mg/8 NEE Addiated energy from the P-wave first-motion solution: 15.51.6x10/14/mg/8 NEC Addiated energy from the P-wave first-motion solution: 15.51.6x10/14/mg/8 NEC Addiated energy from the P-wave first-motion solution: 15.51.6x10/14/mg/8 NEC Addiated energy from 24.51.521.6x10.91 NEC Addiated energy from the P-wave first-motion solution: 15.51.6x10/14/mg/8 NEC Addiated energy from the P-wave first-motion solution: 15.51.6x10/14/mg/8 NE	/S 3.50 237 dPn 3.51 91 Pn 3.56 64 dPn 3.57 86 dPn 3.60 65 Pn 3.62 258 Pn 3.77 60 Pn 3.81 234 Pn 3.81 234 Pn 3.81 234 Pn 3.81 256 Pn 5.89 76 Pn
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Kobe and Nishinomiya, AI least 28 people were killed by OSHJ Oshima a landskide at Nishinomiya, AI least 28 people were killed by OSHJ Oshima evacuated to temporary shelters. Over 200,000 buildings OSHJ Oshima ware damaged or destroyed. Numerous firses, gas and CHJ Chichibu waier main breaks and power outages occurred in the epicential area. Felt VIJ and gas costal strip CHJ Chichibu extending trom Suma Ward, Kobe to Nishinomiya and in the Ichinomiya areae on Awaij-shrma; V MM at Iwakuni, Also felt IV J on Shikoku. Right-Iateral surface faulting NU Nakatsue Mass Josherved for 9 kilometres with horizontal area. Depth from broadband displacement seismograms. KIG (I=1 JMA) NEC Radiated energy from the P-wave first-motion solution: 5.5.1.6x10/4/mr8 Nue-0.33; Map-0.33; Map-0.46. Depth Mas1.61; Map-1.70; Map-0.33; Map-0.33; Map-0.46. Depth	3.57 86 dPn /S 3.60 65 Pn 3.62 258 Pn 3.64 45 Pn 3.75 249 Pn 3.77 60 Pn 3.81 234 Pn 3.81 234 Pn 3.89 65 Pn eS 3.89 76 Pn
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 water main breaks and power outages occurred in the epicential area. Felt VIJ Jakong a costal strip extending from Suma Ward, Kobe to Nishinomiya and in the Ichinomkya area on Awaij-shma; V MM at Iwakuni, Also felt IV J on Shikoku. Right-Isteral surface faulting was observed for 9 kilometres with horizontal displacement of 1.2 to 1.5 metres in the northern part of Awaji-shima. Liquefaction also occurred in the epicents. NEC Radicated energy from the P-wave first-motion Southon: S.5.1.5x10/Him/8 NEC Radicate de Soution: State Of Nerv, May O.9; NEC Radicated energy from the P-wave first-motion Southon: S.5.1.5x10/Him/8 NEC Radicate de Soution: S1, scale 101PNm; Mrd.09; HJJ Hachibj jimi Mea1.61; Maj-1.70; Maj-0.33; Maj-0.33; Maj-0.46. Depth HJJ Hachibj jimi 	3.62 258 Pn 3.64 45 Pn 3.75 249 Pn 3.77 60 Pn 3.81 234 Pn 3.89 65 Pn eS 3.89 76 Pn
extending from Suma Ward, Köbe to Nishinoninga and in the Ichinoninga area on Awaij-shima; V MM at Iwakuni, Also felt IV J on Shikoku, Right-Iateral surface faulting was observed for 9 kilometrises with horizontal displacement of 1.2 to 1.5 metres in the northerm part of Awaij-shima. Liquefaction also occurred in the epicentral area. Depth from broaded displacement setsmograms. NEIC Radicated energy from the P-wave firsi-motion solution: E.5.1.5x10/Him/8 NEIC Moment Insors octurion: Scale 10*Nm; Mr.O.9; NEIC Moment Insors octurion: Scale 10*Nm; Mr.O.9; NEIC Radicated energy from the P-wave firsi-motion solution: TATJ Tateyama 2 NEIC Radicated energy from the P-wave firsi-motion solution: Mat.161; Mw=1.70; Mw=0.33; Mw=0.46. Depth Hub Hachhijo jimi	3.05 45 Pn 3.75 249 Pn 3.77 60 Pn 3.81 234 Pn 3.89 65 Pn <i>eS</i> 3.89 76 Pn
Also feft IV J on Shikoku, "Anjoh-lateral surface faulting was observed for 9 kilometres with horizontal displacement of 1.2 to 1.5 metres in the northern part of Awaj-shima. Liquefaction also occurred in the epicentral area. Depth from broadband displacement seisonrograms. NEIC Radiated energy from the P-wave first-motion solution: 8.5s.1.6sr/01^VMm8 NEIC Moment tensor solution: s31, scale 10 ¹⁹ Nm; Mr/0.09; Mae.1.61; Map-1.70; Map-0.33; Map-0.46, Depth 15m; Prinorial avec: T.1.2 th 12*2 metres in the seisonrol and the seisonro	3.81 234 Pn 3.89 65 Pn 2.89 76 Pn 3.89 76 Pn
 Was observed for 9 kilometres with noncontal KMG Kumagaya displacement of 9 kilometres in the northerm part of Awaji-shima. Liquefaction also occurred in the epicentral area. Depth from broadband displacement seismograms. NEIC Radiated energy from the P-wave first-motion solution: S1, scale 101^s Nm; Mr0.09; MIL Vilgata 2 NEIC Moment tensor solution: s31, scale 101^s Nm; Mr0.09; MIL Vilgata 2 NEIC Moment tensor solution: s31, scale 101^s Nm; Mr0.09; ML Hachijö jima 15^c; Mn=0.33; Ma=0.33; Ma=0.46, Depth LU Hachijö jima Alkenso 	3.89 65 Pn eS 3.89 76 Pn
Awaj-Stima. Liguefaction also occurred in the epicentral area. Depth from broadband displacement seismograms. *NEIC Radiated energy from the P-wave first-motion solution: 8.5s.1.6sr10*Mm8 Meal.61; Mag-1.70; Mag-0.39; Mag-0.46. Depth Meal.61; Mag-1.70; Mag-0.39; Mag-0.46. Depth Mag-1.61; Mag-1.70; Mag-0.39; Mag-0.46, Depth Mag-1.70; Mag-0.70; M	3.89 76 Pn
 NEIC Radiated energy from the P-wave first-motion solution: B.5x1.6x10¹⁴ Min/8 NEIC Moment tensor solution: s31, scale 10¹⁹ Nm; M_r0.09; HJJ Hachijö jima Map.1.61; Map. 1.70; Map0.39; Map0.46, Depth HJJ Hachijö jima 15^{cm} Principal avec: T 1 2^{cm} P1012² Am 18^{cm} N 00 All Average 	4.00 82 Pn
NEIC Moment tensor solution: s31, scale 1019Nm; Mr0,09; Mea1.61; Meg-1.70; Mrg-0.39; Mrg-0.33; Meg-0.46, Depth 15km: Principal evec: 1 1 24 Pto124 Azm186* N 0.09	4.02 82 Pn 4.19 49 dPn
15km: Principal avas: T 174 Phil2° Arm186° N 000 All Allering	4.21 109 Pn
Plattin - Handberger and - 1 (17) (1912 Azm270) Bock double All Alleven	4.32 36 Pn
couple: Mo1.8x10 ¹⁹ Nm; NP1:φ ₅ 323°,δ73°,λ0°. NP2:φ ₅ 233°, UNZ Unzen dake	4.37 247 Pn
NEIC Fault plane solution: P waves. NP1:%232°,679°,2153°. UTS Utsunomiya	4.38 83 Pn 4.41 62 dPn
P Pig10",Azm282". The local mechanism is well UTS {I=I JMA}	S 4.43 238 Pn
controlled and corresponds to right-lateral strike slip faulting with a moderate reverse component. The KAKJ Kaldoka Outpot	4.47 262 Pn st 4.51 67 dPn
preferred fault plane is NP1 and has been identified as BSO3 Boso 3 the Nojima Fault.	4.51 85 Pn 4.65 271 Pn
ISC Maximum intensity I=XI MM, maximum peak ground NII Nilgata acceleration recorded 833 cm/sec2, approximate duration BS02 Boso 2	4.66 43 Pn
8-12 sec. (Extract from a report from the Bhabha JFY Yanaizu Atomic Besearch Centre Bombay, India) MGS1 Nagasaki 2	4.73 52 dPn
CSEM 16 ⁴ 20 ⁵ 46 ^m 54 ⁵ 2, 34 ² 70N×135 ¹ 00E, h15 ^{km} , Mw6.9, Mor ² 2 ⁹ -1 0×1018Nm, Fault place solution NP14-218 ⁹ 570 ⁹ MIT Mise	4.78 268 Pn
λ10". NP2:es226*,580°,λ169°, Principal Axes: T Pig15°, MIT (I=1 JMA)	4.75 00 Ph
HRVD 16 ^d 20 ^h 46 ^m 59 ^s 4 ₂ 0 ^s 1, 34 ^s 78N ₂ *00 ^k 134 ^s 99E ₂ *01, b20 ^{km} 4 ^{km} Control To 10 ^{km} 134 ^s 78N ₂ *00 ^{km} 134 ^s 99E ₂ *01,	4.90 87 Pn
GSN; LP body waves: s70,c187; Mantle waves: s58, JSU Suzuyama	4.91 233 Hn
Mrr0.61±.01; Mee1.90±.01; Mee-2.51±.01; Mrm-0.69±.03; CHO1 Chôsi	4.91 58 dPm 4.91 74 Pn
Pig22*, Azm186*; N 0.37, Pig67*, Azm22*; P = 2,61, Pig6*, JFT Otama	3 5.18 223 Pn 5.21 54 dPn
	5.32 60 dPn 5.46 46 dPn
h19km±2.2km, (h18km±1.0km;pP=P), n893, o1#03/827, JYA Atsumi	5.50 58 dPn 5.51 42 Pn
Southern Honshu JKC Kuchingerat	5.70 53 dPn 5.78 226 (S)
KOB KODE 0.18 41 P ⁻ 20 45 55.6 -1.1 JOU Okura KOB (I=VI JMA) S 20 46 59.1 -7 JYK Kaneyama	5.92 48 Pn 6.10 43 Pn
JAJ Awaji shima 0.24 207 20 46 57.9 +0.3 JIO Ouri DSA Osaka 0.42 72 dP* 20 47 00.0 -0.4 AKU Akita 2	6.40 51 dPn 6.58 37 Pn
JKS Kasal 0.46 339 cP* 20 47 00.0 -1.1 JMK Ichinoseki	6.59 41 Pn 6.62 47 dPn
ABU Abuyama 0.53 55 JP° 20 47 01 (2.4) -1.5 OFUJ Ofunato JHE Heguri 0.54 79 dP° 20 47 01.7 -0.9 JOM Ohasama	6.97 48 dPn 7.01 44 dPn
JWY Kouya 0.57 126 dP* 20 47 02.9 -0.1 MRKJ Morioka 2 JWM Minabe 0.75 160 cP* 20 47 07.2 +1.1 JAH Hinai	7.11 43 dPn 7.17 37 dPn
JWT Wachi 0.78 22 cP* 20 47 05.8 -0.9 SEO Seoul JAD Aida 0.82 298 dP* 20 47 06.5 -0.7 JIW Iwasaki	7.20 297 ePn 7.20 32 Pn
MZH2 Maizuru 2 0.89 19 cP* 20 47 07.70.9 MIYJ Miyako 2 JAI Aioi 0.90 213 cP* 20 47 09.6 +-0.9 JKZ Kuzumaki	7.38 45 dPn 7.38 41 dPo
OKA1 Okayama 0.93 277 P* 20 47 08.8 -0.4 JZK Kikaishima OKA1 (I=IV, JMA) S 20 47 22.3 -1 JTH Tarobata	7.58 216 (S)
JJS Sakalde 0.93 259 dP* 20 47 08.7 -0.6 JAM Amami Oshim MAL Maizunu 0.96 17 P* 20 47 08.1 -1.6 A0M2 Approx	a 7.68 219 cPn
MAI (I=IV JMA) S 20 47 20.2 -4 JSI Shiura JMT Mikata 0.98 335 P ⁺ 20 47 09.0 -1.0 MAC I Machineka 2	7.75 32 cPn
OWA Owase 1.07 117 dP* 20 47 11.5 -0.1 JTM Tenmabayas	ni 7.84 36 Pn
JWZ Kozaga 1.16 151 cPn 20 47 12.7 -0.4 JOR Okushj	8.26 23 P
HIK {IzV JMA} S 20 47 30.7 0 JTK Tokunoshim	8.53 219 P
	8.53 30 P 8.55 30 P
TSU1 Tsu -1.23 81 dPn 20 47 14.2 +0.1 HAKJ Hakodate 2	8.66 27 P
TSUI 150 - 1.23 81 dPn 20 47 14.2 +0.1 HakOdate 2 TSUI (151 VIA) - S 20 47 31.5 +1 JYM Yakumo TSRJ Tsuruga 1.25 38 cPn 20 47 14.3 0.0 JKB Kayabe	8.71 31 P
TSU1 TsU -1.23 81 dPn 20.47 14.2 +0.1 HakOdate 2 TSU1 (E1V JAA): S 20.47 31.5 +1 JVM Yakumo TSL1 Tsuruga 1.25 38 cPn 20.47 14.3 0.0 JKB Kayabe JMN Monobe 1.27 230 cPn 20.47 14.3 0.0 JKB Kayabe JKK pKrayoshi 1.30.310 Pn 20.47 14.5 -0.5 MRR Muroran	8.71 31 P 8.97 24 P 9.04 29 P
TSU1 TsU 1.23 81 dPn 20 47 14.2 +0.1 H4KJ Hakodata 2 TSU1 (I=IV JMA) S 047 14.2 +0.1 HMKJ Hakodata 2 TSU1 (I=IV JMA) S 047 31.5 +1 JVM Yakumo JMN Monobe 1.25 38 cPn 20 47 14.3 0.0 JKB Kayabe JMN Monobe 1.27 230 cPn 20 47 14.5 -0.5 MRR Muroran JKR Kurayoshi 1.30 310 Pn 20 47 14.5 -0.5 MRR Muroran TSR I[=1V JMA] S 20 47 14.5 -0.5 MRR Muroran TSR UT JMA S 20 47 34.8 0 SUT1 Suttsu	8.71 31 P 8.97 24 P 9.04 29 P eS 9.17 25 P
TSU1 Tsú 1.23 81 dPn 20.47 14.2 +0.1 Hákó Hakódata 2 TSU1 (EIV JMA) S 20.47 31.5 +1 JVM Yakumo TSRJ Tsuruga 1.25 38 cPn 20.47 14.3 0.0 JKB Kayabe JMN Monobe 1.27 230 cPn 20.47 14.3 0.0 JKB Kayabe JMN Monobe 1.27 230 cPn 20.47 14.3 0.0 JKB Kayabe JMN Monobe 1.27 230 cPn 20.47 14.5 -0.5 MRR Muroran TSR Taruga 1.30 310 Pn 20.47 14.5 -0.5 MRR Muroran TSR Taruga 1.38 37 Pn 20.47 34.8 0 SUT Tsuruga SUT T	8.71 31 P 8.97 24 P 9.04 29 P eS 9.17 25 P 9.19 29 eS 9.31 202 P
TSU1 Ta ² 1.23 81 dPn 20.47 14.2 +0.1 Hakod ate 2 TSU1 (i=U V/Ak) S 20.47 15.5 +1 JVM Yakumo TSRJ Tsuruga 1.25 38 cPn 20.47 14.3 0.0 JKB Kayabe JMN Monobe 1.27 20.0 cPn 20.47 14.3 0.0 JKB Kayabe JMN Monobe 1.27 20.0 cPn 20.47 14.3 0.0 JKB Kayabe JMN Monobe 1.27 20.0 cPn 20.47 14.3 0.0 JKB Kayabe JMN Konzohi 1.30 310 Pn 20.47 14.5 -0.5 MRR Muroran TSR Tsuruga 1.38 310 Pn 20.47 34.8 0 SUTtsurtan TSR (i=V V/AA) S 20.47 34.8 0 SUTtsurtan JG Jouge 1.56 274 Pn 20.47 14.6 -0.2 JMB Moboribetsu JHS Saijyo 1.65 5	8.71 31 P 8.97 24 P 9.04 29 P 6S 9.17 25 P 9.19 29 eS 2 9.31 202 P 9.64 139 P 9.65 139 P
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20 47 37.2 20 47 41.2	-0.2 +1.5
20 47 40.9 20 48 23.5	+0.1 +0.3 +6
20 48 28.3 20 47 40.6 20 47 42 7	-0.8
20 48 29.8 20 47 43.7	+9.
20 47 42.6 20 47 42.7 20 48 26	-0.3
20 47 42.0 20 48 31.1	-1.0 +9
20 47 43.0 20 47 43.7 20 47 44.3	0.0 +0.1 +0.4
20 47 43.1 20 48 25	-1.0
20 47 43.0 20 48 25.0 20 47 48.2	-1.1 0. +1.8
20 47 46.6 20 47 47.4 20 47 47.4	0.0
20 48 30.4 20 47 54	0
20 48 40.2 20 47 48.0 20 47 50.7	+9 -0.2 +2.2
20 47 50.0 20 47 52 20 47 51.1	0.0 +1.8 +0.1
20 47 54.0 20 48 42	+2.0
20 47 55.1 20 47 53 20 47 54.7	+3.1 -0.5 +0.8
20 47 55.9 20 47 56.0	-0.3
20 48 40.3 20 47 58.9 20 48 54	+0.8
20 48 00.6 20 47 57.7 20 47 59 3	+1.7
20 48 58.3 20 48 00.6	+7 +0.9
20 48 00.2 20 47 59.5 20 48 00.1	0.0 -1.3 -0.1
20 48 01.6 20 48 10.9	-1.3 +7.9
20 48 03.4 20 48 04.1 20 48 05.3	-0.3 +0.1 +0.7
20 48 03.1 20 48 04.5	-1.6
20 48 07.3 20 48 05.4	+1 +1.7 -0.9
20 48 06.6 20 48 07.2 20 48 06.2	+0.2 +0.8 -0.3
20 48 06 20 48 11.1	0.5 +0.8
20 48 11.1 20 48 11.8 20 48 14.5	+0.4 -0.5 +0.3
20 48 14.5 20 48 15.8 20 48 17 7	+0.1
20 49 28.9 20 48 21.3 20 48 24 2	+0.6
20 48 24.2 20 48 27.8 20 48 31.5	+0.3 +1.4
20 48 31.1 20 48 30.7 20 48 36.1	+1.0 +0.1 +0.5
20 48 36.4 20 48 37.7	+0.4
20 48 38.8 20 48 40 20 48 38.8	+1.3
20 48 41.8 20 48 41.5 20 50 21 5	+0.5 +0.2
20 48 45.4 20 48 44.6	+0.4 0.9
20 48 46.5 20 48 47.2 20 48 47.9	2.0+ 1.0+ 1.0+
20 48 48.7 20 48 51.8	+1.J 0.J
20 48 55.0 20 48 55.0 20 48 57.4	+0.1 +0.2
20 49 00 20 48 58.9 20 48 59 6	+2.7 +1.3
20 49 01.1 20 49 04.6	+1.4 +1.2
20 49 08 20 50 59 20 49 08	+30 +12 +1J
20 51 03.6 20 49 10.2 20 49 12 5	+2,1
20 49 12.5 20 51 02.7	-03
20 49 10.8 20 49 12.1 20 49 14.9	-0J +1.3
20 49 13 20 49 13.5	-0.1
20 49 14.9 20 49 17	0.1 +2.1
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20 49 26.0 20 49 31 20 49 26.1	-21
20 49 31 20 49 28.3	+21 -11
20 51 32.0 20 49 34.5	-1
20 49 32.1 20 49 29.1 20 49 30	-21
20 49 35.7 20 49 32.6	+21 -13
20 49 35.4 20 49 35.4 20 49 39.0	-31
20 49 46.0	43

8



(b) WKBJ Amplitude (model AK135)





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Used Stations (N = 718)



AK135 (Kennett et al., 1995; Montagner and Kennett, 1996)





EPICENTER SHIFTS (EHB VS ISC)

160°E

180°

160°W

140°E

100°E

120°E

(b)

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(a) WKBJ Seismograms (model AK135) T - 7.0/degree (sec)









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Azimuthal station correction for log-scaled amplitude anomaly

-

90°







Figure 2.15





30°

V



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, [.]



Averaged relative travel time residuals distribution map









Figure 2.21











latitude





CRUST 5.1: crustal types





Site effects and CRUST5.1(Mooney et al., 1998)



Amplification - Crust Type of CRUST5.1

Chapter 3.

A whole mantle P wave attenuation structure obtained from ISC amplitude data

3.1 Introduction

The global three-dimensional anelastic structure of the whole mantle remains poorly resolved compared to the elastic structure, although evidence for large lateral heterogeneity in the mantle attenuation of seismic waves has been abundant since the 1970's.

Many tomographic studies of attenuation have been done for local or regional earthquake data and they have contributed toward understanding the tectonics and dynamics in the crust and the upper mantle (e.g., Ho-Liu et al. [1988], Young and Ward [1980], Besana et al. [1997]). Investigations on the lateral variation of QScS, attenuation factor of multiple bounce ScSn waves, have shown large variations between ocean basins, subduction zones, and back-arc regions (e.g., Sipkin and Jordan [1980], Nakanishi [1979], Flanaghan and Wiens [1990]). Mikami and Hirahara [1981] investigated global variations of attenuative properties in the upper mantle by using WWSSN long-period P-wave records. Their estimate is very rough, but some correlation between the differential attenuation and heat flow were identified. The first investigation of the global heterogeneity of the Earth was done by Romanowicz et al. [1987]. They used fundamental spheroidal mode spectra from very long period GEOSCOPE records and obtained a pattern from degree 2 heterogeneity of shear-wave Q in the upper mantle. Subsequently, their method has been applied to various long-period data. Therefore, models in higher degree heterogeneity now exist for the upper mantle (e.g., Suda et al. [1991], Durek et al. [1993]). At present, QR19 (Romanowicz [1995]) is the best global threedimensional attenuation model for the upper mantle, with degree 6 heterogeneity for both vertical and horizontal directions. The heterogeneity of this model is consistent with tectonic features in shallower regions, and in deeper parts of the model the pattern shifts and becomes correlated with the hotspot distribution. (Romanowicz [1995]). However, these global models do not match each other very well. Investigations of whole mantle attenuation heterogeneity is still a developing field in seismology.

In this chapter, I applied a tomographic approach to obtain a whole mantle attenuation structure using the ISC amplitude data. The vast amount of ISC amplitude data have seldom

been used for structural investigations. However, I thought that dealing with the data set appropriately could yield valuable structural information. In the previous chapter, I introduced the amplitude station correction. Here I present the P-wave attenuation structure for the whole mantle by applying a tomographic method and station corrections obtained in Chapter 2 to the ISC short-period amplitude data. I divided an inversion process into two subprocess. First a joint inversion for determining source amplitudes and one-dimensional Pwave attenuation structure was applied to the ISC amplitude data corrected in Chapter 2, then I inverted for three-dimensional perturbations from the one-dimensional model. This is due to obtaining a numerically-stable solution of the attenuation structure.

3.2 Methodology of grid model attenuation tomography

3.2.1 Basic theory of attenuation tomography

A teleseismic P-wave amplitude of the i-th event at the j-th station can be expressed by

$$A_{ij}(f) = M_i(f) \cdot R_{ij} \cdot G_{ij} \cdot C_j(f) exp\left(-\pi f t_{ij}^*\right)$$
(3.2.1)

where $A_{ij}(f)$ denotes the observed amplitude at the frequency f, $M_i(f)$ is the amplitude, R_{ij} is the radiation pattern of the source mechanism, G_{ij} is the geometrical spreading, $C_j(f)$ is the site amplification, and t_{ij}^* is the attenuation factor,

$$t^{*} = \int_{raypath} V^{-1} Q^{-1}(f) ds \quad .$$
(3.2.2)

Since the focal mechanisms are known and the velocity structure and frequency are assumed in this investigation, the logarithm of the corrected equation of (3.2.1) and its discretized form become

$$log A_{ij} = log M_i + log C_j - \pi f \int V^{-1} Q^{-1} ds$$

= log M_i + log C_j - \pi f \sum_k V_k^{-1} Q_k^{-1} \Delta s_k (3.2.3)

where k indicates the position on the raypath and Δs_k is the step length for the ray tracing (Figure 3.1). Here the Q^{-1} value is assumed to be frequency independent in the analyzed frequency range. The principal unknown parameters are M_i , C_j and Q_k^{-1} in this inversion equation. The constructed inversion equation, however, needs more constraints because one degree of freedom still remains in the site effect term. Negishi [1998] investigated the highresolution attenuation structure in the epicentral area of the 1995 Kobe earthquake using this method and the grid model formulation, which expressed in the next section. He used the criterion that the site effects have a factor more than 2.0 due to the free surface amplification, and succeeded in obtaining fine tomographic images of P and S wave attenuation based on a spectral amplitude analysis. This criterion means that the smallest amplification factor of site effect should be 2.0. The difference between the actual smallest amplification and the assumed amplification (here 2.0) is represented by offsets for all of the source amplitude terms. But I already obtained the relative variation of site amplification factors (site effect terms, equation (2.3.7) in Chapter 2) for each station in the previous chapter, so using the station corrections, site amplification terms of equation (3.2.3) were excluded from the unknown parameters in this study.

3.2.2 Grid modeling formulation

The physical properties of the Earth's mantle varies more in the vertical direction than horizontal direction. So the velocity and attenuation structure in the Earth is usually expressed as a sum of the spherically averaged parameter-depth functions with 3-D perturbations. The spherical harmonic expansion representation has been used in most of the previous studies of the whole mantle velocity or attenuation structure (*e.g.*, Dziewonski [1984], Morelli and Dziewonski [1987], Romanowicz [1995]). This approach has an advantage that fewer parameters can express the global heterogeneous pattern, and the

-68-

harmonic model can be compared directly with other geophysical maps, such as gravity and magnetic field. However Inoue *et al.* [1990] pointed out that the capability of representing a distribution by a discrete parameterization model is essentially the same as representing one by harmonics. From the pioneering study of Aki and Lee [1976] and Aki *et al.* [1977], block modeling has been mainly used for local and regional tomographic studies. Recently the block modeling approach has become usable for whole mantle tomography, because of improvements in computer power and development of computational algorithms for solving large and sparse matrix problem. Recent investigations (*e.g.*, Inoue *et al.* [1990], Fukao *et al.* [1992], Kennett *et al.* [1998]) have clarified the whole mantle velocity structure by using fine block models.

On the other hand, Thurber [1983] developed a different approach to the modeling space. The 3-D heterogeneous structure is represented by a 3-D grid of nodes. Parameters (velocity or attenuation) vary continuously in all directions with linear B-spline interpolations among nodes. This representation expresses a smoothly-varying structure anywhere in the modeling space, while in a block configuration parameters change suddenly at block boundary. This is an advantage for three-dimensional ray-tracing, and it is easy to include laterally-varying discontinuities. Zhao *et al.*, [1992] adopted this approach to the Tohoku region in the northern part of Japan, and succeed in clarifying the fine velocity structure of the subducting Pacific plate and the mantle wedge by using pseudo-bending ray tracing (Um and Thurber [1987]) with heterogeneous discontinuities. I modified this grid modeling approach to an attenuation tomography problem.

Figure 3.2 shows schematically the block model and grid model representation. The constant- Q^{-1} block approach treats the Earth as a set of boxes within which the seismic attenuation is constant. In this modeling, the attenuation factor t^* (equation (3.2.2)) becomes

$$t^* = \sum_{l} \frac{L_l}{V_l} Q_l^{-1} = \sum_{l} t_l Q_l^{-1}$$
(3.2.4)

where V_l , L_l and t_l are the velocity, length of ray-segment, and travel time through the *l*-th block, respectively. As indicated above, ray tracing and segmentation of rays depend on the configuration of blocks in this approach.

-69-

In the grid configuration, the problem has a different form. As shown in Figure 3.2, t^* is represented by the integral along the raypath that is determined independently from the grid node configuration. Q^{-1} on the raypath is interpolated by the Q^{-1} at each grid node surrounding the raypath. The unknown modeling parameter to be solved for is the Q^{-1} at each grid node. The Q^{-1} value at a given point (r, θ, ϕ) is represented by the B-spline interpolation of the peripheral eight nodes, as follows

$$Q^{-1}(\phi, \lambda, h) = \sum_{l=1}^{8} Q_l^{-1} w_l$$

$$= \sum_{i=1}^{2} \sum_{j=1}^{2} \sum_{k=1}^{2} Q^{-1}(\phi_i, \lambda_j, h_k) \left\{ \left(1 - \frac{|\phi - \phi_i|}{|\phi_2 - \phi_1|}\right) \left(1 - \frac{|\lambda - \lambda_j|}{|\lambda_2 - \lambda_1|}\right) \left(1 - \frac{|h - h_k|}{|h_2 - h_1|}\right) \right\}$$
(3.2.5)

where w_l is the weighting function, ϕ is the latitude, λ is the longitude, h is the depth, and ϕ_i , λ_j , h_k represent the coordinates for the eight grid nodes surrounding the point (ϕ, λ, h) . $Q^{-1}(\phi_i, \lambda_j, h_k)$ is the inverse of quality factor at the grid node (see Figure 3.3). The velocity at the position (ϕ, λ, h) is also expressed by the same formulation mentioned above,

$$V(\phi, \lambda, h) = \sum_{l'=1}^{8} V_{l'} u_{l'}$$

$$= \sum_{i'=1}^{2} \sum_{j'=1}^{2} \sum_{k'=1}^{2} V(\phi_{i'}, \lambda_{j'}, h_{k'}) \left\{ \left(1 - \frac{|\phi - \phi_{i'}|}{|\phi_2 - \phi_1|}\right) \left(1 - \frac{|\lambda - \lambda_{j'}|}{|\lambda_2 - \lambda_1|}\right) \left(1 - \frac{|h - h_{k'}|}{|h_2 - h_1|}\right) \right\}$$
(3.2.6)

where $u_{l'}$ is the weighting function for velocity model. Here different configurations of grid arrangement can be used for the velocity and attenuation model. Substituting equations (3.2.5) and (3.2.6) into (3.2.4), t^* becomes

$$t^{*} = \sum_{k} V_{k}^{-1} Q_{k}^{-1} \Delta s_{k}$$

$$= \sum_{k=1}^{N} \left[V_{k}^{-1} \sum_{l=1}^{8} Q_{l}^{-1} w_{lk} \right] \Delta s_{k}$$

$$= \sum_{k=1}^{N} \left[\left(\sum_{l'=1}^{8} V_{l'} u_{l'k} \right)^{-1} \sum_{l=1}^{8} Q_{l}^{-1} w_{lk} \right] \Delta s_{k}$$
(3.2.7)

where N is the number of segments of the raypath, and w_{lk} is the interpolation weight for that node. The inversion equation (3.2.3) in the grid modeling formulation then becomes

$$\log A_{ij} = \log M_i + \log C_j - \pi f \sum_{m=1}^{M} \sum_{k=1}^{N_y} \frac{\Delta s_k^{ij}}{V_k^{ij}} \sum_{l=1}^{M} w_{lkm}^{ij} \delta_{lm} Q_l^{-1}$$
(3.2.8)

where A_{ij} is the observed amplitude with corrections for geometrical spreading and source mechanism, M_i is the unknown source amplitude of the i-th event, C_j is the unknown site amplification factor at the j-th station, f is the frequency (assumed to be 1.0 in this study), N_{ij} is the number of segments along the raypath from the i-th source to j-th station, Δs_k^{ij} is the length of the k-th ray-segment, V_k^{ij} is the velocity at the k-th ray-segment, w_{lkm}^{ij} is the interpolation weight at the k-th position on the ray for the l-th grid node, δ_{lm} is the Kronecker delta, and Q_l^{-1} is the unknown parameter of attenuation at the l-th grid node. This inversion equation seems complex but it is linear. The above equation represents one amplitude observation, and I convert it to a matrix equation Gm = d, where G is a coefficients matrix, m is an unknown parameter matrix and d is a data matrix, respectively.

The equation (3.2.8) can be solved directly because of its linear form. However such direct solution is often trapped by local minima and sometimes becomes smaller than 0, especially in the problem of the large-scale inversion matrices. Therefore I solve the one-dimensional attenuation structure as a reference model first, and then calculate the perturbations from the reference model to obtain the stable solutions in this study. This approach have been often applied to the local or regional attenuation tomographic studies (*e.g.*, Solomon and Toksöz [1970], Scherbaum [1990], Sanders [1993]). When we know the reference values for each parameter (souece amplitude, site amplification and Q^{-1} model), the inversion equation (3.2.8) can be modified, using the reference attenuation model Q_0^{-1} , to the following form;

$$\Delta \log A_{ij} = \Delta \log M_i + \Delta \log C_j - \pi f \sum_{m=1}^{M} \sum_{k=1}^{N_{ij}} \frac{\Delta s_k^{ij}}{V_k^{ij}} \sum_{l=1}^{M} w_{lkm}^{ij} \delta_{bn} Q_{0l}^{-1} \left(\frac{\Delta Q^{-1}}{Q_0^{-1}}\right)_l$$
(3.2.9)

where $\Delta \log A_{ij}$ is the logarithm of the amplitude ratio of the observed amplitude to the calculated amplitude from the reference parameters, $\Delta \log M_i$ and $\Delta \log C_j$ are the unknown source amplitude and site amplification ratio, respectively (actually $\Delta \log C_j = 0$ in this study because we already set the site effect term in Chapter 2 as the site amplification). In this

formulation, the Q^{-1} perturbation from the reference model, $\left(\frac{\Delta Q^{-1}}{Q_0^{-1}}\right)_l$, is the unknown parameter to be solved. I used (3.2.9) formulation in this study.

3.2.3 Smoothness constraint

Frequently smoothness is introduced to modeling of an under-constrained problem (e.g., Inoue et al. [1990], Lees and Crosson [1989]). In our case, smoothness constraints can be imposed by minimizing a measure of the roughness of the model, where I have chosen the roughness to be the second differential operator in the horizontal plane. This is just the Laplacian operator ∇^2 in vector notation. I augment the system of equations to be solved in the least squares method,

$$\begin{bmatrix} G\\ \alpha D \end{bmatrix} m = \begin{bmatrix} d\\ 0 \end{bmatrix}$$
(3.2.9)

where D is the two-dimensional, finite difference Laplacian operator applied over horizontal planes in our model. Solving (3.2.9) by least squares is equivalent to a weighted minimization of the Laplacian operator at each point of the model in horizontal planes. In two dimensions this corresponds to the following equation for the j-th grid:

$$4(j - th _grid_parameter) - \sum (adjacent_parameter)$$

= $4m_j - (m_{j-1} + m_{j+1} + m_{j-n} + m_{j-n})$
= 0 (3.2.10)

where n is the number of grids in each latitude. In polar coordinates the element of the roughness matrix D becomes,

$$D_{i} = \begin{cases} -2\left(1 + \frac{1}{\sin^{2}\theta_{j}}\right) & \{i = j\} \\ \frac{1}{\sin^{2}\theta_{j}} & \{i = j - 1, j + 1\} \\ 1 & \{i = j - n, j + n\} \\ 0 & otherwise \end{cases}$$
(3.2.11)
where θ_j is colatitude of the j-th grid. Using the adjustment system, we will minimize the following function

$$|Gm - d|^{2} + \alpha^{2} (m^{T} D^{T} Dm) = |Gm - d|^{2} + \alpha^{2} ||Dm||^{2}$$
(3.2.11)

where i represents the Euclidean norm.

In the equation (3.2.11), the positive parameter α is used to adjust the relative weight of roughness. In the inversion there is a trade-off between α and the misfit reduction. This hyperparameter α is often determined subjectively because we know nothing about it *a priori.* One method to determine the parameter is using ABIC (Akaike's Bayesian Information Criterion) (Akaike [1980]) which has been recently used in some fields of inverse problems. However, the computation of ABIC is almost impossible in such large problems as our tomographic inversion, since it requires trailing procedures including calculation of the Hessian matrix $G^T G$. Moreover, Nishizawa *et al.* [1994] pointed out that the ABIC often leads to wrong results when the number of data is not much larger than the number of unknown parameters, such as in tomography problems. Recently Nishizawa and Noro [1995] and Aoike *et al.* [1998] applied the Extended Information Criterion (EIC) for determining an optimum model in seismic velocity tomography. The EIC is estimated by a numerical simulation based on bootstrap statistics. This method can be used even if the number of unknowns is large, but it needs tens of trial computation of the inversion.

I applied the simplified cross validation approach (Inoue *et al.* [1990]) in this study. The generalized cross validation (*leave-one-out cross-validation*) requires large computational efforts, requiring the number of trial runs equal to the number of data. However, if we have a vast amount of data, the cross validation score can be simplified as follows. First we divide the original data tod₁ and d₂ by random sampling. Then the inversion process with a trial hyperparameter α is applied to data d₁ and we estimate a model $m_{1\alpha}$. This model should predict the remaining data d₂, which is independent of the inversion process, if model $m_{1\alpha}$ represents true structure well. So we calculate the synthetic amplitude of the data d₂ by using the model $m_{1\alpha}$, and the approximate cross validation score is given as,

$$Sc(\alpha) = \left\| d_2 - G_{2\alpha} \left(G_{1\alpha}^{-1} d_1 \right) \right\| = \left\| d_2 - G_{2\alpha} m_{1\alpha} \right\| .$$
(3.2.12)

I found the hyperparameter α that minimizes $Sc(\alpha)$ by a grid search. If data set d_1 is taken to be too small, the results tend to depend on the size of d_1 and the estimated optimal values become biased. On the other hand, if the size of d_2 is too small, the estimated values become unreliable. Figure 3.4 is the results of the cross validation test using three different sizes of d_1 and d_2 , d_1 : d_2 is 2:1, 5:1 and 7:1. These scores are normalized by the score with no smoothness for each test. The three curves show approximately the same minimum position around the hyperparameter 2 or 3. I adopted the value $\alpha=2.5$ in this study.

3.2.4 LSQR inversion algorithm

Many investigators have adopted the damped least square method (*e.g.*, Aki *et al.* [1977]) or Generalized nonlinear inversion (Tarantora and Valette [1982]) for tomographic analysis. These methods, however, are impracticable in our calculation because of the huge size of the inversion matrices and limitation of computer power. Therefore most of the recent work on large-scale tomography adopt iterative algorithms to solve the equation system, such as the Algebraic Reconstruction Technique (ART) (*e.g.*, Nakanishi [1985], Hirahara [1988]) and the Simultaneous Iterative Reconstruction Technique (SIRT) (Hager and Clayton [1989]). These are mainly based on backprojection techniques. These methods have been used by many investigators, because the calculation process is simple and easy to understand. However, these methods have the undesirable property that they do not converge to the exact least squares solution (Menke [1989]).

To solve the linear equation, I adopted the LSQR method (Paige and Saunders [1982]), which is one kind of conjugate gradient methods. This method is a superior algorithm to solve large and sparse matrix problem, because of its fast convergence and ability to give exact solutions. The LSQR algorithm is briefly described as follows (Nolet [1987]).

$$m_{0} = 0$$

$$\alpha_{0} = |G^{t} \cdot d| \beta = |d|$$

$$v_{0} = \frac{1}{\alpha_{0}} (G^{t} \cdot d) u_{0} = \frac{1}{\beta_{0}} d$$

$$w_{0} = v_{0}$$

$$\rho_{0} = \alpha_{0}, \phi_{0} = \beta_{0}$$

loop i = 1, n

$$\beta_{i} = |G \cdot v_{i-1} - \alpha_{i-1}u_{i-1}|$$

$$u_{i} = \frac{1}{\beta_{i}} (G \cdot v_{i-1} - \alpha_{i-1}u_{i-1})$$

$$\alpha_{i} = |G^{t} \cdot u_{i} - \beta_{i}v_{i-1}|$$

$$v_{i} = \frac{1}{\alpha_{i}} (G^{t} \cdot u_{i} - \beta_{i}v_{i-1})$$

$$m_{i} = m_{i-1} + \frac{\rho_{i-1}\varphi_{i}}{\rho_{i-1}^{2} + \beta_{i}^{2}} w_{i-1}$$

$$w_{i} = v_{i} + \frac{\alpha_{i}\beta_{i}}{\rho_{i-1}^{2} + \beta_{i}^{2}} w_{i-1}$$

$$\rho_{i} = \frac{\rho_{i-1}\alpha_{i}}{\sqrt{\rho_{i-1}^{2} + \beta_{i}^{2}}}, \varphi_{i} = \frac{\rho_{i-1}\varphi_{i}}{\sqrt{\rho_{i-1}^{2} + \beta_{i}^{2}}}$$
(3.2.13)

end loop

where v_i are the Lanczos vectors (Lanczos [1950]) and n is the number of local iteration, which is the same as the number of unknowns. r_i is the absolute length of the residual vector Gm - d, and m_i indicates the solution of i-th local iteration. Figure 3.5 is the simple LSQR program coded in Ratfor (Nolet [1987]). Details of this algorithm are explained by van der Sluis and van der Vorst [1987].

3.2.5 Resolution

In seismological tomographic studies, especially for global problems. hypocenters and stations are not distributed uniformly. Consequently, ray paths sample grids unevenly, and the density of ray sampling has large fluctuations. The solutions are not reliable at grid points that have only a few samples. Moreover, systematic inclinations of ray sampling directions often cause improper results even if the ray sampling is dense. Therefore, it is necessary to investigate not only the solution itself but also the resolution of the results for objective evaluations. For the matrix inversion techniques, such as the damped least squares or generalized inverse method, covariance and resolution matrices (C'_m and R) can be computed with the solution, using the following equations

$$C_{m}^{'} = \left(G^{T}G + \alpha^{2}D^{T}D\right)^{-1}$$
(3.2.14)

$$R = C_m' G^T G.$$
(3.2.15)

There is important difference in these matrices from that in the normal damped least squares. The covariance and resolution matrices $C_m^{'}$ and R are not symmetric because $G^T G$ and $D^T D$ are not commutative.

The actual computation to obtain the inverse matrix of $G^T G + \alpha^2 D^T D$ is, however, impossible due to the huge size of the matrices in our study. Moreover, these computations cannot be made simultaneously with the solution for the iterative back-projection method. Nakanishi and Suetsugu [1986] and Hirahara [1988] produced a new formulation to obtain resolutions for the parameters by an iterative tomographic inversion method. But this method also takes much computation time, and the time for one column of the resolution matrix is the same as the time for one whole solution. So I adopted the synthetic test called the "checkerboard resolution test", as applied in Inoue *et al.* [1990] and Zhao *et al.* [1992].

The procedure for this method is briefly listed as follows. First an attenuation model with a checkerboard pattern in both the horizontal and vertical coordinates is constructed. The checkerboard pattern is expressed as

$$m_{check} = p \sum_{k} c_k e_k \tag{3.2.16}$$

where p is the perturbation size of the checkerboard pattern, c_k are the coefficients 1 or -1 defining the pattern, and e_k is a unit vector, in which only the k-th grid has the unit value. Then, synthetic data set for the checkerboard structure is produced using the data kernel for the real data set G,

$$d_{syn} = Gm_{check} \tag{3.2.17}$$

Finally, the synthesized data d_{syn} is backprojected into the Earth to reconstruct the checkerboard pattern. The reconstructed image can be written as

$$m_{back} = pR \sum_{k} c_k e_k = p \sum_{k} c_k \hat{e}_k$$
(3.2.18)

where \hat{e}_k is not a unit vector but the point spread function at the k-th grid. These coefficients clearly indicate the checkerboard resolution. If non-diagonal elements of the vector \hat{e}_k can be ignored, the ratio m_{back} to m_{check} is the same as the diagonal element vector of the resolution matrix R. The obtained structure from the synthetic data set will show a clear checkerboard pattern where the resolution is good. And in 'he region with poor resolution, the obtained structure becomes a blurred pattern or no pattern.

3.3 One-dimensional attenuation structure and setting for tomographic inversion

3.3.1 Setting of data and modeling space

First a one-dimensional P-wave attenuation structure was calculated. I analyzed the dataset that corrected for radiation pattern of the source mechanism and geometrical spreading of the 1-D velocity structure in Chapter 2. Figures 3.6 and 3.7 show the geographical distribution of stations and events, respectively. Figure 3.8 is the histogram of the bottoming depths of the raypaths. Worse resolution is expected in the uppermantle because body waves

primarily sample the structure near their bottoming depths (Stewart [1981], Tajima and Grand, [1998]) and there are no raypaths with bottoming depth shallower than 700 km. Of course there is no resolution (and no unknown parameters) in the lowermost mantle deeper than 2700 km because no data are sampled there.

We cannot apply observation errors to the inversion because there is no information in the ISC database, so I adopted a robust estimate by applying a weight which is a function of the relative log-amplitude anomaly determined in Chapter 2. The weight w is expressed as the following function of the relative log-amplitude anomaly r,

$$w(r) = \begin{cases} \left[1 - \left(\frac{r}{2.6}\right)^2\right]^2 & , |r| \le 2.6 \\ 0 & , |r| > 2.6 \end{cases}$$
(3.3.1)

This function is called the Biweight estimation function, which is one kind of M-estimation method (Turkey [1977], Nakagawa and Koyanagi [1982]). The threshold value 2.6 is set to twice the standard deviation of the relative log-scale amplitude anomalies in Figure 2.12 in Chapter 2.

Usually station corrections are not applied to data in velocity tomographic studies except for elevation and telemetry delays. This is because site effects for travel times do not vary rapidly among close stations, and time delays from site effects are smaller than the velocity heterogeneity on a global scale. Such time lags are indicated as low- or high-velocity anomalies at the nearest grid to each station. The site amplification factor, however, has large fluctuations with large values as shown in Chapter 2. Therefore, I applied station corrections to the amplitude data before the inversion. The resultant site effect terms (equation (2.3.7), Figure 2.12 in Chapter 2) was used for the correction terms, and site amplification terms were excluded from the unknown parameters. Finally, 3,461 parameters (16 Q_p^{-1} and 3445 source amplitudes) remained as unknowns.

I set the modeling grid points at 16 different depths; 12, 51, 110, 190, 290, 410, 551, 712, 893, 1095, 1317, 1559, 1821, 2104, 2407 and 2730 km. The grid interval varies with depth, with the interval becoming larger with depth. Figure 3.9 shows the grid configuration

and sampling count at each depth. The step length for the ray tracing, Δs_k in equation (3.2.8), is set to 20 km in this study. A ray samples grid nodes at each step length ,and the step length is smaller than the interval of modeling grid, so the sampling count in grid model tomography is much larger than the hit count in block model tomography. The Q_p^{-1} at any depth in the model is calculated by linearly interpolating the Q_p^{-1} at the upper and lower target depths.

3.3.2 Result of one-dimensional inversion

Figure 3.10 and Table 3.1 show the resultant one-dimensional Q_p^{-1} structure in the mantle. In the computation process, an inequality condition constraint (Menke [1989]) was included in the inversion for obtaining positive Q_p^{-1} values. The AK135 model of Montagner and Kennett [1996], which was obtained from analysis of the Earth's free-oscillations, is also shown for comparison. The general tendency of high-attenuation in the upper mantle and relatively low-attenuation in the lower mantle can be seen, and this pattern is similar to AK135 and other attenuation models (Figure 3.11). Mikami and Hirahara [1981] analyzed a large number of WWSSN long-period P-wave records, and they concluded that the body wave data generally support the SL8 model (Anderson and Hart [1978]), which has low Q (200-280) layers in the upper mantle and increasing Q zones from 350 km to the lower mantle. This is consistent with our results. Q_p^{-1} has a strong frequency dependence between the Earth's free-oscillation periods to the short-period body wave range, with stronger attenuation in the higher frequency (Sato [1991]). Therefore, an offset between my resultant model and AK135 is expected, but such trend is not seen. All of the event occurred in the upper mantle and about 70 % of the rays pass through the lower part of the lower mantle (see Figure 3.8). This means that the separation between source terms and structure terms might be incomplete and it is possible that the bias is absorbed in the source amplitude terms. Figure 3.12 is a lot of the resultant source amplitude versus ISC magnitude. We can see the positive relation between them, despite the fact that no magnitude information was included in the inversion. This indicates that the simultaneous inversion gives fairly reasonable results. But the absolute

values are meaningless because they includes not only magnitude effects but also the bias of the attenuation structure and the offsets of the station amplification corrections.

3.3.3 Settings and conducting the tomographic inversion

The configuration of the three-dimensional grid nodes is shown in Figure 3.13. There are 17 nodes spaced in latitude, 36 in longitude, and 16 in depth. The total number of nodes is 9,794 including nodes on the North- and South-Poles on each layer. The grid interval is 10° for both latitude and longitude, and in the vertical direction the same spacing was used as in the one-dimensional inversion. Smaller thickness intervals are used to model the greater complexity at shallower depths, because we know a priori that the various model parameters (velocity, attenuation, density, etc.) vary more rapidly at shallow depths for both the vertically heterogeneous model and its lateral variations. The deepest grid nodes (2730 km) were used only for interpolating and excluded from the unknowns in this tomographic process.

As expressed in equation (3.2.4), the attenuation factor t^* is proportional to the inverse of (velocity x Q factor). This means there exists a strong trade-off between velocity and Q factor in attenuation tomographic problems. I used the whole-mantle tomographic model of three-dimensional P-wave velocities (Obayashi *et al.* [1997]) for calculating attenuation factors. Figure 3.14 shows the velocity model. These figures are made from the original block data, with the mantle divided into 32 x 64 x 16 (latitude x longitude x radius) blocks. This velocity model is parameterized by 5.625 x 5.625 degree blocks globally and a vertical configuration of layers that is different from the grid configuration used in our attenuation tomography. The grid model tomography, however, can accommodate the interpolation of Q_p^{-1} and Vp from different grid spacings, because the expression of Q_p^{-1} and Vp at optional position is done independently. I used the velocity model in its original configuration. The heterogeneous velocity model was only used for obtaining velocity values in constructing the inversion matrices, while the ray tracing and the calculation of geometrical spreading were performed in the spherical homogeneous model.

3.3.4 Checkerboard resolution test

Prior to inverting the actual data, I examine the checkerboard resolution test. Figure 3.15 shows the horizontal pattern of the initial checkerboard. Two kinds of patterns were tested in order to see the resolutions at different wavelengths, $3 \times 3 \times 2$ grids (upper), and $6 \times 6 \times 3$ grids (lower) in latitude x longitude x depth. Incidentally, a still smaller checkerboard pattern ($1 \times 1 \times 1$) cannot be applied to the grid modeling, because parameters are obtained by interpolation of adjacent grids and this procedure would cancel out the contrast. Since the maximum perturbation of the quality factor is approximately 50 to 60 % from the one-dimensional model in the upper mantle (Romanowicz [1995]), I set the test patterns to $\pm 60 \%$ perturbations from the one-dimensional model obtained in the previous section. The synthetic amplitudes are calculated for the ray paths in the actual data set and then they are backprojected into the mantle. The hyperparameter for smoothness constraint is the same value as in the real data inversion.

Figures 3.16 and 3.17 show the reconstructed image of the small (3 x 3 x 2) and large (6 x 6 x 3) patterns, respectively. Figure 3.18 is the map showing distributions of the sampling count. Generally the resolution in the large scale checkerboard is better than in the small scales. The resolutions have a correlation with the fluctuations of sampling count, where regions of dense sampling are well resolved. In the depth rage of 12 - 110 km, the small scale resolution is better at only limited area, around Japan. The large scale resolution is better around the Pacific, Europe, and India. However, the oceans and the northern part of the Eurasia continent are not well resolved. In the depth range of 190 - 410 km, the resolution of both small and large scale patterns are good around the Pacific. In the depth range of 551 -893 km, the resolution increases, except for the oceans and the high latitude side of the southern hemisphere, mainly due to the large amount of data that have bottoming points around this depth range (Figure 3.8). In the depth range of 1,095 - 1,559 km, the well resolved area moves to the central part of Pacific ocean and the resolution in continental regions decreases for the small scales. The large scale resolution is quite good in this range. In the depth range of 1,821 - 2,407 km, the resolution is good in middle to east Eurasia and the central Pacific ocean. This pattern is almost the same as the distribution of sampling counts.

As shown in these figures, the resolution is extremely poor at the depth of 2.104 km, despite the fact that the sampling is not sparse (Figure 3.18). As shown in the equation (3.2.9), the coefficients for the unknowns of the attenuation structure include the reference value of Q^{-1} , and the reference Q^{-1} at the depth of 2104 km is much smaller than that at the depths of 1,821 and 2,407 km (Fig. 3.10, Table 3.1). This means that the actual weighting of the inversion equation became smaller at the depth of 2,104 km than that at the neighbor depths. Therefore the grid at the neighbor depths absorbed the effects at the depth of 2.104 km, and the range of the perturbations is smaller than that at the other depths. This problem might be solved by introducing some constraints, such as vertical smoothness or weighting factor for each depth. However it increases *a priori* parameters in the inversion and makes the inversion problem more complex. I did not apply any particular operation in the inversion process because the one-dimensional Q_p^{-1} at this depth is reliable.

The polar regions, where the absolute value of latitude is larger than 80° , are not shown because of poor resolution in all depths. This is due to the effect of the smoothness constraint, because the interval of the grid nodes in the iongitudinal direction is very narrow in polar regions. This problem was also seen in the other whole mantle tomographic study with block modeling (Inoue *et al.* [1990]).

3.4 Tomographic result

The three-dimensional P-wave attenuation structure, QPB3DV2, was obtained by using the algorithm developed in Section 3.2. Only the nodes sampled by more than 10 rays were solved for in the inversion. The actual computation was performed on a personal computer with Dual Pentium II CPU (400 MHz x 2) with 512MB on-board memory. All the calculations of solutions, cross validation, and checkerboard resolution tests were done on this machine. Since the approximate size of the inversion matrices are over 450 megabytes, the

inversion matrices and the smoothness matrix (G, d, m and D) can be kept in memory. The other data and matrices (e.g., temporary matrix for reordering in LSQR process) were stored on the hard disk. The data access on the hard disk takes about 40 times as that in memory. The computation time for one inversion process is approximately 105 minute.

Figures 3.19 and 3.20 show the resultant Q_p^{-1} perturbations from the one-dimensional model and their standard errors, respectively. Red with large positive values of Q_p^{-1} perturbations and blue shows negative perturbations indicating high and low attenuation, respectively. The color-scale ranges from -60 % (blue) to +60 % (red) and values exceeding these are clipped. The complete table of the attenuation structure is listed in Appendix C. The locations of hotspots according to Richards *et al.* [1988] are also shown in Figure 3.19. The P-wave velocity perturbation obtained by Obayashi *et al.* [1997] is shown in Figure 3.21 for comparison. Vertical cross sections of all information along great circles are also shown in Figures 3.22 to 3.27 (Figure 3.22; Q_p^{-1} perturbations, Figure 3.23; P-wave velocity perturbations obtained by Obayashi *et al.* [1997], Figure 3.24; result of the checkerboard test with 3 x 3 x 2 pattern, Figure 3.25; result of the checkerboard test with 6 x 6 x 3 pattern, Figure 3.26; sampling count, and Figure 3.27; standard error of Q_p^{-1} perturbations). The positions of the cross sections are shown as circles in an inset world map. These maps do not include the D" layer because I did not solve the solution for that region.

There is a high attenuation area in the western part of North America (California to Mexico) in the crust and the uppermost mantle. This high attenuation gradually becomes weak with depth, and it disappears suddenly at the depth of 893 km (cross sections (d), (h)). This anomaly coincides with the distribution of hotspots, such as Yellowstone and Juan de Fuca/Cobb Seamount (Richards *et al.* [1988]). According to the velocity tomography, the back-arc basins in the Circum-Pacific belt exhibits large slow anomalies of about 1.5-2.5 % (Inoue *et al.* [1990]) in the upper mantle. These low velocity anomalies are not consistent with the resultant attenuation pattern. However, the high attenuation anomaly might be a smaller scale feature smeared over a large area, because only large scale patterns were resolved in the checkerboard resolution test. A small region of high attenuation exists in the central part of Europe from the crust to over 800 km depth. At the depth of 190 km, high

attenuation appears around the Black Sea. This anomaly shifts to the east with depth, and disappears beneath the Caspian Sea around the depth of about 1,000 km.

The most remarkable high attenuation anomalies exist around the Southern Pacific (Fiji, Tonga and Polynesia). These attenuated regions have good relation to the distribution of hotspots. The regions around the Tonga and Fiji islands are characterized by high attenuation down to 300 km or deeper (cross sections (a), (d)). This anomaly seems to disappear at about 400 km, but it can be seen again at depths of 1,300 to 1,800 km in the lower mantle. It is possible that the anomaly is too small (or narrow) in the upper part of the lower mantle and it cannot be resolved in this tomography. This anomaly in the upper to lower mantle is also seen in the P-velocity tomography as a low velocity region (Obayashi et al. [1997]). The low velocity anomaly spreads to Tasmania and the southern part of New Zealand, while this larger extent of the anomaly does not exist in the attenuation tomography. No characteristic feature is seen in these areas (< -30° in latitude) in the attenuation image, because of the low resolution there. On the other hand, the high attenuation anomaly can be seen through all depths from 51 km to 1,317 km around the Polynesian region. This anomaly shifts to the northwest and combines with the high attenuation region under Tonga and Fiji down to the depth of 1,821 km. It is likely an upwelling which originates in the deeper part of the lower mantle.

The regions around the East Asia show high attenuation in the crust and the uppermost mantle. It shifts to the northern part of China in the upper mantle then spreads out under Southeast Asia at depth greater than 410 km. This anomaly continues down to the deeper part of the lower mantle beneath the Philippines and Papua New Guinea region (cross sections (e) and (f)). A low velocity anomaly is also seen in the velocity tomography (Obayashi *et al.* [1997]) there, but no hotspot is found there.

High attenuation is found in a wide area in the southern Indian Ocean in the upper mantle. This exists at the top of the transition layer and shifts to the Great African Rift Valley in the middle to lower mantle (cross section (d)), although the resolution is poor. A high attenuation anomaly is also seen under the northern Atlantic Ocean at depths of 1,559 to 1,821 km, despite the poor resolution.

Some low attenuation anomalies are found beneath the stable continents. The most remarkable low attenuation anomaly can be confirmed in South Asia in the upper mantle. The clear elongated pattern of low attenuation exists from West Asia to Australia. The shape of the anomaly is consistent with the high velocity pattern in the whole mantle velocity tomography constructed by Kennett *et al.* [1998]. A remarkable region of low attenuation can be seen at depths of 190 to 410 km in the coastal side of the Western Pacific, which may be due in part to the existence of subducting slabs. Such patterns were also found in the P-wave velocity structure of Inoue *et al.* [1990], but their depth for the high velocity region is deeper (478 to 629 km) than our results. However, there is high velocity materials at depths of 120 to 180 km in the S-wave velocity structure of Suetsugu and Nakanishi [1987], and this fits with our result.

There is a low attenuation anomaly beneath South America and the eastern part of North America in the upper to middle depths of the mantle. Also there exists a remarkable low attenuation body beneath the Eurasia Continent in the lower mantle (cross section (h)). These regions have better resolution and these anomalies are reliable. A low attenuation root is also found beneath central Africa, whose absolute motion with respect to the mantle is very slow (Minster and Jordan [1978]). A low attenuation body beneath the Eurasia continent spreads out at the depth of 2407 km. The shape of this body is, however, the same as the extent of the areas of better resolution, so the reliability of this anomaly is low.

We find a clear low attenuation anomaly beneath Japan and China in the lower mantle, as shown in the cross sections (b), (c) and (f). The resolution of this area is relatively good, so this anomaly is reliable. But no high velocity anomaly can be seen there in the model of Obayashi *et al.* [1997]. There is a low attenuation anomaly along the extension of the subduction zone in the Tonga-Kermadec region in the lower mantle with good resolution. This suggests the existence of slab penetration into the lower mantle (Creager and Jordan [1984]). This anomaly can be seen in P-wave (Inoue *et al.* [1990]) and S-wave velocity structures (Grand [1987]) as high velocity anomalies.

Previous tomographic models of the whole mantle show predominantly degree 2 patterns, with low velocities in the central part of the Pacific Ocean and beneath Africa (*e.g.*,

Masters *et al.* [1982], Inoue *et al.* [1990]). However, a large heterogeneous pattern of degree 2 is not clear in our model. This is due to few data and less resolution around Africa.

3.5 Discussion

There are some reasons why the anelastic stricture of the mantle should be of fundamental interest to geophysics. The most important reason for considering threedimensional attenuation structures is that it may provide constraints on mantle dynamics that are complementary to those inferred from elastic modeling (Romanowicz [1995]). The absorption of seismic waves is affected by mainly thermal conditions, in other words, heterogeneity of absorption of waves maps the thermal structure in the Earth. The effects of temperature anomalies on attenuation and velocity are different. Figure 3.28 is a sketch of the behavior of attenuation and velocity as a function of temperature (referred from Romanowicz [1995]). The temperature dependence of attenuation follows an Arrhenius exponential law and is therefore much stronger than that of elastic velocity (e.g., Minster and Anderson [1981], Kampfmann and Berckhemer [1985], Jackson et al. [1992]). This means that the attenuation structure is more sensitive to temperature variations at higher temperature, while less sensitive at lower temperatures. Therefore, "weak' upwelling currents of elevated temperature relative to the surroundings can be emphasized through the mapping of Q, whereas it is harder to detect the presence of "strong" cold downwelling (such as slabs in the upper mantle) when mapping elastic velocities (Romanowicz [1995]). Also in our results, characteristic high attenuation anomalies were identified clearly, while only large scale low attenuation regions could be found. The velocity structure and the resultant attenuation structure must be interpreted together.

In the present section, I obtained a fine three-dimensional P-wave attenuation structure for the whole mantle. Now I point out a problem due to the effect of the velocity structure.

Amplitudes of seismic body-waves are sensitive to effects in heterogeneity of elastic velocity, which create focusing and defocusing of seismic energy (e.g., Aki and Richards [1980], Resovsky and Ritzwoller [1994]) in addition to anelastic attenuation. For that reason I calculated the amplitude variation due to the whole mantle P-wave velocity structure to estimate the effect of velocity heterogeneity. Here I used the tomographic result of Obayashi et al. [1997]. The density is also set heterogeneous, assuming the density as a linear function of the P-wave velocity. P-wave attenuation structure was set to one-dimension. The amplitude calculation was conducted by using two types of ray tracing, pseudo-bending method on polar coordinate (Koketsu and Sekine [1996]) for kinematic ray tracing and the dynamic ray tracing (Červený [1985], Sekiguchi [1992]). The calculation was carried out as following procedure: 1) Put an event on the actual position, and distribute tentative stations on the surface by 10° x 10° interval. 2) Conduct two-point kinematic ray tracing from the hypocenter to each tentative station. The step length of the path segment was set to 5 km. 3) Calculate the first- and second-partial derivatives of velocity structure, and then conduct dynamic ray tracing. I used the subroutines of Sekiguchi [1992] in the procedure of the dynamic ray tracing. 4) Apply the free-surface correction. The amplitude variation due to the attenuation was also calculated to compare with the velocity effect. In this case the velocity and the density are set to 1-D structures. To eliminate the difference of heterogeneity pattern, I used Obayashi's tomographic pattern as Qp heterogeneity, but the perturbation range was set to ± 60 %.

Figures 3.29 shows the ray amplitude variations due to the 3-D P-wave velocity structure for some explosion-type point sources. Only the data with epicentral range between 28° to 89° are shown. Blue circle and red rectangle indicate larger and smaller amplitude than that from 1-D velocity and attenuation structure, respectively. The size of the mark is proportional to the common-logarithm of the amplitude ratio. Figure 3.30 shows the same as Figure 3.29 but obtained from the 3-D attenuation structure. As shown in these figures, amplitude variation due to the Qp heterogeneity is larger and longer wavelength than that due to the Vp structure. The wavelength of amplitude fluctuation is shorter than 20° at the almost area in the 3-D velocity structure, while more global distribution can be seen in the 3-D attenuation structure. There are very large or small amplitudes in some places in the 3-D

velocity structure. These anomalies are caused by the focusing and defocusing effects of velocity structure. However these anomalies appear very irregularly and they should be canceled out by each other with processing a large amount data from various hypocenters. Mentioned above it can be said that the teleseismic amplitude is affected more strongly by the attenuation heterogeneity than the velocity in global scale. This is the opposite tendency to the result of Sekiguchi [1992], who investigated the regional amplitude variation around Kanto-Tokai region, Japan. He calculated the Gaussian-beam amplitude by adopting a 3-D velocity and attenuation structure, and concluded that the effect of the Q structure on the amplitude is small. But in my case, the scalelength of the velocity structure is over 1000 km and its perturbation does not exceed ± 3 %. This means that the velocity gradient is very small in horizontally direction, and it is difficult to happen the focusing or defocusing at the wide area. As considering above I did not include the focusing and defocusing effects in the present calculation, because the scale of any heterogeneous velocity model in the whole mantle is much larger than the wavelength of the data used in this study, and present three-dimensional velocity models are not accurate enough to allow for the correction of amplitude data by forward modeling. The consideration of these effects of elastic heterogeneity should be included in the future.

I presented a three-dimensional P-wave attenuation model of the whole mantle, named QPB3DV2. This is the first result of its kind. This model is clearly very preliminary, but I think it will greatly contribute toward understanding the Earth's deep interior and mantle dynamics.

Table Caption

Table 3.1The spherically symmetric Q_p^{-1} model obtained in this study. The values fromAK135 (Montagner and Kennett [1996]) are also shown for comparison.

Depth (km)	Qp ⁻¹ (x 10 ⁻³)	s.d. (x 10 ⁻³)	count	Qp ⁻¹ (AK135) (x 10 ⁻³)
12	8.773	2.270	883925	1.146
51	6.023	1.360	1037502	2.274
110	3.472	0.620	1115536	8.681
190	5.093	1.620	1179346	8.186
290	3.752	1.030	1226344	4.566
410	2.134	0.390	1283333	4.566
551	1.372	0.210	1358124	3.793
712	1.042	0.170	1438711	1.210
893	1.708	0.370	1500496	1.262
1095	0.784	0.100	1408180	1.303
1317	0.988	0.240	1383114	1.347
1559	0.802	0.130	1284412	1.395
1821	1.213	0.270	931397	1.456
2104	0.211	0.010	423499	1.540
2407	2.702	0.830	193587	1.635
2731	0.941	0.180	43124	1.737

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Figure Captions

- Fig. 3.1 Illustration of discrete raypath. Three-dimensional seismic ray path is divided into N segments of step length Δs . The parameter (velocity and Q^{-1}) of each segment is represented by that at the mid point of each segment.
- Fig. 3.2 Comparison of representation of three-dimensional structure by block modeling (left) and grid modeling (right). Raypath is segmented at the block boundaries in block parameterization, while the incremental characteristic length is determined independently in the grid configuration. The attenuation factor (t^*) is represented by the segmented path length, velocity and Q^{-1} at each block in block modeling. On the other hand, t^* is calculated from the velocity and Q^{-1} on the raypath, whose parameters are represented by the B-spline interpolation (w: weighting function) of the peripheral modeling grids. See the text for details.
- Fig. 3.3 Representation of velocity and Q^{-1} at optional positions on a raypath. These are obtained by interpolation of values at eight surrounding grid nodes.
- Fig. 3.4 Results of the simplified cross-validation test. RMS error of log-amplitudes is shown as a function of the smoothness weight α . The RMS errors are normalized by the value when $\alpha=0$. The three-curves indicate the results with the different groupings of the data. These curves show approximately the same minimum position around the α as 2 or 3.
- Fig. 3.5 Simplified LSQR program from a version of Ratfor (Rational FORTRAN) (after Nolet [1987]). Output variables phibar and r are the absolute and relative lengths of the residual vector Ax u. Vector v and scalars (α, β) correspond to the quantities described by Van der Sluis and Van der Vorst [1987].
- Fig. 3.6 Map showing locations of 3,445 epicenters that occurred during the period from
 1984 to 1995 used in this study. The location parameters of each event were
 taken from the relocated hypocenters data base named EHB (Engdahl *et al.*

-91-

[1998]). The events that has more than 15 amplitude data were used. The minimum and maximum body-wave magnitude are 4.4 and 6.9.

- Fig. 3.7 Map showing locations of 718 stations used in this study. Totally 155,778 amplitude data observed these stations were used in this study.
- Fig. 3.8 Histogram of the bottoming depths of all the data. These bottoming depths were calculated by using AK135 velocity model (Kennett *et al.* [1995]). The depth variations are limited between 700 km to 2,700 km because of the limited epicentral distance (28° 89°).
- Fig. 3.9 The one-dimensional distribution of 16 grid nodes and sampling count at each grid depth. The grid interval becomes larger with depth. The number of the sampling count is depend on the step length for the ray tracing: large number of sampling count with shorter step length and small sampling number with longer step length.
 - Fig. 3.10 The resultant one-dimensional Q^{-1} structure in this study (solid line). Horizontal thin bars represent the standard error at each depth. This model is listed in Table 3.1. The Q^{-1} model of AK135 (Montagner and Kennett [1996]) is also shown for comparison (dashed line).
 - Fig. 3.11 Various P-wave attenuation models in the mantle obtained by body-wave analysis; MM8 (Anderson *et al.* [1965]), Model G (Teng [1968]), and SL8 (Anderson and Hart [1978]).
 - Fig. 3.12 Scatter diagram of the resultant source amplitudes versus the ISC body-wave magnitude (mb).
 - Fig. 3.13 Horizontal view of the grid configuration for tomographic inversion. The grid interval is set to 10°. There are 17 nodes spaced in latitude, 30 in longitude. Vertical grid configuration is shown in Fig. 3.9. The total number of grid nodes is 9,794 including nodes on the North- and South Poles on each depth.

-92-

- Fig. 3.14 Three-dimensional P-wave velocity structure of the whole mantle (after Obayashi et al. [1997]). Slowness perturbations from the averages at each depth are shown.
 Red and blue indicate slow and fast P-wave velocity, respectively. Whole the crust and mantle were divided into 32 (latitude) x 64 (longitude) x 16 (depth) blocks. This model was used for the construction of inversion matrices.
- Fig. 3.15 Horizontal view of the initial checkerboard pattern for the resolution test. The alternate patterns of $\pm 60\%$ anomalies in Q_p^{-1} extend both horizontally and vertically. Two types of checkerboard size, 3 x 3 x 2 grids (upper) and 6 x 6 x 3 grids (lower) in latitude x longitude x depth, were tested in order to see the resolutions in different wavelengths. Red and blue are correspond to high-attenuation (large Q_p^{-1}) and low-attenuation (small Q_p^{-1}), respectively. The displayed area is 75°S to 75°N in latitude and 0° to 360° (west to east) in longitude.
- Fig. 3.16 Resultant images of the resolution test for 3 x 3 x 2 checkerboard pattern. The portion where the resolution is good will show a clear checkerboard pattern, and the pattern becomes blurred where the resolution is poor. The displayed area is 75°S to 75°N in latitude and 0° to 360° (west to east) in longitude. The polar regions are not shown because of poor resolution in all depths (see the text for details).
- Fig. 3.17 The same as Fig. 3.16 but for 6 x 6 x 3 checkerboard test.
- Fig. 3.18 Horizontal view of the distribution of sampling count. The regions of dense sampling are black.
- Fig. 3.19 Q_p^{-1} variation maps for each depth. Red shows large positive values of Q_p^{-1} perturbations and blue shows negative values, indicating high and low attenuation, respectively. The color-scale ranges from -60 % (blue) to +60 % (red) and the values exceeding this range are clipped. The distribution of hotspots according to Richards *et al.*[1988] is also shown as green dots. The displayed area is 75°S to 75°N in latitude and 0° to 360° (west to east) in longitude.

- Fig. 3.20 Distributions of the standard error of the attenuation structure. Dark area shows large standard error.
- Fig. 3.21 P-wave velocity perturbations of Obayashi *et al.* [1997], but spatially desampled to 10° interval to compare with the attenuation results. Red and blue are correspond to high and low velocity perturbations from the average velocity at each depth, respectively. The displayed area is 75°S to 75°N in latitude and 0° to 360° (west to east) in longitude.
- Fig. 3.22 Vertical cross sections of the Q_p^{-1} variation along the great circles, which is indicated by the circle in the map given in the portion of the core. The pole position of the great circle is given at the top left of each figure. Perturbations greater than ± 50 % are clipped.
- Fig. 3.23 Vertical cross sections of the reduced P-wave velocity perturbation from onedimensional velocity model (Obayashi *et al.* [1997]). Other details are same as Fig. 3.22.
- Fig. 3.24 Vertical cross sections of the result of the checkerboard test for 3 x 3 x 2 pattern along the great circle. The position of the great circle is also given in the figures. Perturbations greater than ± 50 % are clipped.
- Fig. 3.25 The same as Fig. 3.24 but for 6 x 6 x 3 checkerboard pattern.
- Fig. 3.26 Vertical cross sections of the sampling count along the great circle. The regions of dense sampling are indicated by black.
- Fig. 3.27 Vertical cross sections of the standard error along the great circle. Dark area shows large standard error.
- Fig. 3.28 Comparison of the temperature dependence of velocity and attenuation. Units are arbitrary. The temperature anomalies are referred to an average value neat T=4.5. A) Q_p^{-1} versus temperature. The exponential dependence of Q_p^{-1} on temperature favors hotter than average anomalies, even if colder than average anomalies have

larger amplitude. B) Velocity versus temperature. They have a linear relation, that will emphasize the anomalies that are larger in amplitude, that is, cold anomalies (after Romanowicz, [1995]).

- Fig. 3.29 Ray amplitudes of the vertical component of P-waves for an explosion-type point source in the 3-D P-wave velocity structure of Obayashi *et al.* [1997]. Ray amplitudes for frequencies of 1 Hz are shown. Only the position with epicentral range between 28° to 89° are shown. Blue circle and red rectangle indicate larger and smaller amplitude than that from 1-D velocity and attenuation structure, respectively. The size of the mark is proportional to the common-logarithm of the amplitude ratio. The event locations are as follows,
 (upper) Ethiopia (1985/05/14 13:25:02.5 10.61°S, 41.38°E, 30.4 km M5.8) (middle) Bulgaria (1990/05/30 10:40:07.7 45.66°N, 26.65°E, 89.8 km M6.4)
 - (lower) Kuril (1994/08/02 14:17:54.2 52.25°N, 157.99°E, 150.1 km M5.8)
- Fig. 3.30 The same as Fig. 3.29 but obtained from the 3-D attenuation structure. P-wave velocity structure is set to 1-D. Same heterogeneous patter as Fig. 3.29 is used for the Qp heterogeneity, with setting the perturbation range to ± 60 %.











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```
subroutine pstomo(m,n,x,u,v,w,itmax)
#
# subroutine to solve the linear tomographic problem Ax=u using the
# lsqr algorithm (C.C.Paige and M.A.Saunders, ACM Trans.Math.Softw.
# 8, 43 - 71 and 195 - 209, 1982).
#
# Input: m is the number of data, n the number of unknowns, u cont-
  ains the data (is overwritten), itmax is the nr of iterations.
#
# Output: x is the solution
# Scratch: arrays v(n) and w(n)
# Subroutines: routines avpu and atupv to be supplied by the user.
#
   avpu(m,n,u,v) computes u=u+A*v for given input u,v
#
    atupv(m,n,u,v) computes v=v+A(transpose)*u for given u,v
#
dimension x(n), u(m), v(n), w(n)
open (9,file='tomo.int',form='unformatted')
do i=1,n { x(i)=0; v(i)=0 }
                                               # initialize
call normlz(m,u,beta); b1=beta;
call atupv(m,n,u,v); call normlz(n,v,alfa)
rhobar=alfa; phibar=beta; do i=1,n { w(i)=v(i) }
write(6,*) 0,x(1),beta,1
do iter =1, itmax {
                                        # repeat
  a= - alfa; do i=1,m { u(i)=a*u(i) }
                                               # bidiagonalization
   call avpu(m,n,u,v); call normlz(m,u,beta);
  b = -beta; do i=1, n \{ v(i)=b*v(i) \}
. call atupv(m,n,u,v); call normlz(n,v,alfa)
  rho=sqrt(rhobar*rhobar+beta*beta)
                                              # modified OR
  c=rhobar/rho; s=beta/rho; teta=s*alfa;
  rhobar= - c*alfa; phi=c*phibar; phibar=s*phibar;
  tl=phi/rho; t2= - teta/rho
  do i=1,n { x(i)=t1*w(i)+x(i); w(i)=t2*w(i)+v(i) } # update
  r=phibar/bl; write(6,*) iter,x(1),phibar,r
  write(9) iter,x,v,alfa,beta,phibar,r
                                              # intermediate output
   }
return; end
                                        # return
#
subroutine normlz(n,x,s)
                                        # normalizes vector x
dimension x(n)
s=0.; do i=1,n { s=s+x(i)**2 }
s=sqrt(s); ss=1./s; do i=1,n { x(i)=x(i)*ss }
return; end
```



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Used Stations (N = 718)











Magnitude v.s. obtained source amplitude



Grid mesh $(10^{\circ} \times 10^{\circ})$


Figure 3.14 (1/2)



Figure 3.14 (2/2)





Figure 3.16 (1/5)



Figure 3.16 (2/5)



Figure 3.16 (3/5)



Figure 3.16 (4/5)



Figure 3.16 (5/5)



Figure 3.17 (1/5)



Figure 3.17 (2/5)



Figure 3.17 (3/5)



Figure 3.17 (4/5)



Figure 3.17 (5/5)



Figure 3.18(1/5)



Figure 3.18(2/5)



Figure 3.18(3/5)

Figure 3.18(4/5)



Depth = 1095 km



Figure 3.18(5/5)



Figure 3.19(1/5)



hotspot (Richards et al., 1988) .

Figure 3.19(2/5)



Figure 3.19(3/5)



Figure 3.19(4/5)

Depth = 1821 km



hotspot (Richards et al., 1988)

Figure 3.19(5/5)

Figure 3.20 (1/5)



Figure 3.20 (2/5)





Figure 3.20 (3/5)

Figure 3.20 (4/5)



Figure 3.20 (5/5)





Figure 3.21 (1/5)

Depth = 190 km



$\frac{120^{\circ}}{\text{Depth}} = \frac{180^{\circ}}{290} \frac{240^{\circ}}{\text{km}}$



$\frac{120^{\circ}}{\text{Depth}} = \frac{180^{\circ}}{410} \frac{240^{\circ}}{\text{km}}$



Figure 3.21 (2/5)

Depth = 551 km



$Depth = {}^{180^{\circ}}712 km$



$Depth = {}^{180^{\circ}}893 km$



Figure 3.21 (3/5)



Figure 3.21 (4/5)



Figure 3.21 (5/5)



Figure 3.22 (1/4)



Figure 3.22 (2/4)



Figure 3.22 (3/4)


Figure 3.22 (4/4)



Figure 3.23 (1/4)



Figure 3.23 (2/4)



Figure 3.23 (3/4)



Figure 3.23 (4/4)



Figure 3.24 (1/4)



Figure 3.24 (2/4)



Figure 3.24 (3/4)



Figure 3.24 (4/4)



Figure 3.25 (1/4)



Figure 3.25 (2/4)



Figure 3.25 (3/4)



Figure 3.25 (4/4)









Figure 3.26 (4/4)



Figure 3.27 (1/4)



Figure 3.27 (2/4)



Figure 3.27 (3/4)



Figure 3.27 (4/4)





Figure 3.28



Fig. 3.29



Fig. 3.30

Chapter 4.

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General Conclusion

A whole mantle attenuation structure was obtained by applying a tomographic method to the P-wave amplitude data of the International Seismological Center Bulletin. This is the first result which delineates the whole mantle attenuation structure, not only in the upper mantle but including the lower mantle.

Before the tomographic inversion, I analyzed the ISC amplitude data based on the method of Negishi and Sato [1993]. Relative log-scaled amplitude was defined and the station correction term and azimuthal dependency were analyzed. 3,445 earthquakes and 718 seismic stations were investigated after the correction of radiation pattern and geometrical spreading effect. Averages and azimuthal dependency were obtained for relative log-scaled amplitudes. The azimuthal dependency of P-wave travel time residuals, which were recently compiled and re-determined with AK135 travel time table by Engdahl et al. [1998], were also analyzed by the same process, and the correlation between log-scaled amplitude anomalies and relative travel time residuals were investigated. Azimuth-independent terms for amplitudes at the central part of old continents, such as Eurasia and North America, are generally large, while there are small amplitudes around the Pacific Ocean and southern Europe. These station anomalies seems to have weak correlation with the type of crustal structure. The first azimuthal terms, which indicate the arrival direction with larger amplitude, have more complex distributions and do not show an obvious global tendency. The second-azimuthal terms show systematic distributions, east-west directions around the western Pacific Ocean, north-south directions in North America, and complex area in Europe. The results of the travel time residuals are similar to the result by Dziewonski and Anderson [1983]. The second azimuthal terms show good relations with the S-wave polarization anisotropy. There exist systematic clusters of negative correlation between amplitude and travel time for large amplitudes in southern Eurasia (western China and India) and for small amplitudes in the southern part of southeastern Asia (Malaysia, Singapore and Indonesia). This means that large amplitude observations are due to weak attenuation in the crust and the upper mantle in southern Eurasia, while there exists a strong attenuation area beneath Southeast Asia region.

The whole mantle three-dimensional structure of P-wave attenuation was obtained using the ISC data corrected above. I developed a attenuation tomography formula by using grid model formulation. The simultaneous inversion technique determined source amplitude and one-dimensional attenuation structure down to 2700 km depth, then three-dimensional perturbations from the one-dimensional model were calculated. The attenuation in the upper mantle is relatively stronger than that in the lower mantle. The lateral variations in longwavelength attenuation show similar patterns to the previous P-wave velocity studies. Two major high attenuation zones appear to be located in the central Pacific and beneath northern Africa in the middle to lower mantle, while low-attenuation region spread beneath the Eurasia continental shield in the upper to middle mantle. There exists some remarkable high attenuation zones in the upper and lower mantle. Hotspots are located close to those regions, therefore the high attenuation may be due to upwelling flow.

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Appendix A

Azimuthal variation of log-amplitude anomalies and relative travel time residuals.

A-1 Azimuthal variation of log-amplitudes

x-axis:	azimuth viewed from each station to events
y-axis:	relative log-amplitude anomaly
curve:	the least-square fit of equation (2.4.1)
horiz. line:	the constant term A_0 of equation (2.4.1)

A-2 Azimuthal variation of travel times

x-axis:	azimuth viewed from each station to event
y-axis:	relative travel time residuals
curve:	the least-square fit of equation (2.4.1)
horiz. line:	the constant term A ₀ of equation (2.4.1)















































A-2












































Appendix B

Amplitude and travel time station corrections for ISC stations

B-1	Amplitude	station	corrections
	1		

B-2 Travel time station corrections

ist	ID number of station
stc	station code
Neve	number of events used for calculation
Nw	number of windows used for fitting
lat.	latitude (degree)
lon.	longitude (degree)
elev	elevation (m)
ave	average term
a0	azimuth-independent term
al, dirl	amplitude and direction of first azimuth-dependent term
a2, dir2	amplitude and direction of second azimuth-dependent term
rms0, rms1	RMS residuals before and after the fitting
vr	variance reduction
corr	correlation coefficient between amplitude and travel time

Appendix B-1: Station Correction for log-amplitude

i s t	ste	Neve	Nw	lat.	lon.	elev	ave	aO	al	dirl	a2	dir2	rms0	rmsl	VΓ	COLL
13 18 46 63 66 82 83	AAT AAS ACO ADE ADE AFR AGA	80 21 50 269 647 522 21	8 4 11 14 15 17 7	-3.700 -62.160 36.699 -34.967 51.863 -17.538 38.795	128.167 -58.463 -99.146 138.709 -176.655 -149.778 -27.232	79 14 521 654 0 50 79	205 555 . 159 . 234 . 085 . 131 . 443	. 094 . 252 . 180 . 134	. 022 . 031 . 499 . 062	191.4 222.7 93.0 146.3	. 322 . 121 . 272 . 184	159.3 33.3 54.3 53.5	.75 3.20 1.12 .85 .98 .55 .49	. 95 . 82 . 41 . 44	28.5 5.3 82.1 37.0	26 . 35 18 . 25
88 90 116	AGM AGR AKRL	14 11 16	6 6 4	47.082 27.133 23.660	-69.023 78.017 32.710	238 163 0	. 707 . 758 . 260						1.31 1.04 1.07			
$\begin{array}{c} 117\\ 118\\ 124\\ 134\\ 172\\ 173\\ 177\\ 177\\ \end{array}$	AKSR AKU ALE ALQ ANM ANN ANT	19 543 382 961 192 117 29	6 18 18 17 14 9 8	$\begin{array}{r} 23.\ 672\\ 65.\ 687\\ 82.\ 483\\ 34.\ 942\\ 64.\ 705\\ 44.\ 883\\ -23.\ 699\end{array}$	33.021 -18.107 -62.400 -106.458 -165.417 37.300 -70.415	0 24 64 1853 330 0 79	. 435 . 001 265 215 258 . 237 . 101	. 001 265 234 264	.048 .209 .151 .219	151.4 244.2 103.3 185.3	. 036 . 127 . 270 . 096	168.3 75.2 173.3 121.8	1.28 .76 .60 .81 .78 1.33 1.07	. 75 . 44 . 63 . 66	1.8 46.9 38.6 28.0	. 62 61 . 42 . 00
186 194 202	APA APO AQU	12 18 10	5 11 7	$67.550 \\ 60.590 \\ 42.354$	33,333 14,030 13,403	0 340 720	098 446 . 537	366	. 450	123.5	. 960	33.4	1.23 2.20 1.18	1.01	78.9	. 52
213	ARC	208	18	40.877-	-124.075	59 2451	248 - 082	248	.116	254.6	. 358	109.1	1.01	. 79	39.0	. 30
214 221 227	ARE ARMA ARU	172 172 184		-30.448 56.400	151.730 58.600	1129 250	292	131 .584	. 368 . 272	236.3 270.7	. 280 . 164	37.2 131.5	. 70	. 60 . 39	24.9 59.7	65 .10
229	ARV ASA ASH	245	11	43.033	142.373	111	432	512	. 317	49.4	. 331	104.6	. 75	. 35	77.6	14
211	ASP	978	16	-23.683	133.897	600	.055	.058	. 269	129.8	. 088	109.2	. 59	. 30	74.1	41
280	AVE	623	17	46.855	3.376	224	096	-,096	.121	75.1	. 089	33.8	. 34	. 21	59.5	. 28
304 308 332	BAG BAL BBU	128 207 33	10 12 5	$16.411 \\ -30.665 \\ 26.215$	120.580 116.772 50.457	1506 300 0	. 438 312 . 220	. 453 354	.660 .301	220.1 80.5	. 381 . 182	176.9 146.5	1.18 .54 1.23	. 42	87.6 82.4	. 21 21
333 353 256	BCA BDF RD1	134 92	15	41.550	41.673 -47.933	500 1254	.005 007 - 352	. 007 043	. 121	197.5 186.6	. 064 . 186	48.1 142.4	. 84 . 64	. 64 . 52	41.1 33.2	. 02 29
362 365 371 384	BDT BDW BEE BEW	526 77 59 15	14 11 9 6	17. 233 42. 862 26. 017 -32. 415	99.050 -109.582 50.522 22.630	0 2190 0 870	. 070 522 . 042 . 149	.030 448	. 117 . 324	65.7 24.5	. 094 . 376	139.1 40.8	. 31 1. 26 1. 66 . 86	. 25 . 91	32.5 47.6	. 38 . 65
386 390 391 395 397 412 418 432 440	BFD BFS BFT BGC BGF BHG BHO BING BJA BJA	$ \begin{array}{r} 166\\ 111\\ 101\\ 53\\ 592\\ 292\\ 13\\ 149\\ 24\\ 691 \end{array} $	$12 \\ 14 \\ 14 \\ 13 \\ 17 \\ 15 \\ 7 \\ 13 \\ 6 \\ 18 \\ 16 \\ 18 \\ 18 \\ 18 \\ 18 \\ 18 $	-37.176 -26.898 -25.687 37.962 46.558 47.721 34.508 42.157 525.992 40.040	142.544 26.785 30.043 -122.170 2.846 12.879 -94.873 -76.067 50.608	234 1309 1868 610 389 474 143 407 0 43	034 . 216 . 064 . 198 097 . 140 165 . 019 . 395 013	018 . 200 . 100 . 016 095 . 149 029 017	. 223 . 198 . 154 . 781 . 101 . 097 . 446	298.1 129.9 146.4 302.3 199.4 199.8 209.6	. 258 . 130 . 009 . 564 . 115 . 165 . 199	60.6 40.8 55.3 41.8 111.9 65.5 39.7	6 . 69 6 . 65 6 1. 14 7 2. 13 . 41 6 . 59 1. 40 7 1. 10 . 71 1. 43	.50 .54 1.12 1.68 .31 .50 .64	47.6 31.4 4.1 38.2 41.3 28.3 65.8	33 . 34 17 . 04 . 46 . 25 37 07
115	BKB	19	1	-1.283	116, 833	0	. 269						1.51			

456 BKS	693-16	37.877-122.235	275	. 186	.185	. 069	237.5	.072	160.8	. 52	. 49	10.5	. 24
460 BL/	390-16	37.211 -80.421	634	.035	.029	.170	191.6	. 288	\$5.4	. 66	. 43	58.0	. 42
462 BLB	E - 32-11	-33.900 18.645	78	.129	. 296	. 113	237.2	. 409	159.9	1.33	1.18	21.2	07
463 BLE	186-15	-29.109 26.188	1419	. 061	.053	.150	265.5	. 056	112.9	. 75	. 70	15.0	57
474 BLS	5 30 8	59.450 6.590	1169	358						1.06	~ .	0 5	4.0
490 BM	262 13	40.563-117.267	1504	066	055	. 082	111.1	. 116	14.4	. (8	. 14	8.1	. 43
01 BN	G 160 17	4.367 18.567	0	019	045	. 195	22.2	. 287	81.9	.97	. 80	31.1	. 5h
503 BN	10 6	45.077 6.752	0	291	5.0.0	0.00	000 0	400	0.0	1.00	e.e	57 5	9.9
507 BN	5 131 11	50.964 7.175	200	. 318	. 509	. 669	203. b	. 480	33. U	1.02	. 00	91.9	52
510 DO		44 220 0 589	0.50	917						1 29			
517 BO	5 11 E 5 999 14	- 44.110 - 9.002 - 57.850 114 183	930	158	135	241	307 6	177	13-1	69	56	34.9	01
575 BO	2019	-31 598 -64 546	1200	- 133	~ 220	310	97 4	529	25.6	1.42	1.03	46.7	31
532 BP	5 5 13	-26,175 28,030	1700	104	050	. 258	185.9	. 142	172.9	1.13	1.05	13.9	.10
546 BR	10 5	26.073 50.583	0	. 430						. 85			
547 BR	G 282 16	50.874 13.946	296	.019	008	.195	78.1	. 295	156.8	1.10	. 95	25.5	. 09
556 BR	S 119-10	-27.392 152.775	524	792	775	.138	247.1	. 083	93.0	. 89	. 85	9.0	. 41
557 BR	Г 14-6	40.878 17.204	0	. 236						.91			
559 BR	208-15	71.274-156.785	-14	. 224	.236	. 091	92.0	. 228	169.5	. 63	. 48	41.3	24
564 BS	306-16	55.110 14.910	87	.012	.026	. 113	196.0	. 042	69.5	. 78	. 76	6.0	. 01
						0.45		0.7.0		50	5.0	C 1	0.0
566 BS	F 496-18	47.832 6.792	1200	~. 150	150	. 045	289.8	.072	112.6	. 58	. 56	b. I	. 33
567 BS	I 76 9	5.500 95.317	0	. 401	1.40	0.0.6	0 0	200	70.5	1. (1	17	59-1	51
- 980 BL	1 228 13	40.598 110.018	1120	110 990	 140 956 	. 030	102 0	. 255	60 3	1.07	. 41	50.5	15
- 598 BU	L 8810 06 59117	-20.143 28.013	1040	020	000	016	130.0	230	173 7	79	70	99 7	34
- 010 D# - 641 CA	00 JOLIA D 575 17	42.101-103.002	620	- 069	- 074	052	312 2	059	51.2	34	. 10	14.3	. 20
649 CA	r 313-11 R 40-10	10 507 -66 927	1031	. 185	. 175	. 203	233.2	. 129	115.1	. 71	. 58	32.9	. 03
671 CB	K 141-12	48 947 -57 997	379	. 411	. 473	. 097	205.3	. 194	59.8	. 77	. 69	19.0	. 13
672 CB	M 5414	46.932 -68.121	250	.040	.045	. 354	101.2	. 226	32.3	1.00	. 69	52.5	. 41
673 CB	N 60-10	38.205 -77.373	70	145	. 099	. 803	94.9	.178	122.7	1.43	. 92	58.4	. 50
692 CC	M 44 8	38.107 -91.346	223	014						. 96			
702 CD	2 566 16	30.910 103.758	628	. 264	. 281	. 184	42.5	. 117	24.2	. 62	. 50	33.1	35
707 CD	F 463 17	48.394 7.271	1100	207	210	. 101	55.8	. 015	98.0	. 35	. 30	24.9	. 45
722 CE	H 159-17	35.891 -79.093	151	IUZ	093	. 204	201.2	. 190	10.2	. 90	. (9	31.0	10
- 727 CE	K 103-14	-33.362 19.295	472	. 048	. 122	. 279	124.0	. 293	107.0	. 89	. 00	41.1	. 1 (
744 00	E 11 0 D 05 0	09.002 9.291	50	- 021						86			
752 00	r 959 V 167	-96 348 96 375	0	199						. 78			
761 CH	G 609 16	18 790 98 977	416	- 177	185	. 118	93.8	.079	114.8	. 49	. 43	23.7	. 48
- 774 CH	T 663 18	22.350 91.817	14	155	155	. 130	128.4	. 058	79.6	. 68	. 64	12.1	. 00
797 CK	I 15 8	3 44.499 8.399	0	.187						1.28			
813 CL	L 277-15	51.309 13.004	230	.179	.187	. 046	133.3	. 083	178.1	. 48	. 45	11.3	24
827 CM	A 140-15	64.290-149.180	180	329	358	.068	278.3	. 233	104.6	. 84	. 73	23.5	. 15
828 CV	B 301-14	38.035-120.385	718	114	120	. 093	226.9	. 129	119.6	. 86	. 82	9.7	. 50
841 C.V	S 152-11	-31.487 145.828	254	210	241	. 153	71.3	. 105	84.1	. 55	. 43	37.6	. 54
847 CM	2 764 13	43.801 125.448	230	093	063	. 154	31.9	. 046	12.5	. 58	. 51	22.0	30
848 CN	B 239 12	-35.315 149.363	850	002	097	. 288	41.0	. 200	11.0	.91	. (4	43.0	. 1 1
- 880 CC	L 218-13	64.900-147.783	182	. 089	. 144 956	. 180	93.7	. 240	26.7	. 02	, 00 28	37.3	- + (
- 883 C	0 138 13 0 420 10	5 ~30.318 131.892 5 55 693 19 493	260	515	000 909	. 100	61 1	149	69 G	. 45	200	31.5	- 21
884 CC	a. 410 fo	0 00.000 12.400	10	. 200	. 202	. 045	01.1	. 142	02.0	. 40	. 00	01.0	. 61
885 CI	R 19 5	7 44 585-123 303	123	- 196						3.24			
909 CT	T 39.10	40.673-112.190	2227	. 044	. 278	. 681	193.9	. 355	13.5	1.43	1.15	35.7	. 52
\$13 CF	7. 12 f	5 50.210 -5.585	197	277						1.06			
960 CS	Y 360 14	-66.344 110.639	5.6	285	274	. 043	212.4	. 079	108.9	. 82	. 80	3.8	27
962 C1	A 513-14	-20.088 146.255	356	. 190	. 191	.134	174.9	. 256	89.0	1.09	. 94	24.6	. 49
990 CV	F 103-13	42.568 8.870	529	134	156	.128	21.2	. 213	117.9	. 65	. 55	28.3	. 32

995 (VP 66 1i 17,600 121,700 0 -.138 -.194 .249 149.7 .549 79.1 1.18 .82 51.8 -.15 1011 (YP 301 16 51.380 23.000 0 .954 .942 .050 32.2 .116 116.0 .89 .87 5.3 .25 1025 DAG 910 18 76.770 -18.770 16 -.044 -.044 .109 257.1 .066 86.0 .44 .39 23.2 .44 1029 DANN 82 11 28,350 83,760 2500 .732 .860 .350 260.8 .170 29.7 .86 .60 51.6 .36 . 59 32 7 7.088 125.575 85 .725 1033 DAV 13 10 -5,550 150,467 250 -,579 -,433 ,240 319,3 ,662 1.6 1.12 ,66 65.1 -,10 1034 DAW 1037 DB1C 38 13 6.701 -4.913 25 -.136 -.178 .082 218.4 .330 90.7 1.29 1.17 19.0 .20 1048 DCN 258 16 53.343 -7.278 150 .474 .548 .276 147.2 .361 151.9 .97 .76 39.8 .08 1.58 1055 DDK 16 6 53.387 -6.339 85 .381 . 311 . 103 164.1 . 240 70.6 . 44 . 29 55.6 - 05 1095 DE2 420 13 38,906 121,628 61 . 341 .196 .038 296.4 .166 133.8 .69 .62 18.2 -.50 1098 DLE 184 15 53.287 -6.544 140 . 196 .656 .102 182.5 .208 149.4 1.11 1.04 12.1 -.33 1099 DLF 158 15 53.296 -6.531 96 .632 1110 DMN 371 18 27.690 85.160 2224 .306 . 306 . 126 117.8 . 051 24.8 . 53 . 48 18.2 - 11 257 14 53,899 -6.911 280 .381 .420 .164 203.6 .091 159.2 .56 .49 25.0 .29 III3 DMC 1126 DOI 20 7 44.535 7.354 1014 - 439 1.40 1133 DOL 116 16 50,210 4,692 224 -.098 -.098 .174 64.7 .090 169.8 1.12 1.06 9.7 .36 56 26 6 50.433 16.511 759 .141 1137 DPC 1151 DRLN 23 9 49.310 -57.542 238 -.655 .056 4.8 .50 .42 31.0 -.09 1175 DLG 440 16 40, 195-112, 813 1476 ~, 082 -, 101 , 165 46.9 .135 41.8 .077 78.6 .70 .67 9.8 .13 1202 EAB 148 15 56,188 -4,340 250 . 029 ~. 003 . 290 103.0 .80 .54 55.2 -.51 . 478 353.9 1206 EAU 124 14 55,845 -3,455 349 .004 -.167 .104 .033 .158 318.5 .247 110.2 .72 .58 34.5 -.40 1210 EBH 142 14 56.248 -3.508 375 . 273 2.8 . 384 99.4 . 78 . 59 42.0 . 10 1212 EBL 100 14 55,773 -3.044 365 -.052 -.194 1218 ECB 186 15 52, 366 -6, 781 125 . 306 . 332 . 051 276.1 . 238 161.4 1.06 . 98 14.8 -.07 1227 ECP 337 15 52.180 -6.369 4 .389 .393 .142 280.7 .077 165.8 .53 .44 31.0 -.05 78 13 55.923 -3.186 125 -.085 -.210 .293 34.0 . 275 103.2 . 66 . 53 36.2 -. 59 1234 EDI 1236 EDM 280 16 53.222-113.350 730 .336 .364 .223 186.2 .228 59.0 .89 .72 34.5 .16 40 14 56.934 -2.604 388 .128 -.007 .450 354.5 . 152 93.1 1.10 .93 27.4 -.31 1237 EDR 1239 EDU 136 13 56.548 -3.014 275 .069 -.032 .310 347.7 . 277 92.6 .64 .42 57.3 -.15 1258 EKA 878 17 55.333 -3.159 229 -.169 -.174 .131 304.5 .074 126.4 .47 .39 29.6 .35 1271 ELK 103 10 40.848-115.288 2210 - 214 - 234 .251 228.8 . 446 172.9 1.00 .67 54.5 -.45 1274 ELO 132 15 56.471 -3.712 495 .100 .168 .257 166.3 .195 9.6 .77 .63 32.5 .49 23 9 53,250 86,267 0 -.025 1.48 .155 165.9 .46 .37 36.8 .09 1299 ENN 831 18 50,767 5,923 119 .055 . 055 . 064 327. 5 1306 EPF 571 17 43.031 .340 750 -.200 -.191 .202 192.6 .044 102.3 .72 .63 23.3 .36 . 289 175.9 .099 42.7 .68 .51 44.1 .18 1332 FSD 88 15 46, 323-122, 150 1608 -, 699 -, 682 .088 285.1 .093 94.8 .54 .49 16.3 -38 1334 ESK 270 14 55.317 -3.200 241 .107 .092 . 182 99.4 1.02 .79 40.3 -.13 1342 ESY 140 14 55.918 -2.615 324 . 287 357.2 1345 ETA 176 15 52,696 -6.210 140 . 407 . 448 . 181 227. 2 .169 6.3 .74 .64 25.9 -.14 .174 352.7 .059 89.0 .84 .78 12.2 .33 1359 EUR 204 13 39,483-115,967 2177 -.494 -.500 . 255 94.9 1.09 .96 22.3 55 13 -26,555 29,170 1621 -.076 -.109 . 14 1361 FVA .073 49.4 .71 .68 6.9 -.19 1371 EYMN 116 10 48.062 -91.600 474 .020 . 114 234.9 .180 93.9 186 178.0 .61 .43 49.8 .43 1381 FBA 826 16 64.860-147.835 180 .044 .067 70 11 58,762 -94,087 39 ,219 ,202 ,174 309.0 .060 45.2 .64 .57 18.9 .51 1399 FFC 770 16 54.725-101.933 337 -.135 -.148 .187 65.9 .068 42.9 .57 .45 37.0 .54 65 9 40,802-123,985 610 .027 1408 FHC 1415 FIN 149 16 44.209 8.208 589 -.480 -.520 .382 22.7 .152 10.31.12 .89 36.4 -.19 .369 17.81.32.84 59.7.74 1419 FITX 61 13 -18, 192 125, 728 109 -, 293 -, 141 1424 FKO 18 4 35.363 -97.386 351 .195 . 80 .027 15.5 .41 .38 14.3 .10 1431 FLN 785 17 48,763 - 482 0 .112 .116 .088 229.4 91 11 40.863 -73.885 24 -.186 .102 .777 269.9 . 30 . 538 54.51.07 .54 74.9 1455 FOR 1463 FRB 436 16 63.747 -68.547 17 -.030 -.027 .115 76.4 . 078 138.1 .38 .30 39.2 . 26 1466 FRF 508 17 43.657 6.768 310 -.050 -.053 .062 137.9 . 112 105.9 . 48 . 42 21.0 -. 07 1475 FRS 186 15 -29.750 25.322 0 -.055 -.049 .076 249.6 .058 137.3 .67 .64 6.9 -.30

. 67 1477 FRI 20 7 42,833 74,617 0 .227 .341 .073 259.6 .112 29.7 .66 .63 9.4 .14 1495 FUR 318 15 48,166 11,276 564 .317 11 6 46.682 12.909 0 .029 . 94 1496 FVI .087 .176 184.9 .240 67.7 .70 .49 50.3 -.11 1497 FVM 447 15 37,990 -90.510 310 .055 38 7 45,703 -75,470 112 -.358 . 73 1506 GAC .343 .175 274.6 .275 63.5 .86 .69 36.3 -.37 1509 GAM 49 10 39.000 70.317 1299 .290 1.06 17 7 47.477 11.064 725 .139 1511 GAP .160 57.4 .152 61.5 .57 .44 42.6 -.46 1518 GBA 868 17 13.604 77.436 25 -.241 -.248 .100 20.2 .169 93.1 .70 .61 23.4 -.48 1544 GDH 321 16 69.250 -53.533 23 -.063 -.053 .182 4.8 .030 79.8 .60 .53 23.8 .50 1551 GEC2 370 16 48.951 13.715 1136 -.585 -.605 . 214 89.5 . 101 8.4 . 85 . 75 23.2 . 08 1557 GERE 154 16 48,951 13,715 1136 -.660 -.666 .116 358.9 .091 71.6 .52 .45 22.8 -.13 1596 GKN 248 18 28,030 84,670 1478 .347 .049 3.0 .103 95.0 .29 .23 39.7 .34 1601 GLD 495 14 39.750-105.221 1761 .166 . 95 1613 GMB 20 6 38,167 15,863 1350 -.238 . 226 149.8 . 242 78.4 . 77 . 61 37.7 . 12 1636 GOGA 48 10 33,512 -83,616 150 -.034 1638 GOL 593 16 39.700-105.371 2358 -.206 . 199 .021 81.5 .165 130.5 .47 .36 38.6 .09 1.11 1649 GRB1 11 8 49.472 11.687 493 -.061 . 142 71.1 . 049 149.7 . 46 . 38 30.7 . 02 1653 GRF 658 17 49,692 11,222 499 158 1656 GRI 60 9 38,821 16,451 479 .060 . 54 97 13 -33.312 26.508 601 .358 .337 .088 9.0 .028 22.2 .46 .43 11.3 -.20 1658 GRM 1660 GRO 61 8 43, 317 45, 700 123 . 426 .147 .065 285.7 .077 153.4 .33 .28 27.1 .29 1663 GRR 636 17 48.388 -.851 0 .145 . 66 20 6 39,500 46.333 0 .367 1664 GRS .018 .108 93.6 .105 43.5 .41 .32 39.8 .03 1679 GTA 822 17 39.400 99.800 1340 .015 . 313 64.7 1.12 .69 62.6 .18 1685 GUA 411 16 13,538 144,912 230 .179 206 404 172.5 1689 GUM 221 15 20.680-103.324 1567 .288 . 212 . 331 216.3 . 262 15.2 1.08 . 87 35.3 . 14 .107 254.8 .273 76.3 .76 .60 36.9 -.63 .470 1690 GUN 231 17 28,006 85,994 2900 .450 .193 35.4 .125 88.9 .77 .67 24.8 -.49 1709 GYA 610 18 26.459 106.664 1161 .028 . 028 1713 GZH 195 14 23,087 113.344 10 .072 .032 219.3 .098 95.8 .70 .67 6.2 .17 789 18 48.005 6.350 569 -.086 -.086 .050 187.1 .014 107.2 .44 .43 3.9 .33 1733 HAU 1766 HFS 850 17 60.134 13.696 223 -.243 -.251 .390 61.4 .192 161.8 1.28 1.04 34.0 .09 1.03 1768 HGH 10 7 51,638 -2,806 209 - 221 88 13 50.890 6.067 135 -.073 -.113 .257 355.0 .332 152.6 .74 .46 61.3 .04 1769 HGN . 258 65.3 . 73 . 59 35.1 . 15 1774 HHC 534 17 40,849 111,564 1169 .174 .186 .044 67.6 . 90 1799 HKT 12 3 29,950 -95,833 -122 -.124 . 497 44.4 .91 .48 72.6 .19 288 13 50.314 11.877 565 .005 .159 .447 207.3 1836 HOF 1852 HPK 162 15 54.004 -1.690 226 -.187 -.193 .149 16.3 .154 138.7 1.23 1.19 6.8 -.07 1867 HRV 118 14 42.506 -71.552 180 -.095 -.029 .485 173.6 .445 104.1 1.20 .74 62.6 -.03 33 10 -30,604 25,496 1378 .255 . 225 . 220 37.2 . 230 98.2 . 99 . 83 29.2 . 11 1.83 45 7 61.310 6.220 29 .199 1910 HYA .306 .147 139.0 .106 41.5 .89 .84 10.9 .19 235 11 17.417 78.553 509 .322 1911 HYB 32 11 47.285 2.694 428 .177 .407 .648 159.4 .068 150.2 1.15 .87 42.8 -.07 1914 HYF .285 59.0 .016 69.4 .73 .57 38.7 .08 1955 ILT 184 13 67.833-178.800 0 .297 . 361 .125 163.6 .58 .45 41.2 .33 1958 IMA 1013 17 66.085-153.786 0 -.165 -.163 .177 51.0 1973 INGI 21 8 -8.818 115.145 202 .235 1.19 1975 INK 721 17 68.237-133.520 39 -.136 -.133 .079 114.0 .196 149.5 .56 .43 41.5 -.31 837 16 4.581 101.027 246 -.011 -.043 .049 23.5 .285 90.7 .69 .51 44.9 .17 1984 IPM 188 14 52.267 104.317 467 .083 .187 303.2 .224 67.9 1.18 1.05 21.9 .60 1993 IRK 1996 ISA 249 16 35,643-118,477 759 -.268 -.254 .361 166.6 .067 39.5 1.08 .89 33.0 .27 .442 66.1 . 236 82.7 .84 .63 44.0 -.24 64 12 -2.500 140.667 400 -.569 -.517 2045 JAY 2059 JCT 87 12 30.479 -99.802 591 .012 .009 .088 95.6 .393 9.2 1.00 .79 38.0 .16 2080 JFWS 96 10 43.042 -90.381 335 -.051 -.212 .150 87.9 . 297 176.6 .71 .63 21.5 .24 . 52 2112 JIRN 45 9 27.660 86.190 3063 .307 16 10 -27.445 32.078 244 -.131 -.180 .417 345.9 .231 168.2 1.38 1.12 35.1 .08 2188 JOZ 67 9 49.192 -2.099 52 .316 1.36 2196 JRS

2258 KAF 365 16 62.113 26.306 204 -.140 -.142 .088 274.3 .192 96.0 .59 .46 39.3 .51 2263 KALI 13 6 -7.106 106.659 810 .526 1.47 2276 KBA 682 17 47.184 13.447 1720 .070 .088 .144 213.8 .175 12.0 .61 .50 32.7 .31 2300 KDC 467 16 57.748-152.492 0 .134 .138 .333 26.3 .161 62.11.11 .96 24.8 .16 2311 KED 35 6 12,926 -12,321 0 -.279 1 60 1.09 2315 KELL 16 7 -8,217 114,491 591 -.256 2321 KEV 437 18 67.755 27.007 79 .016 .016 .221 237.8 .039 54.0 .85 .76 19.5 .04 . 48 2331 KGM 284 9 2.015 103.317 103 . 263 2337 KHC 569 16 49.131 13.579 699 -.092 -.089 .018 164.3 .104 168.7 .55 .52 10.3 .11 2351 KIC 148 17 6.360 -4.741 174 .113 .104 .035 136.1 .300 86.6 .65 .39 63.1 .37 2356 KIM 31 LT -28, 752 24, 780 1320 -. 032 . 136 . 356 131.8 . 488 144.0 1.44 1.13 38.8 -.13 2358 KIP 66 11 21, 423-158, 014 72 .080 .068 .126 46.8 .164 63.2 .63 .56 21.5 .21 2360 KIS 82 7 47.017 28.867 0 .838 . 48 .744 49.81.551.1743.3.31 2362 KIV 109 11 43,950 42,683 1200 .329 .205 .377 156.5 2364 KJF 99 15 64.199 27.715 159 .090 .078 .061 274.8 .205 89.9 .79 .70 21.8 .29 2371 KKM 361 14 6.015 116.211 0 .011 .043 .260 145.4 .039 93.2 1.14 1.04 17.0 -.25 2372 KKX 319 17 27,790 85,280 1919 .257 .253 .191 21.0 .045 48.6 .48 .34 49.9 -.13 2380 KLB 232 11 -31.673 117.850 300 -.289 -.234 .126 167.6 .226 66.3 .70 .53 42.9 .01 2389 KLM 23 8 3.100 101.650 0 .271 . 91 2407 KMI 508 16 25.123 102.740 1945 .321 .321 .055 173.7 .095 39.7 .44 .40 14.7 -.04 29 8 59.320 5.370 57 -.257 1.31 2420 KMY .51 2421 KMZ -11 6 -13,505 25,837 1223 -.393 2423 KNA 121 12 15,750 128,767 54 -.011 .058 .170 285.2 .275 51.2 1.24 1.13 17.3 .40 . 61 2436 KOD 39 7 10.233 77.467 2315 -.032 2142 KOL 91 9 41,493 35,911 144 .484 2144 KON 19 9 59.649 9.632 216 -.313 1.03 2462 KRA 543 17 50.052 19.937 223 .204 .217 .164 140.3 .234 41.8 .78 .61 38.0 .68 2488 KSH 434 18 39.455 75.980 1286 .297 .297 .108 220.5 .174 168.7 .74 .66 21.4 .00 10 7 -3.638 102.673 0 -1.419 1.80 2489 KST 2193 KSP 566 15 50.843 16.293 379 .112 .133 .086 168.8 .129 23.7 .36 .26 47.3 -10 2494 KSR 199 16 -25.850 26.897 1623 -.101 -.169 .311 318.8 .335 90.6 .92 .64 50.8 -.55 2512 KTK1 35 9 69.117 23.271 340 .298 . 95 2.81 2519 KUG 11 6 -10.163 123.653 52 -.723 2525 KUP 33-10-10.168-123.586-52-.180-.455-.451-238.9-.534-57.5-.91-.68-43.3-.51 2526 KUR 64 11 45,233 147,867 0 .092 .097 .539 100.3 .189 38.2 1.28 .82 58.6 .40 2557 LAR 12 6 41.314-105.583 0 .283 1.69 2569 LBF 698 17 46,985 3,977 714 -.157 -.160 .035 125.3 .070 88.8 .45 .43 8.7 .57 2573 LBNH 114 15 44.301 -72.009 367 -.244 -.316 .177 281.5 .331 32.9 .89 .71 36.9 .08 2578 LBTB 74 13 -25.145 25.720 1027 .197 .139 .111 137.5 .295 60.9 .99 .82 30.7 .12 2604 LDF 661 17 48.594 -.122 289 .036 .038 .042 256.6 .070 137.3 .35 .32 15.6 .03 2619 LEM 49 9 -6.833 107.617 1241 -.051 1.48 2633 LFF 603 17 44.937 .736 193 .017 .014 .075 37.4 .068 130.6 .40 .36 19.1 -.31 . 79 43 9 48, 417 -89, 267 195 .073 2648 LHC 2660 110 307 17 6.225 -5.028 100 .053 .058 .157 146.4 .162 93.7 .51 .33 58.0 .56 . 75 2672 LIU 66 9 46.043 14.533 395 .427 2678 LK0 155 16 9.614 -5.639 435 .127 .126 .150 237.1 .192 75.2 .64 .48 42.6 -.21 2699 LMN 54 10 45,870 -64,860 363 -,430 -,803 ,916 306.4 ,730 27,31,44 1,15 36.1 ,02 2701 LMQ $23 \quad 6 \quad 47, 548 \quad -70, 327 \quad 418 \quad -, 671$. 82 2702 LMR 482 18 43.333 6.509 200 -.058 -.058 .018 293.9 .087 81.9 .55 .53 7.4 -.42 2723 LOF 29 7 68,260 13,620 79 -.159 . 61 2730 LOR 881 17 47.267 3.850 529 -.045 -.046 .026 351.7 .040 129.5 .41 .41 3.9 .57 2.90 2734 LPA 19 6 -34,909 -57,932 14 -,382 74 13 -16.677 -68.234 3292 .211 .175 .472 52.6 .101 102.3 1.20 .91 41.9 .47 2735 LPB 2738 LPF 668 17 48.165 -1.108 156 .068 .067 .111 7.5 .233 136.4 .61 .41 54.2 -.21 2739 FPG 696 18 45.627 6.765 2569 -.049 -.049 .033 116.4 .125 45.7 .41 .35 27.7 .15

2741 LPL 401 17 45.665 6.874 2069 -.139 -.140 .204 105.5 .104 57.6 .53 .35 55.7 -.31 2743 LPO 618 17 44.683 1.187 330 -.063 -.064 .021 30.6 .047 124.9 .29 .28 9.4 .08 .085 119.0 .130 95.1 .58 .52 20.3 .00 2754 LRG 563 18 43,454 6,360 100 -.021 -.021 2765 LSA 380 16 29,700 91,150 3657 - 272 - 276 ,140 76.5 .048 75.0 .90 .86 8.2 -.42 2766 LSCT 84 12 41.784 -73.294 317 -.076 -.229 . 218 273.2 . 456 19.9 1.12 . 94 29.8 . 49 .021 11.8 .070 156.5 .37 .35 11.1 .01 2768 LSF 518 17 46,250 1,530 430 -.068 -.066 33 8 -15.366 28.232 1184 -.392 . 59 2777 LSZ 2798 LTX 143 13 29.334-103.667 1013 -.198 -.180 . 193 93.4 .88 .82 14.3 .04 . 053 82.3 2825 LZH 630 18 36.050 103.833 1518 .235 .235 .160 90.7 .294 106.5 1.19 1.05 22.1 -.12 2832 MAF 567 17 46.265 2.714 469 -.032 -.033 .053 74.0 .023 58.7 .37 .36 7.2 .41 2835 MAL 267 15 35.472 135.387 30 -.206 -.161 .377 293.2 .284 115.1 1.14 .85 43.7 .07 2836 MAJO 154 12 36.542 138.209 421 -.033 .004 .189 8.0 .286 11.7 .75 .58 40.8 .18 . 78 2837 MAK 12 6 43.017 47.433 0 .679 29 5 14.667 121.083 70 .564 . 53 2840 MAN 2845 MAT 786 15 36.538 138.208 439 -.103 -.080 .113 60.9 .153 54.0 .49 .37 40.6 .46 .139 331.1 .158 88.7 .67 .58 25.6 .45 2848 MAW 466 16 -67,604 62,870 12 -.241 -.246 2852 MBC 997 17 76.242-119.358 14 -.034 -.031 . 242 169.1 . 092 161.7 . 65 . 47 47.6 -. 33 2857 MBL 202 14 -21.160 119.833 200 -.171 -.165 . 097 148.7 . 103 140.4 . 58 . 53 17.8 - 50 . 89 2878 MCQ 16 6 -54.499 158.956 11 -.434 2884 MCW 113 13 48.797-122.973 693 -.010 .054 .088 127.1 .436 65.5 1.26 1.04 32.2 -.09 2897 MDJ 527 14 44.616 129.592 250 -.028 -.039 .190 151.8 .145 72.6 .62 .52 29.6 .02 2911 MEEK 50 8 -26,678 118,745 529 -.096 2914 MEK 30 10 -26.613 118.545 514 -.468 .156 1.184 247.6 .429 86.61.13 .56 75.5 -.14 2916 MEM 105 10 50.692 6.066 0 -.282 -.413 .500 36.7 .515 147.1 .90 .46 73.9 .12 39 11 34, 785 -98, 596 465 . 226 . 134 . 175 333.9 . 322 119.5 . 96 . 84 23.3 . 06 2918 MEO 2923 MEE 10 4 37,101 14,930 985 -.624 . 72 2928 MFF 639 17 46.601 -.143 259 -.021 -.027 . 132 37.5 . 080 120.7 . 42 . 33 38.6 - 06 . 53 61 9 60.100 150.700 219 .072 2938 MGD 16 6 40.176 15.598 259 .322 1.04 2947 MGR 2953 WHC 162 13 37.342-121.642 1281 .278 .428 .288 2.1 .635 178.8 1.24 .78 60.1 -11 2955 MHI 10 4 36,300 59,595 1100 -.007 2961 MIAR 209 14 34.657 -93.630 207 -.069 .005 .230 198.1 .365 80.8 .96 .62 57.5 .2937 11 59.427-146.338 0 .411 .414 .290 18.5 .226 65.2 .50 .37 45.6 .33 2963 MID 92 11 40.345-121.605 1495 .037 .026 .244 352.6 .117 159.8 .74 .58 39.4 .232969 MIN 2578 MJAR 177 13 36.542 138.209 421 -.756 -.720 .291 124.3 .192 80.1 .71 .57 35.0 -.13 2990 MKS 44 8 -5.067 119.633 28 .082 1.40 . 74 3013 MME 10 4 44,194 10,700 2160 ,155 24 6 1.450 124.800 128 -.061 1 95 3033 MNI . 84 3034 MNK 66 9 53,900 27,567 0 .433 13 5 37.931 14.695 1840 -.188 . 53 3038 MNO 3042 MNS 15 8 42.396 12.800 600 .086 3043 MNT 87 13 45.502 -73.623 112 -.070 -.058 .103 155.4 .062 144.8 1.20 1.19 2.8 .45 65 11 38.572-118.194 1506 -.152 -.260 .100 207.0 .505 152.9 1.14 .69 63.4 .06 3045 MNV . 95 3058 MOL 34 8 62,600 7,680 97 ,166 . 50 3064 MOR 43 6 42.103 140.572 18 .212 . 86 24 8 55.733 37.633 120 .495 3065 MOS 3066 MOT 102 13 30.797-104.082 2019 -.229 -.239 .234 77.1 .072 141.7 .84 .73 23.9 .53 240 17 50.646 11.616 453 .102 .111 .011 141.0 .156 13.5 .44 .36 32.7 -.46 3070 MOX 42 9 51.683 100.983 0 .016 . 94 3071 MOY 3101 MRW 226 15 -41.232 174.705 0 -.671 -.704 .183 86.5 .179 120.5 1.04 .95 15.7 -.20 3128 MTA 71 8 41.700 44.800 0 .110 .77 3138 MTX 113 11 -12.847 131.130 79 .204 .457 .368 232.9 .410 60.1 .91 .81 21.5 -.44 3150 MUD 312 14 56,460 9.170 12 -.104 -.077 .159 157.5 .137 150.1 .49 .35 48.7 -.20

.179 149.5 .133 38.8 .67 .54 34.8 .09

3153 MUN 340 12 -31,978 116,208 234 -.066 -.066

3173 MYNC	33 7 35.13	39 -84.229	550	. 024			. 63			3679 PMG	245 1	2 -9.	. 409 147	7.154	67	. 282	. 386	.179 187.7	. 319	67.7	. 66 .	27	82.5	48
3180 MZF	17 9 46.21	0 2.084	4 (9	11.5	1.20	150 149 9		7.6	- 06	3685 PMO	762 1	7 -15	004-147	7 897	9	0.4.6	044	084 191 9	197	73 3	. 61 .	48	37.0	. 36
3199 NAL 2969 NAV	- 110 10 ~ 1.07 - 99 11 - 99 04	39 - 00, 00 (39 - 11 9 - 79 9	1092	- 120	- 302	60.1 301 6	737 97 8 1 71 60	75.6	- 01	3687 PMR	1318 1	8 61.	. 592-149	9.131	0	. 034	. 034	.106 60.3	. 139	123.8	. 47	37	38.4	. 22
9904 NAO	00 11 02.00	27 10.074	270	- 010	- 020	200 292 1	095 63 3 1 00 84	29 6	67	3688 PMS	51 1	0 61	245-149	9 561	716	052	126	176 79.5	. 093	45.0	. 78 .	73	11.5	. 61
3204 AAU 2212 XR9	- 100 - 01 - 601 - 601 - 601 - 601 - 601 - 601 - 601 - 601 - 601 - 601 - 601 - 601 - 601 - 601 - 601 - 601 - 60	10.073	717	- 100	- 103	138 52 1	072 169 1 51 43	25.0	- 59	3705 PNT	689 1	4 49.	. 317-119	9.617	550	095	103	. 024 246.6	.078	146.4	. 63 .	61	5.1	25
0616 106	000 11 01.0.	1 11.041	111	. 100	. 100	. 1007 02. 1	.012 100.1 101 110	211.0		3711 POF	86 1	4 - 29	382 19	9.950	0	376	441	. 351 48.1	. 216	57.71	. 26 1.	0.4	31.6	. 64
2927 NDF	220 12 28 63	33 77 917	230	159	192	225 6.8	127 80 6 61 44	48 1	- 22	3716 P00	244 1	4 18.	. 533 73	3.850	555	. 024	092	. 451 100.3	. 320	11.61	. 07 .	76	50.1	64
9947 NCW	557 16 48 96	32-117-120	750	- 133	- 168	221 51 9	158 153 9 66 50	43 5	- 10	3777 PPI	199 1	0 -	452 100	0.384	0	238	475	.728 30.2	. 378	134.8 1	. 08 .	5.4	75.1	35
3241 MD#	- 130 16 - 49 - 43	75 TTT. 120 24 - 20 - 322	555	128	139	094 316 1	111 39.2 .73 .69	11.5	.14	3731 PPN	496 1	7 -17	. 531-149	9.432	0	. 042	. 053	.108 149.8	.178	36.8	. 57 .	45	36.2	.07
2976 X19	193 19 32 05	57 118 854	.45	010	050	159 10 1	136 24 1 51 38	43 3	- 59	3733 PPR	66	9 9	. 750 118	8.733	14	178					. 77			
3305 NVA	101 14 -12 02	23 -76 922	574	- 284	285	. 228 114.5	.174 91.3 1.11 .98	21.5	34	3735 PPT	513 1	7 -17	. 569-149	9.576	259	. 217	. 224	. 200 142.7	.142	57.6	.46 .	19	82.1	. 03
3314 NOR	109 15 81 60	0 -16 683	35	- 558	545	.045 101.3	. 270 33.2 .63 .43	53.0	.17															
3319 NPA	36 8 -15.03	37 39.253	374	.079			1.00			3741 PRA	155 1	2 50.	.070 14	4.430	202	.017	.073	.362 167.0	. 457	28.3	. 89 .	62	51.3	.10
3325 NPO	132 12 64 8	14-146 915	418	- 200	260	. 399 349. 3	. 177 151.1 1.39 1.13	34.2	. 52	3757 PRU	430 1	5 49.	. 988 14	4.542	301	041	031	.114 148.1	. 231	17.5	. 51	. 32	60.2	25
3331 NRI	54 10 69.40	0 88.100	39	. 154	. 342	. 348 275.7	. 329 5. 3 . 92 . 41	80.2	. 67	3760 PRY	126 1	3 -26	. 928 27	7.473	0	083	. 001	.152 221.2	.350	150.9 1	.00	. 78	39.7	38
3340 XSS	42 10 64.65	50 11.970	101	.104	. 224	.614 176.6	. 121 51.5 . 91 . 27	91.2	23	3761 PRZ	34	9 42.	. 483 - 78	8.400	0	. 228					. 99			
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3350 NUR	673 17 60.50	09 24.651	101	079	090	.175 11.1	. 121 143.0 . 45 . 29	59.7	09	3798 PTZ	23	9 -14	. 390 31	1.390 1	026	280				1	. 43			
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3363 NWA	354 14 -33.03	20 117.240	264	465	466	.176 106.9	. 272 8.9 1.17 1.02	23.2	07	3825 PWA	49-1	2 61	. 651-149	9.879	136	. 214	. 239	. 397 193.7	. 687	151.0 1	. 14	. 58	74.0	38
3365 NWL	18 8 -27.7	57 29.981	1332	026			1.88			3832 PYA	126	9 44	. 033 43	3.050	497	. 489					. 42			
3387 OBN	355 17 55.10	67 36.600	0	. 273	. 259	. 227 43.0	. 303 119.3 1.03 .81	38.1	. 39	3838 PYUN	100 1	4 28	.100 82	2.990 1	866	. 764	. 774	.289 316.1	. 289	66.5 1	. 03	. 81	39.0	36
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3410 OGA -	285 16 46.8	68 11.025	934	025	033	. 298 152.0	.095 57.0 .83 .66	36.0	02	3854 QIZ	163 1	1 19	. 029 109	9.843	230	. 064	.197	.506 218.0	. 605	65.8	. 93	. 36	85.2	. 18
3118-0HR -	-315 15 41.2	l 4 - 20. 939	739	358	328	.145 138.9	. 285 25.1 2.10 2.03	6.6	31	3857 QLP	62	8 -26	. 587 14	4.248	209	.169					. 91			
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3170 ORO	16 7 45.6	25 7.980	1161	403			. 59			3882 RAB	41 1	1 -4	. 193 151	2.171	182	. 525	. 520	. 375 256. 3	. 193	5.71	20 1	. 08	18.4	03
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3491 OTT	[4] 14 45.3	94 -75.716	82	. 164	.177	.126 301.1	. 021 93. 3 . 95 . 92	4.9	. 22	3888 RAM	70 1	0 37	. 766 41	1.292	850	. 457	. 469	. 249 238.1	. 400	86.5	. (2	.46	59. I	. 06
3506 OXF	76 8 34.5	12 - 89.409	101	. 314			1.11			3889 RAN	23	(16	. 867 91	b. 183	14	. 149					. 11			
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3517 PAE	- a09 17 -17.6	62-149.580	59	. 132	. 139	.241 131.6	.060 57.8 .52 .31	b5.5	. 50	3891 KAK 2009 DAT	41	9 -21	. 212-13:	9.110 0.4E1	20	097					. 33			
3530 PAS	11 6 34.1	48-118.172	294	. 088	1 050	976 07 9		50 E	9.1	3892 KAI 2017 DDD	24	6 41	.941 110	8.401 9.717	220	251					. 00			
3əbə PCI	133 11 9	33 119.883	0	-1.159	-1.209	.310 91.8	. 319 98.01.18 . 19	59.5	31	0311 NDL	10	0 41	. 100 10	4 000	100	. 001	652	975 179 9	265	196 2 1	. 42	67	56 1	0.4
3560 PCO	17 5 36.6	91 -96,978	331	214			. 51			3930 KES 2027 PEI	199 1	10 14	205 1	4.900	14	~. 072	000 550	525 120 A	348	174 9 1	1.01	76	56.8	. 04
DECO DOT	50 0 14 5	15 101 415		000			1 9.6			2061 DIE	697 1	17 45	205	1 516	100	- 070	- 075	020 120.4	079	94 9	24	19	39 1	07
SODS PUL	10 9 14.4	10 101.427 49 95 669	90	080	- 710	105 997 1	1.00	18 5	7.7	3963 RKC	173 1	10 - 34	008 11,	7 104	300	- 551	- 704	432 48 9	. 015	49 7	81	24	91.0	. 30
0000 FD3	100 10 01.1	90 - 119 209 99 - 119 209	. 00 - A	131	-, 113	165 197 9	294 07 9 76 59	51 0	- 10	3065 RKT	783 1	16 - 23	2 118-13	1.104	100	- 155	- 166	053 32 6	189	99 9	51	40	39.2	- 29
3370 EDI 2577 DDC	- 155 12 - 09,0 - 241 12 - 22 0	33 112.(U3 70_117 957	615	- 008	229	270 50 3	061 8 1 1 08 1 00	15 E	. 10	3974 RMP	13	6 41	911 15	7. 512	379	263	. 100	.000 02.0	. 100	00.0	. 38	. 10	001 0	
9509 DDI	21 11 -22 1	10-111.201	680	. 056	117	208 265 8	128 111 7 1 04 - 98	12 1	- 97	3975 RM()	172 1	13 - 26	540 14	8 800	360	185	028	543 88 3	256	125.3	99	. 52	72.5	. 57
3584 PEX	11 5 30 4	67 - 87 - 183	003	- 262		. 200 200.0	1 66	12.1	1	0010 ILIN	112	10 20		0.000	000	. 100	. 0 20		1 200	1 2 0 1 0		101		
9599 DET	207 13 53 0	17 158 650	0	1.47	220	280 30 3	213 38 8 82 60	15 9	09	4013 RSCP	90	4 35	600 -8	5 589	580	239	377	. 370 264.6	. 472	66.4	. 95	. 63	56.0	19
3594 PEO	86 12 33 6	09 - 116 155	1279	- 279	- 343	432 89.6	. 309 101.1 1.08 .58	70.6	. 78	4017 RSNT	393	17 62	. 480-11	4.592	50	143	124	. 190 231. 3	. 223	46.1	. 83	. 68	31.9	26
3598 PCC	211 13 18 6	50-123 151	1	- 065	- 115	345 255 0	409 150 9 1 09 81	45 4	58	4018 RS0	289	15 60	. 572-153	2.788 1	921	030	.003	.123 245.8	. 084	67.7	. 32	. 26	34.9	. 42
3599 PGD	10 5 43.8	75 11.721	1600	248	9	.010 200.0	. 100 100.0 1.00 1.01			4020 RSSD	381	14 44	.154-10-	4.062 2	2059	088	072	.216 269.9	. 267	169.4	. 84	. 54	59.0	. 20
										4041 RUV	791	17 -15	5.189-14	7.384	3	. 159	.163	.056 141.5	. 081	48.7	. 47	. 44	12.9	. 03
3601 PGF	193 17 42.5	48 9.144	1129	062	082	.171 102.3	.187 46.2 .97 .89	16.0	. 05	4063 SAD	17	6 33	8.822 7	3.183	\$37	363				1	1.21			
3604 PGP	35 5 13.4	80 120,960) ()	309			. 36			4070 SAL	13	6 45	675 10	0.612	70	. 876				1	1.56			
3611 PHC	52 9 50.7	00-127.433	32	081			1.14			4073 SA0	187	13 36	5.765-12	1.445	230	120	112	.100 294.6	. 192	164.0	. 66	. 56	27.7	10
3631 PII	14 7 43.7	62 10.588	50	190			1.03			4082 SBA	65	9 -77	7.850 16	6.756	37	311				ſ	1.06			
3636 PIP	20 5 18.3	25 120.619	150	038			. 63			4086 SBF	371	18 43	3.981	7.452	817	.118	.118	.038 168.4	. 050	110.2	. 51	. 50	4.1	. 00
3651 PKI	348-18 27.6	10 85.490	2757	.165	.165	.136 27.1	.142 78.7 .72 .64	21.1	-, 41															
3660 PLC	94-12 - 37.7	63-122.012	462	011	.013	. 258 150.7	. 275 175.4 1.03 .88	27.8	55	4102 SCH	415	17 54	.817 -6	6.783	540	.075	. 086	. 235 236. 7	. 144	77.2	. 58	. 35	63.7	33
3669 PLP	19 5 11.1	65 124.979	133	572			1.00			4107 SCO	332	17 70). 483 -2	1.950	68	.077	. 086	.130 189.9	. 155	4.6	. 57	. 46	35.3	. 06
3678 PME	110 11 61.7	33-149.167	231	002	. 008	. 053 289.4	. 199 158. 9 . 94 . 89	11.0	. 05	4124 SDI	11	6 41	.758 13	3.954	0	. 032					1.59			

4126 SDN 340 15 55.413-160.622 23 .280 .291 .242 139.6 .103 45.9 .71 .53 43.1 .49 . 87 23 9 8.886 -70.633 1580 .159 4129 SDV 1136 SEK 186 16 -28.323 27.625 1485 .000 .007 .145 213.5 .065 95.3 .65 .59 18.4 -.19 . 356 . 237 55.4 . 088 171.9 . 81 . 71 23.9 . 75 1141 SES 108 16 50.396-111.042 769 .386 10 7 43.960 11.870 0 .418 1.09 10 6 40.633 15.384 0 -.438 . 65 46 7 40,633 48,633 0 .267 4181 SHE .387 .199 357.5 .174 7.1 .54 .42 37.7 .60 96 10 34.530 132.678 284 .371 1187 SHK . 70 4188 SHL 58 7 25,567 91,883 1600 .452 1211 SIT 288 14 57.057-135.324 18 -.304 -.293 .096 131.5 .097 159.1 .14 .39 24.3 .23 41 8 18,112 -66,150 456 -.012 4221 SIG . 337 . 118 124.3 . 182 160.8 . 80 . 71 21.7 . 26 4238 SK0 379 17 42.021 21.496 345 .338 1.19 21 9 50.667 156.100 0 .102 1239 SKR . 95 11 5 60.477 13.323 119 .426 1256 SLR 366 17 -25.753 28.420 1348 .071 .068 .042 140.1 .086 72.3 .69 .67 5.6 -.30 1265 SMF 593 17 46.645 3.841 458 -.057 -.064 .135 38.2 .056 46.4 .42 .34 33.8 -.29 1271 SWT 39 8 38,467 70,067 0 .289 1278 SMY 282 12 52.722 174.120 16 .246 .255 .158 311.7 .084 178.5 .40 .30 46.0 .57 1280 SXA 138 13 -70.309 -2.358 52 .169 .194 .321 96.6 .242 106.0 .90 .67 45.0 .12 . 48 73 9 50, 586 4, 133 108 .051 1285 SMG - 379 15 - 7.173 100.620 - 4 - .196 - .125 - .245 - 52.8 - .217 - 97.2 - .55 - .33 - 63.8 - .28 1297 SNY 512 11 41.828 123.578 54 -.024 .004 .160 60.7 .046 .9 .63 .57 19.6 .41 1.15 25 6 34.380 134.908 370 .116 1298 887 1301 S0C 11 7 13.583 39.717 192 .148 . 84 4307 SOI 11 6 38.121 16.099 0 -.270 1317 SPA 1190 17 -90.104 115.000 2927 -. 251 -. 255 .134 167.0 .159 22.9 .57 .44 39.4 .19 1319 SPC 57 10 49.188 20.245 1771 .382 .393 .321 137.9 .192 55.7 .82 .49 64.3 .66 1323 SP1 107 15 57.160-170.225 0 -.307 -.267 .190 214.6 .184 19.7 .73 .63 24.7 .06 1339 SQTA 334 16 47.255 11.287 1307 -.061 -.056 .111 144.6 .122 1.8 .57 .51 20.8 .05 1.14 4344 SRD 33 9 6.932 -72.853 1639 .186 1352 SR0 69 9 47.813 18.313 0 .088 1.20 1364 SSE 833 15 31.096 121.187 9 -.212 -.203 .098 98.2 .112 52.8 .51 .47 17.5 .35 1365 SSF 669 17 17.061 3.507 360 -.103 -.108 .009 322.4 .085 69.0 .42 .39 10.9 .48 . 96 60 8 36,925-116,219 2065 .281 1374 SSP 4381 STA 23 7 17.695 74.000 665 .399 . 83 1.30 11 5 50.703 6.900 270 -.097 4382 STB 1389 STJ 18 10 47.572 -52.733 61 .271 .298 .234 232.1 .083 85.7 .79 .67 28.1 -.39 1390 STK 599 17 -31.882 141.592 212 -.549 -.550 .092 78.7 .066 77.3 .94 .92 4.3 .76 .143 177.5 .58 .38 57.3 -.29 4397 STU 102 12 48.771 9.193 375 .102 .173 .254 206.1 18 6 61.120 4.860 9 .252 4104 SUE .039 43.1 .60 .43 47.0 -.20 4405 SUF 183 15 62,719 26,150 185 -.098 -.043 .279 224.1 80 14 -32.380 20.728 0 .100 .092 .064 271.1 .088 36.3 .62 .59 8.8 .04 4412 SUR .950 .732 215.3 .307 32.5 1.20 .53 80.3 .60 70 10 56,800 60,633 275 .735 1436 SVW 586 17 61.182-155.633 762 .079 .060 .187 27.5 .181 72.9 .79 .68 26.3 .27 18 12 -27.182 25.325 1342 .042 -.068 .252 76.3 .512 56.8 1.36 .89 57.6 -.24 1119 SWZ 1.48 74 9 25.033 121.517 8 .260 1179 TAP 1182 TAT 96 13 34.983 139.867 0 .448 .555 .308 348.1 .359 86.6 1.03 .65 59.3 .67 1490 TB1 221 16 23.349 149.461 9 .073 .081 .068 180.3 .061 18.4 .74 .73 3.8 -.13 .046 126.0 .076 123.1 .34 .31 19.9 .21 4503 TCF 622 17 46.288 2.210 592 -.179 -.177 . 68 4549 THRI 19 6 -8.370 115.543 1000 .140 1555 T1A 256 13 36.211 117.124 300 .108 .073 .119 261.4 .358 85.6 .72 .35 76.7 .74 . 268 108.6 . 96 . 71 45.3 . 72 4556 TIC 277 17 6.550 -5.000 137 .024 .042 .282 154.2 . 286 . 225 40.5 . 155 79.1 . 95 . 81 28.2 . 18 4562 TIK 56 11 71.633 128.867 0 .241 4569 TIY 454 15 37.713 112.434 850 - 211 - 341 .773 172.4 1.028 87.3 2.42 1.62 55.3 - 65 17 2 35,730 -83,840 349 -.555 4578 TKL

1.19 4588 TLG 20 9 43.267 77.383 850 .086 1621 TXP 585 16 38.220-117.227 1932 -.308 -.320 .115 95.5 .039 142.2 .50 .46 15.7 -.12 4626 TOA 344 15 62.147-146.223 908 .478 .460 .435 40.3 .209 104.2 1.06 .74 51.5 .54 4632 TOL 82 15 39.881 -4.049 479 -.105 -.017 .667 133.0 .095 89.61.49 .97 57.2 .34 4635 TOO 323 13 -37.571 145.490 603 -.140 -.125 .153 296.2 .285 41.2 1.12 1.00 20.8 .26 1.24 4640 TOV 16 5 9.820 -69.876 649 .033 4651 TPN 168 15 -8.419 146.987 989 -.139 -.181 .282 90.0 .219 122.5 1.20 1.04 24.8 .27 4655 TPT 771 17 -14.984-147.620 3 .114 .117 .145 180.1 .095 91.5 .51 .42 34.0 .23 1.52 18 9 10.650 -61.400 24 -.219 4674 TRN 1.40 4675 TRO 47 8 69.632 18.928 14 -.103 4680 TRT 218 13 -7.650 112.500 0 -.176 -.228 .262 42.2 .273 142.8 1.23 1.03 29.2 -.11 96 4689 TSI 10 4 3.508 98.695 0 .460 90 9 4,223 118,072 0 .423 4692 TSM 4700 TTA 690 16 62.930-156.022 913 -.150 -.139 .119 58.7 .144 177.1 .63 .54 26.6 .19 . 639 354.4 . 256 58.6 1.31 1.06 35.1 .18 30 10 -33.297 19.150 189 -.029 -.259 4716 TUH .025 131.5 .199 114.7 .71 .62 22.9 .33 4718 TUL 528 17 35.910 -95.793 256 .026 .019 . 270 162.4 .118 31.4 .62 .40 57.6 .30 4730 TV0 543 17 -17.782-149.252 660 .276 .295 .177 292.2 .156 143.0 1.06 .98 13.8 -.48 4751 TXAR 133 12 29.338-103.670 1013 -.762 -.782 . 485 353.4 . 234 4.2 . 72 . 52 47.8 -. 67 41 10 51.567 94.083 0 -.024 .173 4772 UER t. 31 4778 UKR 17 7 50,950 84,750 0 -.241 4782 ULM 112 13 50.397 -95.950 280 .204 .229 .151 235.6 .236 140.9 1.27 1.16 16.9 -.26 . 84 4793 UPA 75 8 9.115 -79.540 41 .314 4795 UPP 126 13 59.858 17.627 14 .428 .397 .344 100.1 .132 166.8 .86 .62 48.4 .29 . 239 . 078 139.6 . 287 171.4 1.24 1.15 14.8 -.30 4819 UZH 121 14 48.633 22.300 0 .246 .122 134.0 .103 44.6 .46 .37 34.0 .27 4824 VAH 763 17 -15.237-147.636 3 .117 .709 19.4 .639 99.7 1.87 1.37 46.5 -.48 4833 VAY 284 13 41.361 22.601 167 -.323 -.555 90 11 45.545 15.316 259 .213 .197 .224 118.1 .149 167.4 .49 .35 49.8 .08 4838 VBY 1.20 15 6 -28.080 26.863 1340 .429 4878 VIR . 225 60.5 1.23 1.11 18.4 -.54 . 286 179.2 55 13 48.265 16.318 400 .373 . 344 4882 VKA . 76 32 9 43.117 131.900 74 .258 4884 VLA 4903 VNDA 145 15 -77.640 161.956 97 -.354 -.362 .283 271.1 .154 110.2 1.59 1.50 11.2 -.02 1.41 4909 VOY 36 8 46.167 13.985 1072 -.176 4918 VRAC 57 10 49.390 16.700 0 .106 .185 .176 219.4 .419 48.5 .82 .57 51.2 .43 93 10 7 46.129 12.486 514 .229 4939 VVI 4955 WAL 203 14 47.460-115.965 0 -.163 -.150 .252 223.8 .224 9.4 .99 .83 30.6 -.26 219 14 52.242 21.024 109 -.327 -.220 .224 186.3 .243 25.3 .72 .65 19.4 .43 4958 WAR 4960 WAT 180 15 -30.317 115.883 0 -.055 -.024 .076 283.0 .225 27.7 .54 .37 52.7 .19 4962 WB2 169 13 -20.028 134.360 425 -.062 -.035 .039 106.4 .49 .27 69.4 -.11 . 233 179.5 . 379 155.9 1.12 .74 55.7 .21 4985 WDC 257 13 40.580-122.540 300 -.240 -.391 . 496 241.6 4997 WET 323 15 49.145 12.880 612 .032 .057 .077 177.2 .167 22.6 .51 .42 32.4 -.08 5017 WHN 575 15 30.544 114.350 26 -.015 -.017 .335 204.6 .422 97.5 1.37 .97 49.7 .32 .074 2.1 .086 11.2 .77 .75 6.2 -.40 5021 WHY 210 15 60.747-135.007 1292 -.051 -.042 5029 WIN 161 14 -22.567 17.100 1728 .002 -.046 .157 312.9 .130 76.9 .84 .80 9.9 -.12 .347 212.2 .204 45.8 .89 .67 42.6 -.37 90 13 49.796 6.174 0 -.148 -.066 5047 WLF . 42 5059 WME 16 6 53,516 -4,334 129 -.149 201 15 34.718 -98.589 504 -.143 -.259 .582 47.8 .317 153.7 1.38 .96 50.9 .41 5061 WMO 5062 WMQ 556 17 43.821 87.695 970 .072 .073 .082 101.3 .042 20.2 .46 .43 12.1 -.02 .098 281.6 .182 74.4 .69 .61 22.2 -.63 5082 WOOL 224 15 -31.073 121.678 0 -.436 -.448 .053 60.4 .192 95.5 .49 .35 47.4 -.37 5095 WR2 320 15 -20.068 134.472 414 -.261 -.268 .060 170.7 .139 73.6 .40 .31 41.9 .32 5099 WRA 1110 17 -19.948 134.351 0 -.234 -.236 .114 128.6 .061 159.8 .40 .34 28.9 .13 5117 WTS 806 18 51.995 6.810 43 .034 .034 .050 114.6 .029 116.9 .59 .58 2.9 .33 5118 WTTA 313 17 47.388 11.663 1764 -.015 -.016 5127 WVOR 237 13 42.439-118.667 1343 -.010 -.026 .195 134.9 .209 97.1 .70 .54 41.1 -.23 5138 XAX 619 17 34.040 108.921 629 -.094 -.106 .119 143.5 .134 89.0 .70 .64 16.3 .21

Appendix B-2: Station Correction for travel time 5146 YAK 209 14 62.017 129.717 0 .398 .406 .237 146.6 .227 108.2 .74 .63 28.7 .09 5151 YBH 159 11 41.868-122.805 968 -.091 -.151 .318 213.7 .106 163.3 .84 .70 29.6 .44 91 5160 YKA 46 9 62.579-114.646 0 -.398 ist ste Neve Nw lat, lon, elev ave a0 al dirl a2 dir2 rms0 rms1 vr corr 5162 YKC 257 16 62, 478-114, 473 197 -. 147 -. 158 .036 173, 4 .166 151, 9 .64 .58 20, 2 .02 1.02 5168 YKU 15 6 59,581-139,836 19 .337 1.73 13 AAI 80 8 -3,700 128,167 79 .009 . 405 1.88 SISE YOU $11 \quad 5 \quad -34. \quad 278 \quad 148. \quad 382 \quad 503$ 18 AAS 21 4 -62,160 -58,463 14 .523 1.58 , 220 -. 017 . 616 357.7 . 301 91.1 . 90 . 70 39.3 . 27 5186 YRH 70 11 52,835 -4,740 300 46 ACO 50 11 36.699 -99.146 521 -.540 -.227 .073 118.0 .300 29.3 .62 .59 10.6 -.16 5189 YSNY 101 14 42,558 -78,575 628 .041 .028 .325 216.6 .212 132.6 1.35 1.17 24.6 .42 . 63 ADE 269 14 -34.967 138.709 654 .015 .728 1.326 244.4 .884 75.0 1.93 1.55 35.2 .31 66 ADK 647 15 51.863-176.655 0 -.365 -.203 .337 304.0 .673 170.6 1.30 1.17 18.6 -.16 5190 YSS 271 14 47.033 142.860 97 .073 .091 .077 51.0 .157 100.7 .62 .56 19.2 .22 82 AFR 522 17 -17.538-149.778 50 1.263 1.270 .185 47.6 .086 127.3 .59 .57 6.0 .25 5204 ZAK 202 13 50.383 103.283 0 .134 .146 .318 26.9 .206 154.9 .76 .57 42.5 -.69 21 7 38.795 -27.232 79 1.709 . 97 83 AGA 3.35 14 6 47.082 -69.023 238 2.023 88 AGM 5224 ZST 137 14 48.196 17.103 250 -.187 -.188 .309 321.2 .140 175.7 1.51 1.38 16.0 .28 1.73 90 AGR 11 6 27.133 78.017 163 1.922 116 AKRL 16 4 23,660 32,710 0 1.378 1.77 . 95 117 AKSR 19 6 23.672 33.021 0 1.771 118 AKU 543 18 65.687 -18.107 24 1.795 2.190 .872 175.0 .711 6.0 1.21 .89 46.0 .56 124 ALE 382 18 82.483 -62.400 64 -.118 -.192 .866 28.7 .089 60.2 .75 .40 71.1 -.59 134 ALQ 961 17 34.942-106.458 1853 .248 .221 .184 176.8 .067 .7 .35 .32 16.7 .41 172 ANM 192 14 64.705-165.417 330 .438 .469 .086 51.7 .409 85.0 .43 .29 53.1 -.01 173 ANN 117 9 44.883 37.300 0 -.143 . 85 1.71 177 ANT 29 8 -23,699 -70,415 79 .404 12 5 67.550 33.333 0 -.149 186 APA 194 APO 18 11 60.590 14.030 340 -.815 -.814 .152 223.8 1.440 24.8 1.96 1.63 31.0 .51 10 7 42.354 13.403 720 .965 202 AQU .051 .440 250.7 .359 100.9 .80 .69 26.5 .30 213 ARC 208 18 40.877-124.075 59 .079 214 ARE 12 5 -16.571 -71.563 2451 .755 . 80 221 ARMA 172 11 -30.448 151.730 1129 .560 .451 .315 42.3 .422 126.1 .73 .70 8.1 -.66 227 ARU 184 13 56.400 58.600 250 -.621 -.172 .164 207.7 .839 162.1 .82 .52 59.2 .27 11 6 43.635 13.021 0 .327 . 50 228 ARV 229 ASA 245 14 43.770 142.373 111 -.687 -.770 .556 302.0 .078 76.3 .67 .50 44.1 -.06 . 82 234 ASH 105 9 37.950 58.350 219 .835 241 ASP 978 16 -23.683 133.897 600 -.893 -1.062 .394 320.1 .330 30.0 .79 .68 25.0 -.40 1.16 10 5 43,105 12,762 0 ,496 243 ASS 280 AVF 623 17 46.855 3.376 224 -.319 -.324 .122 183.4 .315 13.9 .32 .21 55.9 .29 304 BAG 128 10 16.411 120.580 1506 -.742 -.705 .869 301.9 .707 111.8 .90 .37 82.8 .28 308 BAL 207 12 -30.665 116.772 300 -.774 -.716 .101 201.0 .223 7.7 .26 .17 54.7 -.26 2.0733 5 26.215 50.457 0 -.035 332 BBI 333 BLA 134 15 41.550 41.673 500 -.261 -.355 .427 296.9 .373 73.8 .71 .60 28.1 .00 92 13 -15.788 -47.933 1254 -.080 -.139 .824 58.0 .529 163.3 .80 .45 68.6 -.33 353 BDF 356 BDI 17 7 44.173 10.720 0 -.060 . 34 362 BDT 526 14 17.233 99.050 0 -.642 -.411 .857 173.3 .656 11.0 .94 .64 53.9 .38 77 11 42.862-109.582 2190 -.292 -.336 .295 328.9 .290 18.2 .38 .21 68.4 .68 365 BDW 2.31 371 BEE 59 9 26.017 50.522 0 -.484 1.15 384 BEW 15 6 -32.415 22.630 870 .309 386 BFD 166 12 -37.176 142.544 234 .018 .488 .447 188.1 .649 101.1 .87 .59 54.7 -.32 . 720 79.7 . 317 175.5 1.32 1.20 18.2 .24 390 BFS 111 14 -26.898 26.785 1309 -.874 -.605 391 BFT 101 14 -25.687 30.043 1868 .673 .801 .199 194.7 .324 126.8 .69 .63 15.6 -.18 395 BGC 53 13 37.962-122.170 610 -.885 -.564 .533 189.5 .357 105.6 .83 .68 34.0 .09 592 17 46.558 2.846 389 -.190 -.145 .268 170.6 .176 4.0 .36 .29 35.0 .45 397 BGF 412 BHG 292 15 47.721 12.879 174 .415 .093 .523 7.6 .160 93.6 .51 .34 54.1 .24 . 39 418 BHO 13 7 34.508 -94.873 143 -.187 432 BING 149 13 42.157 -76.067 407 -.089 -.030 1.148 101.6 .421 165.4 1.15 .74 58.3 -.37 1.41 440 BJA 24 6 25.992 50.608 0 -.350 441 BJ1 691 16 40.040 116.175 13 -.107 .176 .413 300.8 .092 27.5 .56 .48 28.2 -.08

445 BKB 12 4 -1.283 116.833 0 3.372

995 CVP 66 11 17.600 121.700 0 .772 .967 .945 251.4 .420 40.7 1.38 1.13 32.4 -.17 456 BKS 693 16 37.877-122.235 275 .832 1.180 .430 93.2 .362 174.4 .61 .43 49.9 .21 .519 35.5 .80 .68 28.2 .25 . 323 213. 8 1011 CYP 301 16 51.380 23.000 0 .064 .159 460 BLA 390 16 37.211 -80.421 634 -.144 .142 .569 108.8 .495 94.9 .60 .21 87.9 .51 1025 DAG 910 18 76.770 -18.770 16 -.670 -.468 .415 168.3 . 200 154.8 . 48 . 34 49.1 . 46 32 11 -33,900 18,645 78 1.582 .792 2.616 134.1 1.749 56.4 1.87 1.23 56.5 -.08 162 BEE .463 5.7 .45 .25 69.1 .37 1029 DANN 82 11 28.350 83.760 2500 -.003 .129 .340 17.1 163 BLF 186 15 -29,109 26,188 1419 -.181 -.453 .598 5.2 .316 63.5 .62 .47 43.0 -.59 . 99 474 BLS 30 8 59,450 6,590 1169 1,130 1.49 32 7 7.088 125.575 85 .328 190 BMN 262 13 40.563-117.267 1504 .478 .484 .195 312.8 .231 10.7 .32 .23 46.8 .38 43 10 -5. 550 150. 467 250 -. 009 -. 203 . 974 352. 8 . 906 54. 6 . 88 . 33 85. 5 -. 33 1034 DAW 501 BNG 160 17 1.367 18.567 0 -.377 -.315 .291 267.5 .307 99.1 .58 .49 28.3 .54 1037 DBIC 38 13 6.701 -4.913 25 -1.040 -.868 .482 253.5 . 246 34.3 .71 .58 31.7 .14 . 73 503 BM 10 6 45.077 6.752 0 .724 1048 DCN 258 16 53, 343 -7, 278 150 . 255 .838 140.6 .089 97.9 .84 .59 49.5 .14 . 515 507 BNS 131 11 50.964 7.175 200 .242 .453 .222 126.0 .570 133.8 .46 .19 83.6 -.16 16 6 53.387 -6.339 85 -.264 . 40 1055 DDK 1095 DL2 420 13 38.906 121.628 61 .212 .314 . 376 98.8 .68 .59 23.5 -.01 . 234 35.7 512 B0B 11 7 44.770 9.582 930 .593 . 369 57.8 . 597 143.0 1.10 . 98 20.8 - 50 1098 DLE 184 15 53.287 -6.544 140 .146 .291 514 BOD 222 14 57.850 114.183 0 -.806 -1.054 .652 153.0 .378 77.7 .64 .40 60.6 -.17 1099 DLF 158 15 53, 296 -6, 531 96 . 273 . 228 .198 92.0 .091 160.6 .43 .39 15.7 -.35 39 12 31,598 -64,546 1200 -.328 -.616 .322 44.2 .891 70.4 .97 .78 35.9 -.31 525 BOS .059 56.0 .349 10.8 .49 .41 27.9 -.16 1110 DMN 371 18 27.690 85.160 2224 -.056 .023 55 13 -26,175 28,030 1700 -.777 -.822 1.459 336,3 1.679 2.6 2.18 1.34 62.3 .10 532 BPI . 391 . 741 113.1 . 396 124.9 . 83 . 54 57.6 . 33 1113 DMC 257 14 53.899 -6.911 280 .201 546 BRF 10 5 26.073 50.583 0 .966 2.78547 BRG 282 16 50.874 13.946 296 .275 .217 .179 46.8 .419 96.6 .49 .37 42.7 .10 556 BRS 119 10 27.392 152.775 524 -.372 -.118 .363 278.1 .704 55.5 .54 .36 56.0 .35 1126 DOI 20 7 44,535 7.354 1014 -.430 1.53 .160 .384 76.2 .378 117.9 .48 .26 69.6 .36 1133 DOU 116 16 50.210 4.692 224 .199 . 43 557 BRT 14 6 40.878 17.204 0 .124 1.20 26 6 50.433 16.511 759 .855 559 BRV 208 15 71.274-156.785 14 -.482 .011 .716 301.8 .313 150.7 .86 .66 40.9 -.15 1137 DPC . 87 1151 DRLN 23 9 49.310 -57.542 238 -.373 564 BSD 306 16 55.110 14.910 87 -.356 -.357 1.316 333.0 .945 108.6 1.25 .55 80.7 .01 1175 DUG 440 16 40.195-112.813 1476 .433 .286 .251 173.7 .227 156.3 .31 .18 66.4 -.21 . 294 225.5 . 277 17.6 . 48 . 43 21.4 . 08 1202 EAB 148 15 56.188 -4.340 250 -.191 -.049 566 BSF 196 18 47.832 6.792 1200 -.511 -.408 .088 125.9 .230 150.7 .40 .36 19.7 .38 . 260 130.1 .171 14.4 .26 .15 68.2 -.39 1206 FAU 124 14 55,845 -3,455 349 ,157 1.88 76 9 5,500 95,317 0 -1.041 567 BSI . 262 24.9 . 25 . 11 80.3 -. 39 586 BTO 228 13 40.598 110.018 1120 .115 -.044 .384 212.6 .758 85.7 .58 .28 77.1 .52 1210 EBH 142 14 56.248 -3.508 375 -.021 . 094 . 370 166. 7 1212 EBL 100 14 55.773 -3.044 365 .157 . 579 127.4 . 440 135.5 . 90 . 70 38.3 . 10 598 BUL 88 16 -20.143 28.613 1340 -.195 -.658 1.103 62.7 .385 87.9 1.53 1.26 32.7 .15 . 299 111.8 . 148 143.5 . 34 . 25 46.7 -. 12 1218 ECB 186 15 52.366 -6.781 125 .111 618 BW06 581 17 42.767-109.632 2223 -.362 -.557 .275 276.2 .142 128.1 .40 .33 29.9 641 (AF 575 17 14,926 2.065 629 .190 .053 .318 95.1 .143 24.9 .36 .25 51.1 .21 1227 ECP 337 15 52.180 -6.369 4 .175 .186 .114 112.9 .157 17.7 .22 .17 42.8 -.05 10 10 10.507 -66.927 1031 -.621 .014 .890 61.3 .917 99.3 1.07 .61 66.8 .07 649 CAR . 521 217.4 . 192 18.3 . 40 . 30 43.0 -. 59 78 13 55,923 -3,186 125 .003 .230 . 536 166.6 . 249 27.2 . 72 . 56 39.2 . 10 1234 EDI 671 CBK 141 12 48.947 -57.997 379 -.375 -.392 . 268 353.0 . 227 81.7 . 42 . 33 36.8 . 10 1236 EDM 280 16 53.222-113.350 730 -.296 -.396 672 (BM 54 14 46.932 -68.121 250 -.010 .059 .746 138.3 .564 12.0 .86 .51 64.8 .41 .111 347.2 .208 47.2 .37 .33 19.6 -.33 673 (BN 60 10 38, 205 -77, 373 70 . 430 . 647 . 758 114.9 . 284 178.7 . 83 . 50 64.5 . 50 40 14 56,934 -2,604 388 -,177 -,162 1237 EDR .193 247.6 .114 167.5 .39 .36 16.0 -.19 1239 EDU 136 13 56.548 -3.014 275 -.196 -.009 . 350 195.2 . 524 171.9 . 61 . 45 47.0 . 29 1258 EKA 878 17 55.333 -3.159 229 -.185 .004 692 CCM 44 8 38.107 -91.346 223 -.525 1.53 1271 ELK 103 10 40.848-115.288 2210 .540 .439 .128 286.8 .171 105.0 .35 .31 19.4 -.47 702 (D2 566 16 30.910 103.758 628 -.282 -.076 .591 332.1 .478 152.5 .70 .50 48.2 -.37 .583 208.7 .597 26.0 .59 .20 87.9 .46 1274 ELO 132 15 56.471 -3.712 495 -.284 -.012 707 CDF 163 17 18.394 7.271 1100 -.345 -.372 .225 55.4 .297 148.5 .46 .37 36.0 .45 23 9 53.250 86.267 0 -1.023 95 722 (EH 159 17 35.891 -79.093 151 -.354 -.159 .849 106.8 .124 80.9 .81 .50 62.0 -.13 1279 ELT 1299 EXX 831 18 50.767 5.923 119 .229 .420 .247 140.9 .115 127.6 .40 .35 24.1 .01 727 (ER 103 14 -33, 362 19, 295 472 -, 596 -, 425 , 714 89, 8 , 794 98, 5 1, 41 1, 17 30, 8 , 14 11 5 39.362 9.297 1049 .933 . 77 1306 EPF 571 17 43.031 .340 750 -.255 -.073 .614 213.3 .093 9.3 .58 .36 60.1 .40 1.77 747 CGP 95 9 8.455 124.694 50 -.934 88 15 46.323-122.150 1608 -.072 -.044 .616 251.2 .666 11.1 .96 .72 44.8 .19 1332 ESD 752 (GY 16 7 -26, 348 26, 375 0 -. 624 3.40 348 164 1 . 362 33.8 . 50 . 42 30.0 . 42 1234 ESK 270 14 55.317 -3.200 241 .123 .125 761 (HG 609 16 18, 790 98, 977 416 , 279 , 053 , 582 137, 0 , 014 102, 6 , 50 , 25 74, 3 , 62 . 258 164.6 . 195 149.2 . 34 . 25 44.2 - 14 1342 ESY 140 14 55.918 -2.615 324 -.199 -.125 771 (HT 663 18 22.350 91.817 14 .338 .043 .450 127.8 .110 105.7 .44 .28 59.2 .18 . 285 132.2 . 201 51.6 . 37 . 25 53.4 -. 14 1345 ETA 176 15 52.696 -6.210 140 .290 . 328 . 217 39.9 . 109 149.1 . 27 . 21 35.0 . 33 1359 EUR 204 13 39.483-115.967 2177 .452 . 433 15 8 44, 499 8, 399 0 -. 015 1.02 797 CKL . 754 139.2 .88 .58 55.8 .45 1361 EVA 55 13 -26.555 29.170 1621 .553 .849 456 354.7 813 CLL 277 15 51,309 13,004 230 -.185 -.123 .163 273.9 .199 85.0 .47 .26 70.5 -.29 1371 EYMN 116 10 48.062 -91.600 474 -.972 -.596 .665 62.4 .661 80.8 .74 .45 63.5 -.18 . 301 73.5 .56 .38 53.9 -.01 827 (MA 140 15 64.290-149.180 180 .345 .133 .459 163.4 .661 9.1 .196 149.2 .60 .34 66.9 .51 1381 FBA 826 16 64.860-147.835 180 -.530 -.413 . 577 173.2 .88 .73 30.0 .48 828 CMB 301 14 38.035-120.385 718 .330 . 662 . 402 3. 5 .177 98.2 .47 .45 8.4 .46 70 11 58.762 -94.087 39 -.457 -.510 .065 8.7 . 345 36. 0 . 235 167.9 . 58 . 52 17.3 . 54 841 CMS 152 11 -31, 487 145, 828 254 .093 -.102 847 (N2 764 13 43, 801 125, 448 230 -, 336 -, 436 , 101 219, 7 . 402 108.6 . 37 . 21 68.3 -. 28 1399 FFC 770 16 54.725-101.933 337 -.310 -.433 .239 350.2 .174 53.8 .41 .34 30.5 .53 . 219 53.2 .68 .52 41.7 .19 848 (NB 239 12 -35, 315 149, 363 850 .652 .820 .469 99.5 65 9 40.802-123.985 610 1.106 1.18 880 COL 218 13 64,900-147,783 182 - 385 - 263 .788 23.7 .119 151.9 .72 .44 62.5 .50 1408 FHC 1415 FIN 149 16 44.209 8.208 589 -.633 -.534 .206 162.6 .232 106.3 .47 .40 26.5 -.26 . 226 84.8 .68 .41 63.6 .13 883 (00 138 13 -30,578 151,892 652 -.473 -.446 .739 282.4 1419 F1TX 61 13 -18, 192 125, 728 109 -. 670 -. 451 . 720 182, 6 . 660 1.4 . 74 . 45 63.8 . 74 884 COP 476 16 55.683 12.433 13 .738 .809 .180 65.3 .496 112.6 .66 .56 29.3 -.27 1.78 18 4 35.363 -97.386 351 -.018 1424 FKO .182 279.0 .062 94.8 .19 .13 53.3 .06 785 17 48,763 -. 482 0 -. 348 -. 383 1431 FLN . 61 19 7 44.585-123.303 123 1.199 885 COR . 440 255.0 . 507 168.3 . 76 . 50 57.4 . 26 91 11 40.863 -73.885 24 -.590 -.326 39 10 40.673-112.190 2227 - 992 - 694 .446 149.1 .405 74.6 .90 .75 29.5 .50 1455 FOR 909 CPL .192 104.5 .506 94.0 .59 .46 39.3 .28 436 16 63.747 -68.547 17 -.524 -.115 . 48 1463 FRB 913 CP7 12 6 50,210 -5,585 197 ,257 508 17 43.657 6.768 310 -.250 -.199 . 272 188.2 . 166 179.5 . 35 . 26 44.7 - 03 960 (S) 360 14 -66.344 110.639 56 .112 -.403 1.259 105.1 .167 8.8 2.57 2.41 12.4 -.27 1466 FRF 1475 FRS 186 15 -29.750 25.322 0 -.221 -.328 .674 338.2 .057 174.9 .88 .75 26.9 -.29 962 CTV 513 14 -20.088 146,255 356 -.235 -.105 .533 234.1 .087 164.0 .53 .40 41.2 .52 990 (VF 103 13 42.568 8.870 529 -.193 -.177 .114 196.1 .133 147.2 .35 .33 13.6 .32

2258 KAF 365 16 62.113 26.306 204 -.598 -.409 .200 174.5 .381 115.6 .38 .20 73.1 .48 97 20 7 42,833 74.617 0 .635 1477 FRU 1.77 2263 KALI 13 6 -7.106 106.659 810 -.661 1495 FLR 318 15 48.166 11.276 564 .430 .311 .350 .2 .096 108.7 .43 .35 33.1 .13 2276 KBA 682 17 47.184 13.447 1720 -.052 -.057 .040 127.7 .570 179.0 .49 .28 68.4 .31 . 64 11 6 46,682 12,909 0 .025 2300 KDC 467 16 57.748-152.492 0 -.275 -.016 .371 62.0 .370 36.6 .42 .21 73.9 .20 1497 FVM 447 15 37.990 -90.510 310 -.812 -.749 .216 84.3 .151 58.9 .45 .40 18.9 -.09 2.62 2311 KED 35 6 12,926 -12,321 0 -.220 . 88 1506 GAC 38 7 45.703 -75.470 112 -.361 . 154 . 580 323. 1 . 792 125. 8 . 59 . 22 86. 3 -. 41 49 10 39.000 70.317 1299 .240 1509 GAM 2.61 2315 KELI 16 7 -8.217 114.491 591 -.779 17 7 47.477 11.064 725 .585 2321 KEV 437 18 67.755 27.007 79 -.062 -.067 .334 178.0 .362 106.5 .54 .41 43.4 .04 1518 GBA 868 17 13.601 77.436 25 -.577 -.338 .231 195.9 .268 141.1 .52 .45 25.8 -.59 . 89 2331 KGM 284 9 2.015 103.317 103 .476 1514 GDH 321 16 69.250 -53.533 23 .100 .688 1.282 157.7 . 515 168.9 2.17 1.93 21.3 -.46 2337 KHC 569 16 49.131 13.579 699 .259 .077 .419 5.3 .018 150.8 .37 .23 61.5 .15 1551 GEC2 370 16 48.951 13.715 1136 -.415 -.490 .120 334.5 .215 35.0 .39 .35 22.2 .53 2351 KIC 448 17 6.360 -4.741 174 -.469 -.354 .095 118.9 .138 95.8 .39 .37 10.3 .23 31 11 -28.752 24.780 1320 -.216 -.317 .635 61.0 .723 75.3 .91 .56 62.9 -.09 1557 GERE 154 16 48.951 13.715 1136 -.203 -.393 .326 323.5 .489 64.0 .54 .33 63.5 .22 2356 KIM 66 11 21.423-158.014 72 .634 .340 1.509 355.8 1.062 56.4 .71 .23 89.5 .25 1596 GKX 248 18 28.030 84.670 1478 -.219 -.072 .198 86.9 .468 174.9 .49 .32 57.2 -.11 2358 KIP . 81 82 7 47.017 28.867 0 -.376 1601 GLD 495 14 39, 750-105, 221 1761 .718 .691 .211 296.5 .110 108.2 .25 .20 37.2 .37 2360 KIS 2362 KIV 109 11 43.950 42.683 1200 .443 1.426 1.118 202.8 .909 166.5 1.98 1.56 37.3 .14 . 86 20 6 38.167 15.863 1350 -.169 1613 GMB 99 15 64.199 27.715 159 -.496 -.376 .438 289.1 .217 74.6 .42 .19 80.0 .31 1636 GOGA 48 10 33.512 -83.616 150 -.236 -.427 .235 104.6 .234 165.6 .54 .49 18.2 .07 2364 KJF 1638 GOL 593 16 39,700-105,371 2358 .214 .190 .360 273.4 .044 2.2 .43 .35 34.2 .12 2371 KKM 364 14 6.045 116.211 0 .801 .461 .835 1.6 .585 99.9 .81 .55 54.5 -.18 1649 GRB1 11 8 49.472 11.687 493 .785 1.31 2372 KKN 319 17 27.790 85.280 1919 -.126 -.004 .258 59.3 .456 174.3 .53 .39 44.8 -.17 1653 GRF 658 17 49.692 11.222 499 .618 .405 .425 22.2 .111 84.9 .41 .27 55.4 .26 .669 227.9 .379 34.6 .42 .18 82.6 .02 2380 KLB 232 11 -31.673 117.850 300 -.880 -.499 . 85 60 9 38.821 16.451 479 .386 1656 GRI . 96 23 8 3,100 101.650 0 .479 2389 KLM 1658 GRM 97 13 -33.312 26.508 601 1.396 2.457 2.548 133.3 1.297 150.5 1.83 .88 77.0 -.11 508 16 25.123 102.740 1945 .435 .366 .800 178.7 .288 145.5 .73 .33 78.9 -.02 2407 KMI 1.81 2.20 KWY 29 8 59.320 5.370 57 1.643 1.06 61 8 43, 317 45, 700 123 . 985 1660 GRO 11 6 -13.505 25.837 1223 .860 . 62 2421 KMZ 1663 GRR 636 17 48.388 -.851 0 -.234 -.330 .362 312.5 .073 23.7 .37 .26 52.5 .25 2423 KNA 121 12 -15.750 128.767 54 -.841 -1.264 .727 23.6 .154 35.7 .64 .42 57.7 .43 20 6 39.500 46.333 0 .275 -80 1664 GRS . 94 39 7 10.233 77.467 2315 .272 1679 GTA 822 17 39.100 99.800 1340 .092 .035 .295 246.1 .248 103.4 .46 .37 34.8 .05 2436 KOD 94 9 41,493 35,911 144 .045 1685 GLA 111 16 13.538 144.912 230 -.879 -.981 .451 106.9 .658 115.9 1.02 .89 23.2 .20 2442 KOL 1689 GLM 221 15 20.680-103.324 1567 -1.245 -1.187 .515 214.6 .503 139.5 .86 .69 36.6 .16 19 9 59.649 9.632 216 -.861 1690 GUN 231 17 28.006 85.994 2900 .055 .139 .244 87.9 . 157 171.5 .50 .36 48.0 -.60 2444 KON 2462 KRA 543 17 50.052 19.937 223 .103 .172 .289 190.3 .298 40.5 .56 .48 26.7 .59 . 462 151.4 . 63 . 51 35.4 -. 46 1709 GYA 610 18 26.459 106.664 1161 .180 .091 2488 KSH 434 18 39.455 75.980 1286 1.316 1.006 . 137 123.7 . 358 103.3 . 58 . 51 22.8 -. 12 .438 68.4 .58 .48 32.4 .15 1713 GZH 195 14 23.087 113.344 10 .786 .609 .341 113.9 10 7 -3.638 102.673 0 .043 1.93 1733 HAU 789 18 48.005 6.350 569 -.388 -.380 .016 356.2 .220 164.4 .27 .22 35.3 .32 2489 KSI 566 15 50.843 16.293 379 -.099 -.224 .194 61.0 .129 106.3 .25 .20 36.3 .07 2493 KSP 2494 KSR 199 16 -25.850 26.897 1623 -.310 -.407 .496 133.3 .248 7.2 .65 .53 32.8 -.55 1766 HFS 850 17 60.134 13.696 223 -.650 -.671 .074 309.4 .308 91.6 .29 .19 58.2 .08 . 94 2512 KTK1 35 9 69.117 23.271 340 -.203 64 10 7 51.638 -2.806 209 .243 1768 HGH 2.65 11 6 -10.163 123.653 52 2.735 88 13 50.890 6.067 135 .174 .547 .975 109.8 1.541 138.4 1.64 1.21 45.6 .12 2519 KUG 1769 HGN 33 10 -10.168 123.586 52 .768 -3.729 4.204 50.0 5.598 132.3 3.56 2.20 62.0 -.38 531 17 40.849 111.564 1169 .366 .680 .622 324.6 .450 179.3 1.40 1.30 14.6 .18 2525 KUP 1771 HHC 64 11 45.233 147.867 0 .474 .293 .712 129.1 .186 88.6 .84 .71 28.7 .41 2526 KUR . 66 12 3 29.950 -95.833 -122 1799 HKT 1836 HOF 288 13 50.314 11.877 565 .263 -.010 .327 41.2 .449 78.5 .45 .27 64.0 .53 . 81 12 6 41.314-105.583 0 -.811 1852 HPK 162 15 54.004 -1.690 226 .561 1.269 .963 173.5 2557 LAR . 584 142.1 1.97 1.79 17.6 -.13 2569 LBF 698 17 46.985 3.977 714 -.498 -.403 .183 169.1 .195 163.6 .32 .27 29.8 .59 1867 HRV 118 14 42.506 -71.552 180 -.012 -.421 .498 97.4 .819 177.8 1.12 .84 43.0 .03 313 .633 104.1 .155 22.1 .56 .31 68.8 .10 2573 LBNH 144 15 44.301 -72.009 367 .080 1900 HVD 33 10 -30.604 25.496 1378 -.554 .392 .489 273.6 .942 148.2 1.86 1.72 15.3 .21 2578 LBTB 74 13 -25.145 25.720 1027 -.144 .217 1.469 131.9 .657 149.9 1.10 .72 57.4 .10 1910 HYA 45 7 61.310 6.220 29 .427 . 92 2604 LDF 661 17 48.594 -.122 289 -.369 -.301 .209 237.6 .072 173.8 .21 .14 57.5 .11 1.73 49 9 -6.833 107.617 1241 .427 1911 HYB 235 11 17.417 78.553 509 -.466 .609 2.148 204.1 1.581 33.6 2.07 1.11 71.2 .11 2619 LEM .120 17.8 .26 .19 43.8 -.31 2633 LFF 603 17 44.937 .736 193 .223 . 237 . 205 120.5 32 11 47.285 2.694 428 -.019 -.120 .332 91.8 .041 86.6 .53 .45 27.4 -.05 2.18 43 9 48 417 -89 267 195 - 325 1955 ILT 184 13 67,833-178,800 0 -.627 -.499 .351 100.3 .054 70.1 .57 .51 21.6 .14 2648 LHC 260 LIC 307 17 6.225 -5.028 100 -.429 -.348 .269 149.3 .289 108.0 .39 .26 54.4 .55 1958 IMA 1013 17 66.085-153.786 0 .073 -.023 .457 3.5 .392 39.2 .52 .29 69.1 .28 . 64 66 9 46.043 14.533 395 -.036 1.82 1973 ING1 21 8 -8,818 115,145 202 -.520 1975 INK 721 17 68.237-133.520 39 -.168 -.493 .379 293.9 .136 156.1 .47 .37 40.4 -.31 2678 LK0 155 16 9.644 -5.639 435 -.616 -.558 .110 92.0 .153 114.2 .43 .41 9.5 -.24 1984 IPM 837 16 4.581 101.027 246 .234 .329 .263 286.6 .600 28.4 .74 .58 38.4 .14 54 10 45.870 -64.860 363 .304 .898 1.752 100.2 .714 70.5 1.48 .98 56.3 .03 1993 IRK 188 14 52.267 104.317 467 -.341 -.170 .968 232.9 .132 49.5 1.00 .64 59.2 .60 2699 LMN 23 6 47.548 -70.327 418 -.076 2701 LMQ 1996 184 249 16 35.643-118.477 759 .270 .534 .456 109.6 .127 33.2 .70 .61 24.4 .18 482 18 43.333 6.509 200 -.130 -.179 .130 179.1 .202 173.2 .37 .32 22.6 -.43 2045 JAY 64 12 -2.500 140.667 400 -.519 -1.878 2.069 25.8 2.627 140.3 2.32 1.13 76.3 -.05 2702 LMR 29 7 68.260 13.620 79 -.181 1.13 2723 LOF 2730 LOR 881 17 47.267 3.850 529 -.458 -.443 .103 282.1 .185 160.6 .26 .21 34.4 .56 2059 JCT 87 12 30,479 -99,802 591 -,433 -,173 .090 69,4 .668 23,3 .66 .48 45,9 .21 1.05 49 6 -34,909 -57,932 14 .573 2080 JFWS 96 10 43.042 -90.381 335 -.962 -.917 .285 81.8 .279 27.9 .29 .07 93.7 .21 2734 LPA . 320 . 688 53.8 . 687 129.9 . 94 . 69 45.5 . 46 74 13 -16,677 -68,234 3292 .630 2735 LPB 2112 JIRN 45 9 27.660 86.190 3063 .227 2738 LPF 668 17 48.165 -1.108 156 -.117 -.152 .115 267.7 .270 9.4 .27 .17 61.5 -.19 2188 J0Z 16 10 -27.445 32.078 244 .456 1.324 2.232 169.9 2.347 179.7 2.17 1.12 73.0 .09 .161 .478 292.1 .364 22.3 .48 .20 82.9 .13 2739 LPG 696 18 45.627 6.765 2569 .207 2196 JRS 67 9 49,192 -2.099 52 .147

. 96 3173 MINU 33 7 35.139 -84.229 550 -.462 3180 MZF 17 9 46.215 2.584 479 .096 3173 MYNC 33 7 35,139 -84,229 550 -.462 . 54 2741 [P] 101 17 15.665 6.874 2069 .143 .072 .397 299.5 .314 14.2 .44 .23 72.5 -.30 3199 NAT 116 15 -1,339 36.837 1692 2.042 2.831 1.120 243.4 .832 24.8 1.34 .90 54.8 .00 2743 LPO 618 17 44.683 1.187 330 .150 .113 .233 110.0 .066 28.9 .27 .20 44.0 .11 3203 NAX 88 11 32.063 118.783 7 -.111 -.236 .180 283.3 .687 61.1 .59 .33 68.2 -.01 .013 .065 .162 191.8 .165 5.5 .26 .20 42.3 .02 2754 LRG 563 18 43,454 6,360 100 . 04 NAO 163 16 60.887 10.974 379 -.860 -.218 1.377 282.4 .939 125.7 2.31 1.93 30.6 .57 2765 LSA 380 16 29,700 91,150 3657 1.025 1.008 .324 28.2 .268 172.4 .48 .39 33.5 -.39 3212 NB2 868 17 61.097 11.347 717 -.798 -.634 .508 259.5 .070 78.4 .47 .28 65.7 -.63 2766 LSCT 84 12 41, 784 -73, 294 317 .041 -, 606 .967 117, 2 1, 646 15, 7 2, 25 1, 68 43, 8 .52 2768 LSF 518 17 46,250 1.530 430 -.177 -.184 .152 158.6 .059 160.2 .34 .32 10.5 .03 3237 XDI 339 13 28.683 77.217 230 -.724 .233 .941 253.8 .393 13.7 .83 .49 65.3 -.24 2.20 2777 LSZ 33 8 -15, 366 28, 232 1184 . 799 3247 NEW 557 16 48.263-117.120 759 -.236 -.232 , 305 306, 3 . 271 8.2 . 43 . 29 54.3 - 10 2798 LTX 143 13 29.334-103.667 1013 -.588 -.651 .558 157.3 .233 103.5 .69 .50 46.0 .01 . 256 42.9 . 354 117.3 . 41 . 30 48.6 . 20 3268 NIE 430 16 49,424 20,322 555 .704 .572 2825 LZH 630 L8 36.050 L03.833 L518 .304 .476 .535 332.3 .449 L63.5 L23 L13 L7.0 -.17 3276 XJ2 423 12 32.052 118.854 45 .358 .272 . 390 193. 5 182 103.8 .34 .20 64.0 -.58 2832 MAF 567 17 16.265 2.714 469 .054 .097 .251 139.1 .309 3.9 .31 .14 77.9 .38 3305 NNA 101 14 -12.023 -76.922 574 .182 .125 .412 260.2 .585 144.6 1.32 1.19 18.2 -.35 3314 NOR 109 15 81,600 -16,683 35 -.197 -.083 .859 248.3 .291 55.5 .85 .55 58.2 .17 2835 MAI = 267 15 35, 472 135, 387 30 , 405 , 360 , 428 12, 2 , 162 153, 6 , 48 , 33 50, 8 , 053319 NPA 36 8 -15.087 39.253 374 .984 2.882836 MAJO 154 12 36.542 138.209 421 -1.131 -.876 .455 56.6 .504 83.3 .43 .14 89.3 .24 3325 NPO 132 12 64.814-146.915 418 -.582 -.209 1.064 30.7 .360 64.5 .85 .57 55.0 .61 1.44 2837 MAK 12 6 43.017 47.433 0 .678 3331 NRI 54 10 69.400 88.100 39 -1.594 -.338 1.626 308.9 .496 13.5 1.14 .41 87.1 .66 2.37 2840 MAN 29 5 14.667 121.083 70 .123 2815 WAT 786 15 36 538 138 208 139 -1.075 -.607 .875 45.2 .425 78.3 .79 .42 72.2 .47 3340 XSS 42 10 64.650 11.970 101 -.229 .034 .452 283.4 .556 113.4 .62 .24 85.0 -.16 2818 MAW 166 16 -67,604 62,870 12 .613 .645 .899 324.8 .604 106.0 .94 .58 62.0 .44 3350 NUR 673 17 60,509 24.651 101 -.355 -.182 .181 193.5 .255 114.3 .31 .21 56.5 -.21 2852 MBC 997 17 76.242-119.358 14 .001 -.066 .411 35.6 .235 89.3 .54 .42 39.8 -.34 3360 NVL 37 7 -70.767 11.833 86 .094 1.24 2857 MBL 202 11 -21,160 119,833 200 -.801 -.697 .885 297.6 .460 81.4 .88 .47 71.4 -.42 1.05 3363 NWA 354 14 -33.020 117.240 264 -.508 -.532 .427 306.7 .152 81.0 .47 .36 43.1 -.07 2878 MCQ 16 6 54, 199 158, 956 14 1, 413 3365 NWL 18 8 -27.757 29.981 1332 .827 2.16 2881 MCW 113 13 48,797-122,973 693 -.044 .080 .741 108.3 .492 176.7 .86 .53 61.8 -.08 3387 OBN 355 17 55.167 36.600 0 -.461 -.248 .254 190.4 .559 123.8 .61 .40 56.9 .26 1.95 2897 MDJ = 527 + 4 + 44, 616 + 129, 592 + 250 = 0.080 + -129 = 569 + 235, 6 = -415 + 125, 4 = -67 + -38 + 66, 5 = -0.0822 6 35.590 -97.540 351 .253 3397 OCO 3400 ODAN 75 9 26,860 87,390 2045 .129 . 61 2911 MEEK 50 8 -26,678 118,745 529 -.650 . 74 3402 ODD 18 8 59.950 6.670 629 .799 . 68 2914 MEK 30 10 -26.613 118.545 514 -.507 -1.407 2.025 55.5 1.654 12.71.96 1.37 51.1 -.10 3410 06A 285 16 46.868 11.025 934 .255 .425 .106 132.2 .685 157.2 .55 .18 89.0 -.02 2916 MEM 105 10 50.692 6.066 0 .178 .355 .143 108.4 .406 125.0 .31 .13 81.3 -.16 3418 OHR 315 15 41.214 20.939 739 -.679 -.383 .371 174.2 .629 164.0 .67 .37 69.9 -.28 2918 MEO 39 11 34,785 -98,596 465 -,562 -,682 ,562 10.2 ,203 26.3 ,81 ,70 26.6 ,02 2923 MEE 10 4 37,101 14,930 985 .815 . 81 235 15 50.245 19.934 391 .144 -.029 .436 4.4 .325 106.2 .54 .35 57.3 .172928 MFF 639 17 46.601 -.143 259 -.059 -.073 .085 252.4 .214 177.7 .24 .18 46.0 -.04 1.02 . 97 3470 ORO 16 7 45.625 7.980 1161 -.199 2938 MGD 61 9 60 100 150 700 219 - 133 . 49 3472 ORV 146 12 39.555-121.500 360 .124 .243 .220 175.8 .052 101.8 .48 .46 8.6 .15 2947 MGR 16 6 40.176 15.598 259 -.141 3491 OTT 141 14 45.394 -75.716 82 -.319 -.179 .870 82.5 .612 176.8 .92 .62 54.8 .33 2953 MHC 162 13 37.342-121.642 1281 .566 .280 .476 30.9 .643 85.0 .93 .71 41.0 -.18 . 60 76 8 34.512 -89.409 101 -.766 3506 OXF 36 11 39.546 -4.348 0 .120 -.122 .408 315.5 .345 50.7 .27 .19 49.8 -.03 . 92 3514 PAB 2955 WHI 10 4 36.300 59.595 1100 .403 3517 PAE 509 17 -17.662-149.580 59 1.317 1.534 .453 103.2 .205 163.7 .78 .69 22.6 .57 2961 MIAR 209 14 34.657 -93.630 207 -.500 -.527 .139 106.1 .068 17.0 .43 .42 5.3 .28 14 6 34,148-118,172 294 .009 1.46 2963 MID 37 11 59.427-146.338 0 .858 1.082 1.110 23.4 .465 55.0 .76 .52 54.2 .32 3530 PAS 3555 PCI 133 11 -. 933 119.883 0 1.050 .340 1.313 38.5 1.519 138.3 .90 .56 60.9 -.29 2969 MIN 92 11 40.345-121.605 1495 -.222 -.192 .205 204.8 .590 173.4 .43 .21 76.4 .19 17 5 36,691 -96,978 331 -.176 . 62 2978 MJAR 177 13 36.542 138.209 421 -.737 -.468 .350 31.1 .278 90.4 .39 .24 61.8 -.26 3560 PCO 1.64 2990 MKS 14 8 -5.067 119.633 28 .360 3563 PCT 70 9 14,715 101,427 0 .815 1.98 3013 WME 10 4 44.194 10.700 2160 .714 . 20 3566 PDA 130 15 37.743 -25.662 35 -.077 -.332 .469 210.1 .231 121.2 .54 .37 54.4 .70 3033 MNI 24 6 1.450 124.800 128 -.088 . 95 3576 PDY 138 12 59.633 112.703 0 -.150 -.488 .620 245.7 .147 173.5 .79 .63 37.2 .14 3034 WNK 66 9 53,900 27,567 0 .154 . 80 3577 PEC 341 13 33.970-117.257 615 .105 .376 .389 79.5 .426 10.0 .51 .34 55.3 .53 1.83 3038 MNO 13 5 37,931 14,695 1840 .290 31 11 -33.144 -70.685 689 .237 .228 .482 155.9 .133 72.9 .75 .65 25.8 -.26 3582 PEL 3584 PEN 11 5 30.467 -87.183 0 -.824 i.15 3042 MNS 15 8 42.396 12.800 600 -.223 . 46 3588 PET 207 13 53.017 158.650 0 .125 -.260 .394 146.4 .547 35.0 .69 .40 66.9 -.04 3043 MNT 87 13 45.502 -73.623 112 -.686 -.198 .879 96.0 .181 173.4 .98 .81 32.9 .34 86 12 33.609-116.455 1279 .164 .433 .583 73.8 .207 60.6 .56 .34 62.6 .81 65 11 38.572-118.194 1506 .159 -.287 .937 298.6 2.275 6.4 2.01 1.38 53.1 .07 3594 PF() 3045 MNV 214 13 48,650-123,451 4 .477 .005 1.630 268.8 1.807 173.2 2.22 1.56 50.8 .60 34 8 62,600 7,680 97 ,051 . 85 3598 PGC 3058 MOL 3061 MOR 13 6 42.103 140.572 18 -1.482 3599 PGD 10 5 43.875 11.721 1600 .909 . 78 1.12 3065 MOS 24 8 55,733 37,633 120 -.005 193 17 42.548 9.144 1129 -.412 -.425 .095 137.5 .154 171.9 .34 .31 15.8 .06 3066 MOT 102 13 30.797-104.082 2019 - 254 - 621 .560 26.5 .427 149.1 .84 .65 39.1 .60 3601 PGF 3604 PGP 35 5 13,480 120,960 0 -.683 1.91 3070 MOX 240 17 50.646 11.616 453 .268 .202 .239 355.5 .292 72.6 .47 .39 31.3 -37 . 92 3611 PHC 52 9 50.700-127.433 32 .560 3071 MOY 42 9 51.683 100.983 0 .655 14 7 43.762 10.588 50 -.432 . 64 3101 MRW 226 15 -41.232 174.705 0 -.684 -.537 510 303.0 .107 129.3 .60 .45 44.6 -.20 3431 PII 20 5 18.325 120.619 150 -.462 1.22 3636 PIP 3651 PKI 348 18 27.610 85.490 2757 -.269 -.166 .137 23.6 .409 2.5 .51 .40 37.5 -.43 3128 MTA 71 8 41.700 44.800 0 .273 94 12 37.763-122.012 462 .063 -.116 .737 283.1 .670 68.2 1.06 .68 58.9 -.54 3138 MTN 113 11 -12.847 131.130 79 -.862 -1.734 1.273 60.7 ...649 155.6 ...84 ...62 45.1 -..45 3660 PLC 19 5 11,165 124,979 133 -.228 1.45 3150 MUD 312 14 56.460 9.170 12 .847 .892 .131 294.3 .405 111.4 .55 .46 28.8 -.12 3669 PLP 3678 PME 110 11 61.733-149.167 231 -.622 -.721 .623 353.4 .275 49.7 .72 .59 33.0 .04 3153 MUN - 340 12 -31.978 116.208 -234 -.467 -.515 .179 130.2 .403 .1 .33 .20 61.3 .08

3679 PMG 245 12 -9.409 147.154 67 -.354 -.639 .186 49.4 .569 155.7 .82 .70 26.4 -.46 3685 PM0 762 17 -15.004-147.897 2 1.260 1.103 .405 9.7 .372 88.0 .55 .41 43.9 .39 3687 PMR 1318 18 61.592-149.131 0 -.459 -.167 .340 59.5 .296 10.8 .55 .44 35.9 .35 4150 SEI 51 10 61, 245-149, 561 716 -. 324 -. 250 ,753 16.8 .671 49.8 .65 .46 49.1 .58 3688 PMS 4170 SGO 3705 PNT 689 14 49.317-119.617 550 .210 .319 .024 287.7 .144 52.2 .28 .25 16.2 -.22 86 14 -29, 382 19, 950 0 1, 385 1, 120 1, 235 61, 8 , 993 87, 8 1, 26 , 55 80, 8 , 58 4181 SHE 3711 POF 3716 P00 244 14 18,533 73,850 555 -.283 .229 .630 294.2 .763 115.8 .98 .74 42.8 -.69 3727 PP1 122 10 -. 452 100. 384 0 -. 559 -. 007 .917 254.7 .471 24.1 .78 .38 75.9 -. 38 4187 SHK 3731 PPN 496 17 -17.531 149.432 0 1.301 1.428 .250 104.6 .249 176.4 .65 .60 15.7 .11 4188 SHL 66 9 9.750 118.733 14 1.248 1.58 3733 PPR 3735 PPT 513 17 -17.569-149.576 259 1.265 1.389 .250 91.5 .106 148.6 .62 .58 10.8 .07 3741 PRA 155 12 50.070 14.430 202 .550 .516 .143 258.6 .495 65.6 .40 .17 80.8 .22 4239 SKR 3757 PRU 130 15 19.988 14.542 301 .289 -.078 .523 5.3 .424 81.9 .52 .21 84.0 .09 4251 SLL 3760 PRY 126 13 -26.928 27.473 0 -.129 -.218 .789 15.7 .491 107.0 .85 .59 51.8 -.35 3761 PRZ 34 9 42,483 78,400 0 .950 3770 PS1 264 14 2.691 98.919 0 -.463 .405 1.640 226.2 1.123 45.1 1.60 .98 62.3 .22 23 9 -14.390 31.390 1026 .302 2.14 73 10 59,767 30,317 64 .098 1.822 3.400 197.5 1.769 24.2 1.34 .37 92.3 .58 3804 PUL 3825 PWA 49 12 61.651-149.879 136 -.186 .249 1.132 59.5 .769 42.4 1.26 .92 46.8 -.32 . 89 4284 SNF 3832 PYA 126 9 44.033 43.050 497 -.156 3838 PYLN 100 14 28.100 82.990 1866 -.085 -.050 .208 145.5 .140 17.6 .49 .45 13.7 -.32 1.09 4298 SNZ 3840 PZI 41 9 37.105 15.067 0 .451 4307 SOI 3851 917 163 11 19.029 109.843 230 .514 .717 .141 134.4 .666 39.2 .57 .33 67.7 .23 . 66 3857 QLP 62 8 -26,587 144,248 209 -.021 3870 QEE 114 11 30.188 66.950 1713 -.123 -.599 .940 303.6 2.069 84.4 2.06 1.50 46.5 -.31 3879 QZH 170 11 25.031 118.667 20 -.034 -.025 .228 186.9 .788 71.4 .51 .21 82.6 .24 11 11 -4.193 152.171 182 -.188 .556 .802 273.9 1.076 29.4 1.16 .77 56.1 .04 3882 RAB 94 11 50.083 18.183 209 .914 .789 .481 325.3 .318 82.0 .45 .18 83.9 .33 3883 RAC 70 10 37,766 41,292 850 .214 .128 .215 100.6 .147 129.8 .26 .20 43.0 .08 3SSS RAM 4352 SRO 1.41 3889 RAN 23 7 16.867 96.183 14 -.480 41 9 -21.212-159.773 28 .439 1.68 4365 SSF 3891 RAR 4374 SSP 1.63 24 7 51.941 178.451 225 -.717 3892 RAT 4381 STA . 53 3917 RDP 10 6 41.758 12.717 759 .200 3930 RES 138 15 74.687 -94.900 14 .045 .175 .742 63.0 .177 126.1 .68 .42 61.4 -.01 4382 STB 4389 STJ 3937 RF1 38 10 41,305 13,998 0 .635 .916 .887 218.5 1.207 56.0 1.03 .53 73.0 -.01 3961 RIF 624 17 45.305 1.516 409 .033 -.032 .372 98.6 .089 84.2 .33 .16 75.7 .04 3963 RKG 173 10 -34.098 117.104 300 .170 .072 .231 91.1 .366 179.4 .32 .17 71.6 .39 4390 STK 3965 RKT 283 16 23.118-134.972 100 .726 1.555 .615 279.8 .812 16.8 1.37 1.14 30.8 -.52 4397 STU 4404 SUE 3974 RMP 13 6 41.911 12.723 379 1.178 1.88 3975 RMQ 172 13 -26.540 148.800 360 .451 .432 .446 71.8 .449 86.5 1.04 .91 22.9 .55 4412 SER 1013 RSCP 90 14 35.600 -85.589 580 -.833 -.606 .313 107.3 .676 99.7 .74 .47 60.2 -.09 4423 SVE 4017 RSNT 393 17 62.480-114.592 50 -.235 -.030 .300 71.1 .157 24.3 .43 .36 31.3 -.24 4436 SVW 4018 RS0 289 15 60.572-152.788 1921 -.790 -.616 .481 303.0 .175 69.7 .57 .44 38.3 .34 4449 SWZ 1020 RSSD 381 11 11.151-104.062 2059 -.165 -.370 .273 48.6 .379 175.1 .44 .33 44.9 .22 4479 TAP 4482 TAT 1041 RUV 791 17 -15, 189-147, 384 3 1, 077 1, 026 , 476 30, 4 . 212 92.8 .57 .45 37.6 .02 6.6 4063 SAD 17 6 33,822 73,183 837 -1.136 92 1070 SAL 13 6 15.675 10.612 70 .605 4490 TB1 4073 SA0 187 13 36.765-121.445 230 .496 .667 .058 151.4 .632 17.7 .53 .27 73.1 -.10 1.06 4082 SBA 65 9 -77.850 166.756 37 1.293 4086 SBF 371 18 43.981 7.452 847 -.289 -.213 .247 205.5 .114 17.5 .30 .23 42.8 .08 4556 TIC 4102 SCH 415 17 54,817 -66,783 540 -.226 -.353 .280 89.8 .427 170.6 .55 .42 43.0 -.34 4562 TIK 4107 800 332 17 70.483 -21.950 68 .649 .884 .642 108.2 .236 117.0 .64 .41 58.6 .11 4124 SDI 11 6 41.758 13.954 0 .031 . 67 4578 TKL

4126 SDN 340 15 55.413-160.622 23 -.703 -.553 .452 80.9 .196 59.3 .56 .43 41.0 .48 4129 SDV 23 9 8,886 -70,633 1580 -.300 . 94 4136 SEK 186 16 -28.323 27.625 1485 .282 .535 .250 112.6 .677 157.5 .68 .45 56.3 -.15 4141 SES 408 16 50.396-111.042 769 -.273 -.153 .183 87.8 .146 86.8 .51 .47 12.1 .76 . 47 10 7 43.960 11.870 0 .931 1.21 10 6 40.633 15.384 0 -.214 . 62 46 7 40,633 48,633 0 ,833 .047 .807 26.5 .285 165.2 .65 .33 74.9 .57 96 10 34.530 132.678 284 -.042 58 7 25.567 91.883 1600 -.346 .538 .594 4.5 .204 56.5 .56 .39 51.7 .20 4214 SIT 288 14 57.057-135.324 18 .789 41 8 18.112 -66.150 456 -1.535 .088 .103 136.4 .362 179.8 .45 .36 37.4 .26 4238 SK0 379 17 42,021 21,496 345 .103 24 9 50.667 156.100 0 -.414 1.61 . 83 11 5 60.477 13.323 419 -.534 4256 SLR 366 17 -25.753 28.420 1348 -.475 -.876 .862 38.4 .453 .71.291.0632.0 -.34 4265 SMF 593 17 46.645 3.841 458 -.332 -.298 .193 192.3 .245 12.2 .25 .13 72.1 -.29 4274 SMT 39 8 38.467 70.067 0 .733 1.44 4278 SMY 282 12 52.722 174.120 46 .118 -.205 .659 250.7 .221 173.3 .93 .77 31.4 .59 4280 SNA 138 13 -70, 309 -2, 358 52 , 385 , 217 , 629 115, 3 , 457 125, 4 , 92 , 77 30, 3 -, 02 . 60 73 9 50.586 4.433 108 .256 4285 SNG 379 15 7.173 100.620 4 .577 .678 .259 11.3 .577 9.8 .79 .62 38.4 -.27 4297 SNY 512 14 41.828 123.578 54 -.486 -.424 .514 76.6 .464 100.0 .58 .36 61.7 .41 25 6 34.380 134.908 370 -.287 1.32 1.31 4301 SOC 41 7 43,583 39,717 192 -.279 11 6 38.121 16.099 0 -.323 . 69 4317 SPA 1190 17 -90.104 115.000 2927 .357 .429 .439 158.9 .472 86.0 .68 .51 44.7 .18 . 274 . 252 209.3 . 399 73.7 . 68 . 58 26.1 . 68 4319 SPC 57 10 49.188 20.245 1771 .308 4323 SPI 107 15 57.160-170.225 0 -.204 .065 .509 193.6 .321 88.9 .60 .39 56.5 .16 4339 SQTA 334 16 47.255 11.287 1307 -.168 -.546 1.042 359.5 .533 133.6 .95 .48 74.6 .07 1.39 4344 SRD 33 9 6.932 -72.853 1639 -1.304 69 9 47.813 18.313 0 .777 . 81 4364 SSE 833 15 31.096 121.187 9 -.028 .121 .365 210.5 .460 65.6 .49 .23 78.0 .25 669 17 47.061 3.507 360 -.309 -.306 .048 298.0 .178 178.6 .28 .25 22.3 .45 60 8 36,925-116,219 2065 -,670 1.15 23 7 17,695 74,000 665 .292 1.50 . 54 11 5 50,703 6,900 270 .283 48 10 47.572 -52.733 61 -.449 -.503 1.040 357.9 1.012 28.5 1.40 1.02 46.7 -.39 $599\ 17\ -31,\ 882\ 141,\ 592\ 212\ -,\ 064\ -,\ 239\ ,\ 387\ 89,\ 6\ ,\ 152\ 98,\ 3\ ,\ 72\ ,\ 65\ 17,\ 6\ ,\ 76$ 102 12 48.771 9.193 375 -.154 -.317 .251 17.8 .153 96.3 .39 .34 21.8 -.38 18 6 61,120 4,860 9 .656 . 60 4405 SUF 183 15 62.719 26.150 185 .020 .010 .556 341.7 .150 166.7 .59 .40 54.5 -.20 80 14 -32.380 20.728 0 1.669 1.912 .420 243.3 .555 121.0 1.66 1.56 11.4 .01 70 10 56.800 60.633 275 -.064 .150 1.227 181.0 .312 .5 .93 .47 73.9 .58 586 17 61, 182-155, 633 762 . 273 -. 013 . 983 326.5 . 372 44.6 . 94 . 57 62.8 . 21 48 12 -27.182 25.325 1342 -.391 .102 1.093 301.0 2.346 108.2 2.31 1.63 50.4 -.23 . 58 74 9 25.033 121.517 8 .302 96 13 34.983 139.867 0 -.212 .522 .983 315.7 1.517 77.4 1.29 .43 88.8 .69 221 16 -23, 349-149, 461 9 1, 635 1, 627 , 423 159, 1 , 774 129, 3 1, 17 , 98 29, 1 -, 11 . 396 153.6 . 246 2.8 . 36 . 18 75.1 . 20 4503 TCF 622 17 46.288 2.210 592 -.081 -.008 1.63 4549 THRI 19 6 -8.370 115.543 1000 -.245 4555 TIA 256 13 36.211 117.124 300 -.184 -.296 .349 193.6 .764 92.4 .59 .30 73.2 .72 277 17 6.550 -5.000 137 -.441 -.239 .388 170.2 .356 125.3 .50 .35 52.1 .66 56 11 71.633 128.867 0 -.935 -1.060 .912 185.9 1.162 84.1 .77 .44 67.2 .35 4569 TIY 454 15 37.713 112.434 850 .138 .268 .558 14.4 .057 123.3 .61 .45 44.4 -.65 17 2 35.730 -83.840 349 -1.087

4588 TLG 20 9 43.267 77.383 850 .370 . 78 1621 TNP 585 16 38,220-117,227 1932 .304 .139 .457 212.0 .549 138.1 .99 .83 30.7 -.06 1626 TOA 341 15 62.147-146.223 908 .608 .588 .385 17.0 .237 104.0 .40 .26 56.9 .51 498 488 169 127.3 110 111.8 30 26 25.9 34 1632 TOL 82 15 39,881 -4.049 479 .699 .941 .440 261.3 .460 85.8 .57 .38 55.3 .19 1635 TOO 323 13 -37.571 145.490 603 1610 TOV 16 5 9.820 -69.876 649 . 339 1651 TPN 168 15 -8.419 146.987 989 .717 .732 .633 174.0 .353 163.4 .70 .44 59.5 .27 4655 TPT 771 17 -14.984-147.620 3 1.217 1.064 .301 13.1 .238 91.5 .45 .37 31.6 .23 4674 TRN 18 9 10.650 -61.400 24 -.394 1.56 . 94 4675 TRO 17 8 69.632 18.928 14 -.537 1680 TRT 218 13 -7.650 112.500 0 -.660 .211 1.663 177.7 1.989 9.3 1.32 .50 85.3 -.19 4689 TS1 10 4 3,508 98,695 0 .632 1.77 . 86 4692 TSM 90 9 4,223 118,072 0 .426 1700 TTA 690 16 62,930-156.022 913 -.003 -.187 .717 320.7 .483 15.8 .75 .36 77.5 .09 4716 TUH 30 10 -33,297 19.150 189 .237 -1.086 1.673 125.2 2.386 54.1 2.33 1.09 78.0 .17 1718 TUL 528 17 35.910 -95.793 256 -.455 -.338 .276 295.0 .216 103.9 .54 .47 24.0 .35 1730 TVO 543 17 -17.782-149.252 660 1.420 1.410 .070 128.2 .150 6.2 .65 .64 3.1 .28 1751 TXAR 133 12 29.338-103.670 1013 .192 .150 .570 228.4 .129 65.5 .61 .45 46.5 -.49 4772 UER 41 10 51,567 94,083 0 -,818 -1,329 ,672 149,2 ,800 89.6 ,64 ,46 48.0 -,67 4778 UKR 17 7 50.950 84.750 0 -.505 . 80 1782 1LM 112 13 50.397 -95.950 280 -1.012 -1.173 .372 316.2 .307 45.3 .60 .50 30.8 -.32 1793 UPA 75 8 9.115 -79.540 41 .179 1.24 1795 UPP 126 13 59,858 17,627 14 -.651 -.434 .422 195.1 .069 25.7 .37 .27 46.0 .20 1819 UZH 121 14 48,633 22,300 0 .363 .482 .480 170.7 .241 56.6 .44 .23 74.0 -.31 4824 VAH 763 17 -15,237-147,636 3 1,000 1,013 .544 38.7 .319 65.9 .71 .55 40.2 .27 1833 VAY 284 13 41.361 22.601 167 .030 .202 .519 225.2 .432 35.9 .33 .20 62.1 -.43 90 11 45.545 15.316 259 .067 .137 .164 157.4 .108 83.2 .23 .16 52.1 .08 4838 VBY 4878 VIR 15 6 -28,080 26,863 1340 1.506 3.11 .964 16.9 .326 111.4 .82 .51 62.1 -.57 4882 VKA 55-13 48.265 16.318 400 .769 . 266 1.01 4884 VLA 32 9 43.117 131.900 74 .459 1903 VNDA 145 15 -77.640 161.956 97 .741 .144 .361 272.5 1.043 15.6 1.84 1.62 22.9 -.04 4909 VOY 36 8 46.467 13.985 1072 -.443 1918 VRAC 57 10 49.390 16.700 0 .505 .159 .463 328.2 .248 32.5 1.09 1.00 16.3 .49 4939 VVI 10 7 46,129 12,486 514 .188 1955 WAL 203 14 47.460-115.965 0 .122 -.178 .251 261.3 .262 109.2 .55 .49 21.2 -.25 1958 WAR 219 14 52.242 21.024 109 -.389 -.582 .287 243.8 .493 29.6 .62 .53 26.7 .37 1960 WAT 180 15 -30.317 115.883 0 -.058 -.162 .529 312.7 .162 3.6 .71 .56 38.4 .23 1962 WB2 169 13 -20 028 134,360 425 -1,414 -1,265 ,665 273.0 ,439 46.8 ,81 ,60 44.0 -.12 1985 WDC 257 13 40.580-122.540 300 .072 -.043 1.257 303.3 .991 6.4 1.19 .49 83.0 .21 1997 WET 323 15 49.145 12.880 612 .446 .211 .494 338.3 .248 54.8 .59 .42 50.7 .15 5017 WHY 575 15 30,544 114,350 26 .536 .420 .381 208.2 . 287 138.8 . 39 . 18 79.8 . 34 5021 WHY 210 15 60.747-135.007 1292 .065 -.317 .132 306.8 .616 73.4 .61 .39 59.1 -.52 5029 WIN 161 14 -22.567 17.100 1728 .385 .083 .547 73.5 .438 44.1 .94 .76 34.8 -.07 5047 WLF 90-13 49.796 6.174 0 .411 .326 .391 107.7 . 454 122.2 .58 .44 41.2 -.39 5059 WME 16 6 53,516 -4,334 129 -,466 1.13 5061 WMO 201 15 34.718 -98.589 504 -.528 -.534 .342 339.5 .502 21.2 .69 .51 46.8 .41 5062 WMQ 555 17 43.821 87.695 970 .334 .504 .349 242.3 .086 7.9 .45 .37 31.6 -.06 5082 WOOL 224 15 31.073 121.678 0 -.691 -.428 . 130 162.9 . 231 178.1 . 67 . 58 24.3 - 65 .172 40.3 .53 .47 20.6 -.33 5095 WR2 320 15 -20.068 134.472 414 -.874 -.781 . 278 265.3 5099 WRA 1110 17 -19.948 134.351 0 -1.122 -.800 .566 290.3 .752 47.8 .91 .57 60.3 .37 5117 WTS 806 18 51.995 6.810 43 .481 .690 .116 161.3 .247 122.0 .31 .24 40.7 .02 5118 WTTA 313 17 47.388 11.663 1764 -.079 -.394 .633 5.8 .544 146.5 .92 .69 43.5 .36 5127 WVOR 237 13 42,439-118,667 1343 .318 .302 .354 274.1 .342 165.7 .55 .41 45.0 -.22 5138 XAN 619 17 34.040 108.921 629 -.478 -.566 .089 329.0 .320 118.4 .33 .22 55.6 .27

5146 YAK 5151 YBH	209 14 159 11	62.017 129.717 41.868-122.805	0 968	649 . 327	907 009	.329 1.173	199.7 265.4	.120 .985	47.5 176.9	.51 1.01	. 43 . 30	27.7 91.2	. 14 . 47
5160 YKA 5162 YKC	$\begin{array}{rrr} 46 & 9 \\ 257 & 16 \end{array}$	62.579-114.646 62.478-114.473	0 - 197	-1.029	461	. 553	307.3	. 143	14.8	1.94	. 24	76.6	. 02
5168 YKU 5181 YOU	15 6 11 5	59.581-139.836 -34.278 148.382	19 503 200	2.089	317	360	11.1.3	565	51 5	1.06	67	37-1	21
5180 IKH 5189 YSNY	101 14	42.558 -78.575	628	276	142	. 797	130.4	. 563	126.3	. 72	. 35	76.7	. 40
5190 YSS	271 14	47.033 142.860	97	. 065	073 - 026	. 393	151.5	. 448	99.9 65.6	. 39 63	. 20	72.7 85.8	. 07
5219 ZOBO 5224 ZST	76 14 137 14	-16.294 -68.190 48.196 17.103	4396 250	~. 009 . 588	701 . 141	1.320	. 6	. 888	105.0 48.9	1.47	1.03	51.4 75.5	. 31 . 44

Appendix C

x *

The whole-mantle P-wave attenuation structure :QPB3DV2





	-180.00	-170.00	-160.00	-150.00	-140.00	-130.00	-120.00	-110.00	-100.00	-90.00	-80.00	-70.00	-60.00	-50.00	-40.00	-30.00	-20.00	-10.00
80 00	1 447	1 4 4 7	55 989	-20.651	1.447	2.436	-12.664	1.823	52.016	33.680	1.447	30.269	55.890	-34.098	1.447	64.013	-68.626	-54.510
00.00	0.000	0 000	3 780	1 270	0 000	1 660	1.490	2.190	1.530	1.310	0.000	1,190	2.140	1.350	0.000	3.630	1.650	2.050
	0.000	0.000	246	216	0.000	672	1071	1071	139	139	0	393	393	32	0	561	1595	1329
70 00	1 272	1 277	2 5 4 4	20 515	1 613	2 320	3 072	-3 260	-0 753	23.090	25.545	12.287	19.705	37.245	1.447	4.295	44.659	-28.931
/0.00	-1.2/2	1.277	2.044	30.313	4.0IJ	2.520	1 990	1 880	2 0 2 0	2 0 2 0	2 410	1 750	1.850	2.370	0.000	3.430	3,180	2,720
	1.940	1.970	2.000	2.020	2.200	1011	1001	1911	130	130	11	476	821	360	0.000	591	2172	1855
60.00	367	524	3918	10 707	4/30	14 251	1901	1011	1 554	10 502	1 212	6 132	1 115	7 401	17 152	9 482	10 302	17.780
60.00	-19.374	-39.412	-10.106	-10./9/	1 700	14.551	1 560	1 550	1 440	-10.302	1 150	0.452	1 410	0 950	1 480	0 970	1 410	1.580
	1.520	1.580	1.000	2.300	1.700	1.440	1712	2016	1020	200	1.130	0.520	1271	360	410	456	799	5078
	6651	69//	/500	81/5	2020	10 736	10 547	2310	15 400	16 942	22 101	50 105	20 122	_9 5/9	-10 611	_2 135	1 194	-5 705
50.00	-/.893	-35.45/	-33.851	-12.385	-3.95/	-18./30	19.54/	20.440	1 210	-10.043	1 210	1 250	1 010	1 300	1 470	1 220	1 550	1 500
	1.000	0.890	0.900	1.000	1.220	1.410	2.010	1.700	1.310	1.390	1.510	1005	010	201	1.470	587	177	8247
	644/	66/9	3651	1494	823	3099	0000	54/6	2400	490	100/	1033	EU EU3	21 602	17 957	41 756	-15 316	16 993
40.00	-4.484	-5.432	1.44/	1.44/	1.44/	8.64/	-/5.81/	-60.206	1 250	-9.033	-00.030	-09.993	-50.505	1 020	-17.007	1 370	-12.210	1 160
	0.950	0.800	0.000	0.000	0.000	1.420	1.810	1./40	1.350	1.400	1.0/0	1.000	1.070	212	202	1.370	520	4156
	23	21	0	0	1	4580	10080	9270	17 010	2835	220/	10 200	500 E0 221	24 104	11 622	17 265	_10 678	_1 483
30.00	1.447	-10.004	-11.506	-0.040	1.44/	26.118	61.6/5	-1.146	1/.818	13.018	-3.1/0	-49.209	-50.321	1 1 20	-11.035	0.060	-13:010	0 830
	0.000	0.770	0.660	0.390	0.000	0.520	1.220	1.270	1.180	1.080	1.060	0.880	1.030	1.120	710	551	362	267
	0	19	91	72	0	2167	5134	6043	486/	2520	10 764	10 150	17 046	10 602	12 562	0 065	20 568	10 513
20.00	1.447	-7.262	-3/./03	-34.489	1.44/	1.44/	17.988	4.050	-28.885	-0.163	-13./04	-18.150	-1/.040	-10.003	-12.502	-9.905	-20.500	-19.515
	0.000	0.740	0.920	0.690	0.000	0.000	0./10	0.950	1.190	1.020	0.910	0.860	1.050	1.080	1.110	1.100	0.000	0.500
	0	19	123	104	0	0	34	1192	2272	1627	832	592	004	125	2 6 6 2	12 120	20 026	4/
10.00	1.447	1.447	-11.982	-17.727	1.447	1.447	1.44/	3.527	-0.802	-4.266	-32.190	-51.843	-29.196	-6.986	-2.002	-13.139	-28.036	-45.552
	0.000	0.000	0.820	0.760	0.000	0.000	0.000	0.790	1.130	1.060	0.910	0.900	1.030	1.100	1.050	0.940	0.710	1422
	0	0	32	32	0	0	0	701	18/2	2590	3340	2481	669	368	2 1 2 7	293	224	1423
0.00	1.447	1.447	1.447	1.447	1.447	1.447	1.295	1.782	1.716	-4.361	0.6/3	-12.848	-15.335	-4.309	2.12/	1.403	-39.407	-35.269
	0.000	0.000	0.000	0.000	0.000	0.000	0.480	0.760	0.930	1.050	0.980	1.000	0.980	1.0/0	1.070	0./40	0.620	0.490
	0	0	0	0	0	0	20	233	343	1117	3299	2405	98	19	234	328	2 2 2 3	1/69
-10.00	21.058	15.591	7.175	20.877	20.638	7.927	1.576	0.960	1.290	-3.131	-9.219	11.925	6.035	5.880	5.//2	2.580	-3.004	-9.346
	0.890	0.490	0.460	0.730	0.450	0.400	0.420	0.620	0.720	0.650	0.820	0.850	0.910	0.860	0./50	0.740	0.480	0.420
	1728	1635	77	6357	6357	58	249	265	125	200	1115	1113	207	120	123	45	660	5/8
-20.00	22.944	24.098	14.870	9.078	30.275	21.454	7.345	4.258	2.230	1.447	-2.286	16.833	12.631	9.119	5.349	1.447	1.1/0	0./81
	1.130	0.830	0.690	1.240	0.530	0.580	0.520	0.490	0.570	0.000	0.390	0.560	0.650	0.640	0.530	0.000	0.340	0.570
	3930	3288	165	6663	6915	392	361	371	90	0	1088	1313	208	118	117	0	356	356
-30.00	1.039	5.941	9.105	8.200	10.357	15.493	9.935	7.452	4.588	1.360	-1.677	-5.975	2.652	4.756	1.447	1.447	1.453	1./44
	1.080	0.620	0.540	0.590	0.480	0.470	0.510	0.510	0.410	0.380	0.330	0.380	0.420	0.730	0.000	0.000	0.160	0.250
	2746	2050	66	306	558	334	132	226	147	31	1355	1454	124	50	0	0	171	1/1
-40.00	-6.864	-1.447	1.447	1.447	1.447	1.447	4.220	4.250	4.440	1.963	-1.319	-5.279	-4.292	0.719	1.447	1.447	2.599	2.108
	1.090	0.580	0.000	0.000	0.000	0.000	0.320	0.410	0.400	0.290	0.320	0.260	0.330	0.340	0.000	0.000	0.140	0.130
	1086	348	0	0	0	0	13	39	69	83	582	627	123	49	0	0	64	64
-50.00	-1.226	1.447	1.447	-0.463	-3.801	-3.583	-0.407	1.024	1.760	1.7-4	-0.622	-4.319	-9.877	-9.073	-1.315	1.740	2.538	2.713
	0.980	0.000	0.000	0.170	0.160	0.110	0.150	0.210	0.220	0.200	0.180	0.240	0.220	0.230	0.250	0.150	0.130	0.140
	553	0	0	65	115	50	13	13	12	52	62	50	56	40	12	280	331	67
-60.00	1.447	1.447	1.447	1.337	0.108	-0.543	1.447	1.447	1.447	1.447	1.447	-0.757	-4.375	-13.030	-14.663	-4.413	0.308	1.945
	0.000	0.000	0.000	0.030	0.060	0.060	0.000	0.000	0.000	0.000	0.000	0.200	0.220	0.220	0.240	0.230	0.230	0.180
	0	0	0	65	115	50	0	0	0	0	0	28	81	87	61	342	326	27
-70.00	1.447	1.447	1.447	1.447	1.447	1.447	1.447	1.447	1.447	1.447	1.447	1.447	0.350	-1.879	-6.572	-9.004	-5.303	-1.503
	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.330	0.340	0.220	0.320	0.340	0.300
	0	0	0	0	0	0	0	0	0	0	0	0	25	47	49	45	27	153
-80.00	1.447	1.447	1.447	1.447	1.447	1.447	1.447	1.447	1.447	1.447	1.447	1.447	1.447	1.447	1.447	1.447	1.447	3.823
	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.380
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	153

Depth = 12 km

80.00 90.00 100.00 110.00 120.00 130.00 140.00 150.00 160.00 170.00 50.00 60.00 70.00 0.00 10.00 20.00 30.00 40.00 1.447 -1.964 17.760 1.447 -13.710 -5.467 -5.063 17.960 3.786 -14.049 1.447 1.447 80.00 20.538 55.092 17.138 1.447 1.447 -1.2393.820 1.650 1.140 1.260 0.000 0.000 0.000 1.580 1.190 1.310 2.610 1.400 2.150 0.000 0.000 1.150 0.970 0.000 108 309 397 99 0 0 0 398 15 0 0 38 60 57 0 15 102 504 1.447 0.794 10.706 7.408 -2.985 -1.991 -0.566 12.022 10.199 1.447 70.00 -41.556 -14.179 17.899 15.503 6.942 1.447 1.447 1.447 2.180 2.680 2.270 1.910 1.850 1.810 1.070 0.820 0.000 0.000 3.030 3,090 2.610 3.030 3.460 0.000 0.000 0.000 95 0 483 574 167 75 177 218 4358 2052 15 0 0 0 95 0 710 2985 20.719 15.944 11.692 0.681 -8.494 28.253 1.126 -25.847 -53.285 -19.416 5.378 8.528 12.663 15.236 20.959 33.030 37.347 30.867 60.00 1.330 1.420 1.310 1.250 1.360 1.210 0.930 1.350 1.090 1.250 1.360 1.060 1.410 1.330 1.940 2.220 2.300 1.680 1302 2172 3390 288 536 1040 1600 1120 426 385 848 286 588 314 7440 10059 10284 4088 23.755 13.282 11.820 20.816 37.201 56.948 67.361 68.566 66.152 64.331 46.970 -8.562 40.317 -55.249 -54.821 -12.338 4.080 50.00 19.180 1.550 1.490 1.370 1.510 1.380 1.320 1.060 1.050 1.030 1.230 1.460 1.210 1.340 2.010 2.500 2.060 1.330 1.060 4081 2722 8691 13332 6106 3290 1643 1204 2716 26357 30583 14782 4923 2444 1691 796 1483 2409 5.700 51.860 68.416 76.163 78.075 76.858 71.487 43.634 13.852 1.447 40.00 56.518 -75.633 -64.366 -48.380 -52.866 -8.748 4.196 -9.193 2.080 1.930 1.950 1.160 0.780 0.000 1.410 1.830 2.610 2.200 1.900 1.080 1.340 1.340 1.270 1.470 1.580 1.840 6699 13850 14851 4100 0 19525 23265 9806 3547 2282 2454 1770 3587 3770 2995 4680 7827 7545 70.052 66.354 42.409 1.447 1.447 9.681 -45.155 -71.565 -63.429 -55.472 -56.908 62.808 72.618 -4.592 -14.382 -58.632 -20.043 42.877 30.00 1.220 0.000 0.000 1.830 2.160 2.080 2.290 2.350 1.900 1.760 0.630 0.830 1.210 1.480 1.480 1.690 1.620 1.520 3496 4097 6311 8586 8659 6801 6901 6330 2838 0 0 972 2123 3323 359 443 980 1123 21.199 -0.839 -32.301 -13.016 34.331 49.336 47.001 33.039 14.585 1.447 1.447 1.447 -61.722 -53.163 -52.275 -23.578 20.00 1.447 1.447 0.000 0.990 1.530 1.680 1.640 1.610 1.580 1.680 1.830 1.860 1.650 1.310 1.160 1.150 0.000 0.000 0.000 0.000 2527 4348 4438 2164 1368 0 2242 2814 4171 5983 5795 0 0 0 313 727 2026 1.447 -15.388 -15.346 -18.385 -9.381 1.447 10.00 -24.162 -14.894 -16.021 2.774 -6.117 -5.325 -2.811 -1.418 -10.059 -15.424 -24.837 -12.069 1.370 1.540 0.880 0.630 0.740 0.000 0.000 1.350 1.430 1.340 0.420 0.650 1.180 1.450 1.500 1.350 0.840 0.360 1469 1364 0 0 1804 4621 2669 4451 3705 1292 273 273 432 836 1011 666 1730 2713 -0.649 -4.786 -18.807 -38.873 -30.440 -40.472 -28.605 3.697 1.046 4.024 0.00 -23.305 -14.133 -25.838 7.193 23.612 10.754 10.865 9.675 1.280 1.120 1.030 0.360 1.020 1.080 0.820 0.970 1.280 1.270 1.520 1.450 0.480 0.720 0.810 1.020 0.750 0.450 12 1016 806 58 256 269 219 1849 3931 3512 4485 4485 3147 4212 2430 1292 273 492 12.501 4.673 -0.983 -6.024 -37.182 -49.309 -70.513 -33.217 5.138 18.593 12.084 4.640 13.532 11,923 10.446 -10.00 1.447 1.447 7.825 1.890 0.480 0.700 0.780 1.330 1.630 2.020 1.780 1.580 1.490 0.000 0.000 0.350 0.560 0.700 0.700 0.700 0.640 692 1123 1680 2665 3934 4188 4347 4500 2228 329 932 777 186 453 613 309 0 0 -63.177 -27.146 -33.511 44.038 23.863 18.334 4.958 0.971 -8.424 -30.146 -20.00 1.447 -3.661 2.772 23.549 9.133 5.196 5.507 6.026 0.480 0.430 0.530 1.170 1.710 2.130 2.360 2.080 1.780 1.600 0.000 0.250 0.350 0.510 0.450 0.700 0.690 0.730 779 1161 3966 4332 1063 2738 3278 224 359 463 104 61 61 215 2311 2386 540 0 48.862 28.311 30.477 10.086 -5.626 -26.768 -12.153 6.122 3.644 2.332 3.022 3.079 2.581 1.447 -17.574 -35.440 -5.678 -30.00 1.447 1.620 1.550 1.520 0.940 0.430 0.460 0.530 0.710 0.650 0.530 0.000 0.770 1.480 1.370 1.740 0.000 0.250 0.630 4568 3062 909 1206 198 185 132 53 44 18 0 2287 2558 2481 0 430 2613 2322 2.605 2.759 2.996 0.790 -0.008 21.192 20.944 11.499 -4.524 1.447 -0.503 -6.508 -10.441 -4.060 1.558 1.639 1.717 1.264 -40.00 0.940 0.960 1.240 0.290 0.310 0.380 0.460 0.490 0.420 0.490 0.650 0.790 0.970 0.300 0.340 0.000 0.200 0.260 183 421 242 41 146 105 13 53 51 11 1841 2122 570 1925 2051 490 794 0 1.447 1.534 1.550 -1.389 2.534 2.955 3.489 3.727 7.404 5.082 2.801 1.013 1.447 1.447 1.447 1.447 -50.00 1.641 1.004 0.850 0.190 0.220 0.390 0.320 0.330 0.340 0.590 0.450 0.580 0.160 0.130 0.110 0.000 0.000 0.000 0.000 0.000 30 56 109 177 199 646 22 33 11 15 45 40 11 0 0 0 0 0 1.551 1.801 2.098 2.107 3.068 1.454 1.902 1.200 1.447 1.447 1.447 2.922 1.632 1.447 1.447 1.447 -4.467 -60.00 2.749 0.170 0.190 0.090 0.000 0.000 0.000 0.220 0.070 0.000 0.000 0.000 0.370 0.240 0.210 0.260 0.320 0.300 0.390 378 109 209 155 17 45 40 11 0 0 0 484 484 0 0 0 378 41 2.247 4.123 1.086 2.752 2.295 1.447 1.447 1.447 2.550 2.753 1.447 1.4.7 1.447 -2.118 -2.591 1.447 1.447 3.173 -70.00 0.000 0.000 0.170 0.230 0.210 0.310 0.350 0.000 0.000 0.000 0.500 0.590 0.210 0.310 0.310 0.000 0.000 0.000 34 269 237 484 484 0 0 0 378 378 0 0 153 70 70 0 0 0 1.447 -0.098 1.447 -5.954 -5.404 1.447 1.447 1.447 13.511 31.310 6.712 3.408 1.447 1.447 1.447 1.447 1.447 -80.00 3.418 0.000 0.630 0.350 0.000 0.000 0.000 0.710 3.320 0.280 0.450 0.000 0.000 0.000 0.000 0.000 0.000 0.060 0.700 0 6 2 231 311 0 0 3 237 237 153 70 70 0 0 0 0 1

-180.00 -170.00 -160.00 -150.00 -140.00 -130.00 -120.00 -110.00 -100.00 -90.00 -80.00 -70.00 -60.00 -50.00 -40.00 -30.00 -20.00 -10.00 80.00 -0.277 52.205 27.581 -34.454 -0.277 6.412 -17.247 -6.734 49.993 28.174 -7.144 36.373 51.707 5.201 -0.277 51.867 -66.287 -53.313 2.350 0.000 1.760 1.380 1.730 1.840 1.440 1.210 1.420 1.150 1.820 2.400 0.000 1.510 1.460 0.000 3,170 1.940 514 139 139 5 393 394 84 1 730 1602 1429 0 12 246 246 0 727 1071 1.775 -6.481 -6.120 19.548 21.749 6.883 20.260 34.922 20.161 11.872 14.106 -25.593 -5.159 -3.001 0.028 25.618 24.246 70.00 -1.574 2.220 1.990 1.780 2.280 2.060 Z.050 1.900 2.100 1.880 1.960 1.900 1.810 1.810 1.980 2.180 2.500 2.050 2.480 1248 139 139 110 512 821 360 8 855 2184 1979 541 5114 7055 4765 1903 2000 378 9.317 18.894 18.097 -1.224 7.703 3.904 16.236 16.473 6.237 9.014 2.468 4.559 -2.505 -12.038 60.00 -17.576 -28.753 -7.884 -13.215 0.950 0.950 0.880 1.290 0.880 1.330 0.860 1.180 1.260 1.460 1.610 2.160 1.550 1.160 1.300 1.120 1.210 1.440 362 413 641 868 5078 1681 1598 2316 1044 221 117 969 1274 9154 8567 5611 8155 8837 7.648 -1.934 -2.330 26.872 13.510 8.817 -17.675 -25.192 -41.543 -13.384 -3.861 -0.448 8.982 50.00 -4.738 -27.830 -31.067 -11.534 1.798 1.800 1.510 1.030 0.960 1.110 1.180 0.700 0.890 1.160 0.940 1.230 1.250 1.440 1.090 1.140 1.210 1.250 1.170 221 446 597 193 7955 6135 5796 2954 507 1375 1882 819 1810 925 3379 7824 8375 4291 42.309 -13.562 -52.754 -63.247 -38.603 -13.549 -4.656 40.00 -0.396 -4.450 -0.277 -0.277 -0.277 31.304 -64.295 -36.126 -6.650 -19.580 17.427 0.980 0.620 0.760 1.030 1.050 1.590 1.140 0.650 0.650 0.610 0.000 0.000 1.290 1.720 1.510 1.440 1.010 0.000 2796 2411 1693 369 327 341 745 533 3694 108 64 0 0 4 5050 10528 9025 5724 32.871 10.784 -5.364 -42.054 -40.027 -21.147 -5.294 -7.512 -10.790 -0.469 30.00 -0.277 -11.649 -14.792 -3.250 -0.277 30.166 64.352 33.465 0.720 0.400 0.550 0.560 0.600 0.520 0.540 0.590 0.000 0.490 1.210 0.940 0.970 0.850 0.000 0.990 0.920 0.540 72 0 2509 5642 6382 4880 2493 1113 407 69 524 718 576 350 199 22 91 0 32.507 21.077 -8.505 -17.938 -18.121 -23.361 -16.976 -8.848 -15.102 -13.997 -0.277 -0.277 23.421 28.917 20.00 -0.277 -10.613 -42.574 -39.705 0.410 0.590 0.730 0.590 0.570 0.000 0.740 0.870 0.760 0.000 0.000 0.610 1.010 0.910 0.960 0.510 0.480 0.690 1035 756 706 13 58 95 35 1570 3487 3427 1759 1226 123 104 0 0 0 31 33.138 28.972 -31.181 -55.659 -38.558 -12.038 -5.967 -18.581 -31.192 -34.025 -0.277 -0.277 -0.277 10.00 -0.277 -0.277 -17.134 -24.219 13.429 0.000 1.010 0.000 0.000 0.000 0.660 0.950 0.960 0.910 0.590 0.680 0.620 0.790 0.870 0.690 0.820 0.000 0.760 365 510 293 334 1533 1159 3144 4318 4410 3071 1041 39 38 0 0 0 0 0 0.00 -0.277 -0.277 -0.277 -0.277 -0.277 -0.277 0.151 1.974 6.182 2.859 -3.174 -16.621 -20.884 -9.380 -0.913 -0.629 -51.760 -40.252 0.650 0.770 0.680 0.940 0.970 0.610 0.610 0.780 0.810 0.800 0.600 0.000 0.000 0.000 0.000 0.000 0.000 0.430 235 1279 4074 3096 116 20 240 333 606 1787 0 0 0 0 0 0 20 345 0.311 -0.416 -5.084 -9.732 11.589 3.028 3.054 3.005 0.845 -4.694 -12.794 -10.00 37.071 17.663 -7.929 -5.116 16.618 8.084 1.841 0.380 0.560 0.480 0.390 0.780 0.800 0.730 0.430 0.400 0.680 0.540 0.320 0.400 0.590 0.590 0.550 0.800 0.680 120 123 55 643 592 1996 1012 6357 6134 58 249 265 125 265 2032 2112 284 2155 1.708 39.334 13.386 7.397 3.380 -0.277 0.270 -0.240 17.432 19.023 9.548 6.182 -0.277 5.639 -20.00 47.317 31.521 2.885 -26.562 0.810 0.790 0.780 0.000 0.350 0.400 0.490 1.220 0.530 0.580 0.440 0.410 0.450 0.000 0.430 0.780 0.650 0.790 119 0 356 356 6711 392 361 371 90 0 1881 2438 506 118 4919 4061 1221 6635 0.650 -0.277 0.054 9.887 5.358 1.628 1.898 16.438 16.565 5.212 -0.277 -30.00 9.617 7.988 6.145 -0.666 -1.289 11.341 9.668 0.350 0.280 0.510 0.590 1.010 0.000 0.000 0.110 0.250 0.690 0.530 0.570 0.560 0.520 0.490 0.450 0.500 0.260 171 226 150 35 2194 2529 260 50 0 0 171 3507 2605 138 270 556 334 132 -0.277 -0.277 0.984 0.458 -1.346 -0.277 -0.277 -0.277 -0.277 2.775 3.429 4.316 1.897 -1.350 -3.859 2.120 4.367 -40.00 -0.962 0.180 0.110 0.390 0.300 0.290 0.250 0.360 0.380 0.000 0.000 0.600 0.000 0.000 0.000 0.000 0.370 0.410 1.000 49 0 64 64 1340 495 0 0 0 0 14 40 69 83 1029 1078 124 -50.00 -3.000 -0.277 -0.277 -2.398 -6.099 -5.435 -1.860 -0.474 0.263 0.433 -2.044 -6.169 -12.024 -9.323 -0.003 2.380 1.953 1.204 0.250 0.250 0.190 0.160 0.140 0.240 0.150 0.180 0.260 0.250 0.230 0.310 0.340 0.270 1.050 0.000 0.000 0.190 115 50 13 13 12 52 67 56 56 41 14 416 467 68 596 0 0 65 -60.00 -0.277 -0.277 -0.277 -0.381 -1.852 -2.610 -0.277 -0.277 -0.277 -0.277 -0.277 -2.690 -6.834 -16.416 -17.099 -3.662 1.516 1.555 0.290 0.000 0.000 0.000 0.030 0.070 0.090 0.000 0.000 0.000 0.000 0.000 0.280 0.330 0.340 0.250 0.290 0.190 0 33 81 87 61 464 451 30 0 0 0 65 115 50 3 3 0 0 -70.00 -0.277 -0.277 -0.277 -0.277 -0.277 -0.277 -0.277 -0.277 -0.277 -0.277 -0.277 -0.277 -0.277 -0.386 -1.542 -4.005 -9.180 -11.375 -6.183 -1.665 0.000 0.390 0.300 0.400 0.410 0.360 0.400 0.310 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 5 25 47 44 68 47 155 0 0 0 0 0 0 0 0 0 0 0 -80.00 -0.277 -0. -0.277 -0.277 1.894 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.310 0.000 0.000 0.000 0.000 0.000 0 0 153 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

80.00 90.00 100.00 110.00 120.00 130.00 140.00 150.00 160.00 170.00 60.00 70.00 30.00 40.00 50.00 0.00 10.00 20.00 9.459 -24.741 -28.512 -16.884 19.316 11.071 -8.664 -0.277 -0.277 -0.277 80.00 20.770 53.542 23.881 -1.967 -10.517 -2.680 -2.773 14.448 0.860 1.400 2.710 0.000 0.000 0.000 1.240 0.990 2.370 1.760 2.420 1.110 0.750 0.970 1.240 1.010 1,150 1.840 2 0 0 60 17 66 106 191 348 397 114 530 405 107 40 30 42 60 8.780 11.160 -4.400 -13.764 -13.683 2.327 5.224 -1.874 -2.100 -1.606 -0.277 -0.277 -0.277 17.841 18.832 8.375 70.00 -37.329 -12.151 2.250 2.260 1.550 2.100 1.600 2.210 1.610 1.880 1.640 2.290 0.000 0.000 2.210 2.060 1.940 2.050 1.970 0.000 18 171 399 95 95 51 10 460 581 241 4313 2140 246 0 1 1 949 2973 13.734 23.051 26.822 17.043 8.761 -1.117 -4.626 0.135 0.837 -7.461 7,271 9.734 10.747 10.977 0.967 -18.847 -51.076 -20.242 60.00 0.880 1.020 1.280 1.240 1.300 1.180 1.310 1.220 1.820 1.520 1.230 0.910 0.830 1.210 1.120 1.090 1.550 1.810 1083 437 468 2692 4411 4847 335 588 515 338 541 1133 1597 950 7676 10546 11303 4457 8.806 12.360 22.032 37.204 55.894 57.329 17.078 0.313 25.065 -2.601 54.652 52.179 50.00 21.052 45.480 -30.896 -50.738 -7.617 5.797 1.250 1.500 1.360 1.160 1.200 1.230 0.960 1.240 1.640 1.290 1.130 1.300 1.460 1.380 1.670 2.040 1.710 1.050 2735 13982 21123 10175 4501 2550 1738 1348 2763 4005 2489 2034 1087 1757 26581 31003 15421 5070 10.816 14.788 -6.219 2.779 -17.012 -13.325 23.218 47.549 58.775 64.003 68.517 63.640 33,601 40.00 52.488 -70.243 -58.419 -12.039 -39.424 1.030 0.930 1.620 2.010 1.410 1.250 1.210 2.220 1.560 1.280 1.350 1.370 1.180 1.520 1.800 0.850 1.230 1.020 5957 34 5230 8077 7797 7183 20921 22821 24104 10183 3715 2475 3058 2310 4257 4433 2679 19637 8.849 -33.603 -67.006 -53.897 -46.348 -59.837 -13.253 -18.786 -58.767 -52.290 14.285 14.512 22.454 45.543 56.674 32.725 -0.277 -0.277 30.00 1.550 1.690 1.670 1.370 1.200 0.000 0.000 1.700 1.160 1.080 1.390 1.850 1.620 0.470 0.590 0.920 0.840 0.610 1122 2379 3459 4089 4790 6139 9081 9291 8486 8492 8811 4921 0 0 1108 1239 329 450 -9.481 -32.537 -14.950 -2.333 -10.438 9.188 15.222 -0.277 -0.277 20.00 -4.652 -0.277 -0.277 -58.194 -50.036 -48.455 -29.409 21.143 34.706 1.210 0.000 0.000 1.210 1.080 1.170 0.000 0.670 0.630 0.580 0.840 0.970 1.260 1.360 1.410 1.170 0.430 0.000 6583 6257 3203 2201 1 0 2879 4294 6581 6371 3673 308 733 2054 2324 50 0 0 11.242 -9.465 -31.479 6.903 -0.277 -0.277 -6.344 -14.439 -11.140 -16.988 -0.941 10.00 -14.443 -15.269 -14.782 3.456 -4.130 -0.829 0.758 0.850 0.890 1.140 1.090 1.040 0.660 1.080 0.860 0.920 1.050 0.000 0.000 0.520 0.630 0.800 0.370 0.370 0.420 1927 1 0 3483 5209 3294 6600 5857 2056 1029 666 1808 1730 1292 274 295 460 831 6.690 21.397 10.326 12.682 8.852 -12.199 -2.599 -4.737 -22.680 5.863 18.284 4.127 46.327 35.398 6.533 0.00 -19.222 -12.434 -26.004 0.920 0.740 0.780 0.730 0.710 0.800 0.830 0.400 0.520 0.530 0.650 0.980 0.970 0.840 0.610 0.370 0.500 0.610 6975 7495 4708 6667 4005 13 274 528 1059 809 74 267 284 225 2592 5506 4762 1292 1.053 -20.444 -24.593 -63.624 -5.950 35.622 63.274 50.375 9.539 11.855 16.244 0.092 -2.940 1.296 2.637 8.490 -10.00 -0.277 -0.277 0.930 0.770 1.080 0.600 0.490 0.650 0.690 0.690 0.620 0.610 0.760 0.930 0.770 0.000 0.000 0.400 0.560 0.590 781 204 453 613 309 765 2028 2727 3513 5577 6364 6965 7315 3537 369 969 0 29.968 -63.154 -36.018 -52.353 42.097 55.775 0.956 7.588 5.622 -0.856 -6.810 -27.601 17.924 4.171 4.755 -20.00 -1.232 -3.187 1.733 0.590 0.630 0.590 0.540 0.460 0.390 0.460 0.590 0.950 1.250 1.590 1.160 0.860 1.060 0.330 0.260 0.310 0.480 242 354 458 106 63 61 850 1324 4028 4417 1201 4054 4569 212 2308 2390 527 5 2.195 -0.277 -16.706 -45.164 -20.539 23.209 9.272 20.560 17.456 -30.00 -0.817 -5.804 -20.566 -9.744 3.305 0.492 0.017 2.351 3.908 1.120 0.630 0.910 0.950 0.840 0.820 0.540 0.770 0.440 0.670 0.650 0.640 0.520 0.420 0.000 0.510 0.350 0.400 0 2110 2558 2584 4257 2743 1097 1450 2297 189 185 135 54 46 18 5 436 2572 -4.449 -0.745 -0.520 -0.276 0.561 0.402 1.264 0.438 -3.485 -7.115 12.494 11.099 3.689 -6.956 -40.00 -0.277 -1.992 -6.710 -9.339 0.480 0.500 0.540 0.640 0.730 1.030 0.240 0.310 0.450 0.500 0.430 0.410 0.360 0.360 0.000 0.370 0.260 0.380 2073 573 936 458 289 41 146 110 13 53 51 11 1833 2115 573 1925 0 218 4.349 -0.277 -0.277 -0.277 -0.731 -4.121 -3.669 0.554 0.533 0.892 0.834 1.133 -0.085 -0.730 -0.277 -0.277 -50.00 -0.214 -0.835 0.350 0.490 0.340 0.480 0.850 0.000 0.000 0.240 0.260 0.270 0.290 0.270 0.120 0.120 0.180 0.000 0.000 0.000 0 22 33 11 15 30 56 109 181 223 707 40 15 0 0 0 0 45 -0.114 -0.277 -0.277 -6.954 -7.711 -0.719 -0.301 0.344 0.650 1.756 -0.544 -0.277 -0.277 -0.277 0.970 -60.00 1.412 0.197 -0.584 0.380 0.120 0.000 0.000 0.000 0.180 0.060 0.000 0.000 0.440 0.420 0.180 0.150 0.280 0.290 0.250 0.150 0.280 378 41 109 211 155 14 15 0 0 1 484 484 0 0 14 378 50 40 -0.277 -0.277 -1.993 -6.966 -5.710 -0.277 -0.277 0.479 2.157 1.573 0.354 1.409 0.665 -0.277 -0.277 -0.277 0.902 1.008 -70.00 0.770 0.000 0.000 0.180 0.210 0.220 0.000 0.240 0.270 0.000 0.000 0.630 1.030 0.210 0.500 0.000 0.000 0.460 378 0 0 42 269 237 484 484 0 0 14378 159 70 70 0 0 1 -0.277 2.782 -1.552 -1.295 -2.926 -9.934 -4.287 7.742 4.959 -1.055 10.646 22.880 -0.277 2.083 -80.00 0.362 3.650 0.999 -0.277 0.370 0.120 0.240 0.190 1.020 0.600 0.590 0.460 0.170 1.410 0.830 0.000 0.000 0.000 0.180 0.660 0.190 0.580 154 70 70 0 0 4 13 40 45 45 48 982 1116 200 17 10 237 237

	-180.00	-170.00	-160.00	-150.00	-140.00	-130.00	-120.00	-110.00	-100.00	-90.00	-80.00	-70.00	-60.00	-50.00	-40.00	-30.00	-20.00	-10.00
80.00	2.428	39.653	5.734	-29.689	2.428	16.710	-15.735	-11.579	46.286	23.365	-2.893	39.307	27.171	4.547	11.429	14.230	-24.816	-49.976
	0.000	2.080	1.250	1.690	0.000	1.280	1.170	1.380	1.330	1.090	1.040	1.380	1.000	0.860	2.110	1.410	1.330	1.190
	0	174	246	249	0	737	1071	414	179	139	196	334	594	296	48	656	1588	1221
70.00	-1.109	1.235	18.780	10.097	-10.085	-3.849	5.542	-4.643	-7.411	17.023	18.555	7.442	21.772	23.365	13.924	13.025	15.647	-2.398
	1.590	1.900	1.940	2.120	2.070	2.050	1.760	2.160	2.020	1.940	1.850	2.210	1.960	1.790	1.920	2.150	2.130	2.030
	384	986	5950	7375	3773	1925	2101	1156	193	142	281	514	779	361	65	948	2219	1815
60.00	-25.869	-23.685	-4.842	-13.256	-2.277	1.174	-2.463	2.224	-3.628	-10.957	-1.923	7.603	4.701	10.254	14.112	12.753	12.115	7.718
	1.040	1.110	1.160	1.500	1.210	0.990	0.890	0.730	0.910	0.730	0.630	0.710	0.870	0.770	0.970	0.690	0.890	1.070
	8374	9241	10347	9062	4856	1829	1775	2130	1060	298	306	972	1316	405	456	722	993	5223
50.00	-17.022	-31.268	-27.038	-7.707	0.778	-8.346	17.284	5.936	5.059	-15.188	-18.934	-35.518	-9.458	-1.969	0.452	5.930	4.220	-4.501
	0.920	0.820	1.240	0.830	0.920	0.760	1.410	1.230	0.760	0.670	0.780	0.950	0.560	0.600	0.790	0.650	0.870	1.000
	8059	8561	4666	2287	1114	3373	5833	5451	2741	662	1384	1859	846	222	489	635	343	7961
40.00	-8.330	-8.538	-10.327	2.428	9.117	21.386	-60.750	-25.701	29.728	-11.651	-44.901	-48.982	-26.559	-8.321	-4.410	-16.140	-6.133	12.522
	0.770	0.490	0.390	0.000	0.580	0.810	1.310	1.060	0.850	0.730	1.310	0.770	0.530	0.480	0.480	0.690	0.480	0.520
	568	400	17	1	13	5396	10424	9533	5459	2737	2533	1762	383	333	418	762	510	3559
30.00	2.428	-6.022	-9.099	-2.037	2.428	28.210	54.267	17.342	27.971	6.691	-6.833	-31.591	-23.648	-13.440	-2.018	-4.883	-8.008	1.092
	0.000	0.600	0.630	0.540	0.000	0.620	0.980	0.640	0.540	0.590	0.610	0.380	0.430	0.460	0.460	0.490	0.450	0.440
	0	44	91	70	0	2818	5819	6176	4246	2442	1489	/05	12	507	11 265	584	353	181
20.00	2.428	-4.372	-24.505	-24.223	2.428	2.428	17.814	17.375	40.975	25.468	-3.4/0	-15.303	-10.004	-14.499	-11.205	~5.3/8	-9.195	-0./3/
	0.000	0.450	0.510	0.560	0.000	0.000	0.490	0.710	0.610	0.650	0.380	0.450	1200	0.480	0.540	0.000	U.4/U	105
	0	50	123	103	0	0	41	1592	3889	3980	2012	1419	1200	/4Z	1 642	11 200	24 054	22 269
10.00	2.428	2.428	-13.076	-18.145	2.428	2.428	2.428	12.144	34.302	33.724	-13.045	-4/.00/	-33.091	-0.055	-1.042	-11.209	0 500	-22.200
	0.000	0.000	0.490	0.570	0.000	0.000	0.000	1226	2620	1021	5020	3756	1237	360	530	323	387	1561
0 00	2 420	J 2 4 2 0	2 4 2 0	2 4 2	2 1 2 0	2 120	2 002	1 1220	0 201	9 916	_1 749	_10 597	_15 898	_7 043	1 991	3.046	-35.830	-29.738
0.00	2.428	2.428	2.420	2.420	2.420	2.420	2.002	4.421	0.730	0.010	0 680	0 530	0 310	0.380	0.570	0.540	0.560	0.520
	0.000	0.000	0.000	0.000	0.000	0.000	20	235	345	1287	5198	4259	122	24	259	333	620	1755
10 00	22 101	11 666	3 638	7 485	18 728	9 965	4 611	3 227	2 936	-0.627	-1.675	10,905	3.849	4.755	4,683	3,657	0.303	-6.339
-10.00	0 450	0 320	0 280	0 530	0 330	0 340	0 320	0.470	0.530	0.450	0.500	0.510	0.470	0.590	0.430	0.460	0.350	0.260
	2423	2237	1775	6357	5181	58	249	267	128	364	2881	3258	589	120	125	58	533	441
-20.00	37.519	21.006	-3,900	-0.054	23.734	19.614	11.320	7.919	4.531	3.388	5.169	26.107	10.640	7.868	5.234	2.428	3.068	2.528
20.00	0.640	0.520	0.420	0.900	0.450	0.420	0.370	0.380	0.440	0.520	0.340	0.680	0.530	0.480	0.470	0.000	0.300	0.270
	5606	4649	2024	6624	5844	394	364	369	90	14	2152	3686	1719	120	120	1	327	329
-30.00	-6.150	2.605	1.759	2.068	7.427	13.778	11.039	10.883	7.374	4.791	5.532	14.874	11.189	5.629	2.428	2.428	2.769	3.208
	0.740	0.460	0.280	0.370	0.430	0.460	0.390	0.410	0.410	0.360	0.360	0.530	0.430	0.520	0.000	0.000	0.140	0.170
	3965	2976	223	301	461	334	142	226	158	42	2283	3499	1346	50	0	0	167	171
-40.00	-5.495	-3.794	2.428	2.428	2.428	2.428	5.028	5.307	6.187	4.584	2.733	0.250	3.412	4.631	2.428	2.428	3.430	3.017
	0.800	0.590	0.000	0.000	0.000	0.000	0.320	0.330	0.300	0.300	0.270	0.260	0.320	0.270	0.000	0.000	0.160	0.190
	1399	543	0	0	0	0	12	38	69	83	1114	1258	280	49	0	0	65	65
-50.00	-5.245	2.428	2.428	1.173	-2.106	-2.193	0.615	2.158	2.428	2.949	1.229	-1.869	-6.801	-5.426	1.742	4.507	4.295	3.627
	0.600	0.000	0.000	0.150	0.210	0.180	0.200	0.240	0.000	0.230	0.290	0.260	0.240	0.320	0.260	0.180	0.160	0.140
	587	0	0	65	115	51	15	13	1	41	75	63	56	49	37	496	539	71
-60.00	2.428	2.428	2.428	2.384	1.217	0.375	0.993	1.773	2.428	2.428	2.428	0.624	-2.583	-10.347	-11.428	-1.011	3.747	3.795
	0.000	0.000	0.000	0.020	0.060	0.080	0.070	0.050	0.000	0.000	0.000	0.230	0.240	0.270	0.220	0.270	0.190	0.220
	0	0	0	65	115	51	12	10	0	0	1	34	81	86	70	557	547	80
-70.00	3.484	2.428	2.428	2.428	2.428	2.428	2.428	2.428	2.428	2.428	2.428	2.346	1.480	-0.398	-4.53/	-6.534	-2.616	1.130
	0.240	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.280	0.230	0.290	0.300	0.270	0.300	0.250
	7	0	0	0	0	0	0	0	0	0	2 4 2 0	2 420	25	36	2 4 2 0	2 4 2 0	2 1 2 0	1 252
-80.00	1./33	2.428	2.428	2.428	2.428	2.428	2.428	2.428	2.428	2.428	2.428	2.428	2.428	2.428	2.428	2.428	2.420	4.233
	1.160	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	101
	10	0	()	0	U	0	0	0	0	0	0	0	0	0	0	0	0	101

	0.00	10.00	20.00	30.00	40.00	50.00	60.00	70.00	80.00	90.30	100.00	110.00	120.00	130.00	140.00	150.00	160.00	170.00
80 00	_2 119	40 317	27 293	2 661	-4.776	0.728	0.504	13.717	3.390	-21,456	-14.238	-8.409	12.267	-0.003	-10.020	-9.345	2.428	2.428
00.00	1 270	0 940	1 270	1 310	0 900	0 670	0 670	1.020	0.900	1.920	1.080	1.050	1,180	0.740	1.270	0.770	0.000	0.000
	1.270	0.040	1.270	100	35	36	68	47	79	80	146	196	347	356	145	6	0	0
70 00	0/9	10 050	7 714	15 270	0 660	2 129	2 129	2 128	9 31/	8 162	-1 664	-7 981	_7 588	1.318	-1.785	-7.441	-9.798	-3,124
/0.00	-24./38	-10.052	/ • / 14	15.270	0.003	2.420	2.420	2.420	1 970	1 700	1 040	1 500	1 620	1 590	1 600	1 930	1 720	1 660
	2.100	2.090	2.020	2.020	2.230	0.000	0.000	0.000	1.0/0	1./90	1.940	1.000	1.020	59/	282	20	152	438
	1087	2/59	4045	2163	84/	0 105	10 050	11 010	10 740	10 (7)		11 201	405	2 074	0 924	15 910	16 497	-18 510
60.00	2.688	-10.026	-43.390	-25.115	3.807	8.195	10.052	11.018	12.742	19.6/6	20.778	11.391	4.440	-3.074	- 7.034	-13.019	-10.407	-10.510
	1.230	1.200	1.390	1.270	0.8/0	0./10	0.630	0.860	0./80	0.780	0.620	0.850	0.850	0.860	0.890	0.020	4727	0.930 E101
	8413	12054	12317	4783	1635	618	588	541	303	525	988	1394	1008	496	481	3068	4/2/	27 520
50.00	16.804	33.744	-9.316	-43.986	-8.556	5.559	8.857	12.062	19.638	29.315	47.988	50.489	38.213	25.688	-0.099	-26.800	-3.630	-27.529
	1.300	1.510	1.320	0.860	0.860	0.770	0.830	0.920	0.870	1.060	1.080	0.680	0.910	0.770	0.670	1.240	1.080	0.630
	26588	31717	16389	5317	2562	2415	1079	1894	2680	1746	1860	2724	3370	2834	15571	23190	10976	4920
40.00	42.694	-57.436	-53.296	6.910	-25.666	-2.702	7.837	-9.420	-7.899	22.098	35.610	46.638	54.532	53.907	23.131	-0.409	-6.207	1.659
	0.870	1.070	1.190	0.760	0.930	0.990	0.630	1.020	0.800	0.980	1.250	1.050	0.950	0.820	1.380	1.170	0.640	0.700
	19676	23675	10239	3767	2625	3411	2451	4849	5245	2851	5639	7556	7316	8005	23068	25050	6485	203
30.00	9.178	-18.967	-55.207	-41.212	-31.943	-44.790	-7.670	-12.604	-49.400	-53.015	15.546	3.555	0.769	20.698	16.728	6.499	2.428	2.428
	0.340	0.380	0.580	0.530	0.400	0.980	0.770	0.700	0.800	1.270	0.970	1.250	1.320	1.120	1.180	0.540	0.000	0.000
	299	476	1096	1336	1231	2588	3463	4890	5699	6549	9330	9460	9832	10078	9723	5636	4	0
20.00	-0.070	2.428	2.428	-48.486	-44.171	-31.735	-18.415	-7.021	-27.988	-23.518	8.542	27.892	-15.341	-18.602	-6.724	2.400	2.315	2.428
20000	0.320	0.000	0.000	0.450	0.450	0.460	0.660	0.690	0.850	0.690	0.930	0.780	1.010	0.630	0.610	0.540	0.490	0.000
	59	0,0000	3	308	745	1950	2128	2858	4366	6749	6421	4343	7785	7158	3866	3033	20	0
10 00	_5 413	-9 250	-9.933	5.487	-2.781	-0.077	4.107	-2.572	-15,216	-15,969	-14.111	-0.113	10.424	-6.976	-41.091	-7.011	4.381	2.428
10:00	0 590	0 280	0 260	0.380	0.490	0.520	0.650	0.640	0.760	0.550	0.520	0.310	0.860	0.770	0.570	0.790	0.400	0.000
	1293	268	320	487	839	1065	666	1804	1730	3819	5634	3725	7588	6887	2707	2522	20	0
0 00	_13 688	-7 245	-19 805	8 256	20.938	10.261	12,210	9.083	-11,160	-7.536	-7.594	-21.890	5.903	26.872	-14.544	8.872	25.522	9.745
0.00	0 520	0 290	0 370	0 480	0.450	0.490	0.540	0.660	0.520	0.450	0.650	0.380	0.610	0.840	0.740	0.730	0.580	0.340
	1248	273	542	1085	810	131	293	279	232	2849	5836	4975	8792	9676	5513	7684	4631	85
10 00	2 129	2 4 2 8	2 891	3 646	8 010	10.339	11.840	15.405	1,137	-2.636	-4.661	-20.301	-12.717	-47.235	-21.086	-1.358	54.269	53.449
-10.00	0 000	0 000	0 320	0 4 3 0	0.490	0.540	0.480	0.470	0.370	0.370	0.430	0.520	0.610	0.830	0.770	0.800	0.940	0.780
	0.000	0.000	353	960	795	212	453	613	312	737	2076	2787	4568	6942	7250	7954	8816	4515
20 00	1 900	0 857	3 668	15 155	5 673	2 498	6.485	8.525	6.739	1,110	-2.771	-18,978	-50.892	-14.341	-45.145	4.064	20.204	46.188
-20.00	0 230	0.057	0 240	0 360	0 460	0 530	0.570	0.510	0.330	0.210	0.360	0.420	0.790	1.050	1.370	1.050	0.730	0.850
	12	208	2216	2296	591	249	328	431	107	68	64	878	1449	4070	4446	1436	5213	5607
20 00	2 002	1 600	11 420	6 001	1 523	2 7 4 2	2 338	1 5/3	5 730	4 362	2 4 2 8	-6.501	-30.422	-12.988	13.416	0.420	2,187	2,162
-30.00	2.002	-1.090	-11.429	-0.094	4.525	2.742	2.550	1.040	0 300	0 300	0 000	0.390	0 970	0 480	0 730	0.820	0.730	0.550
	0.300	0.200	0.430	0.030	0.330	196	1/5	61	0.550	18	0.000	2033	2558	2723	4278	2787	1243	1615
10 00	2 420	4.32	2 2 2 2 4	2320	1 177	1 0 2 0	2 044	2 247	2 202	3 0 2 8	3 712	2000	0 573	_3 457	9 1 9 9	7 053	-5.582	-24.015
-40.00	2.428	1.121	-2.4/4	-4.440	-1.1//	1.020	2.044	2.547	0 220	0.220	0 240	0 240	0.075	0 470	0 480	0 580	0 500	0 720
	0.000	0.260	0.240	0.190	0.230	0.230	0.350	0.400	0.520	0.520	11	1661	1052	641	1012	2078	528	978
	0	220	534	362	40	146	2 4 2 0	2 420	2 0 4 7	0 5 5	11	2 0604	2 005	2 5 2 0	2 2 2 2 0	5 690	3 0/18	_1 352
-50.00	2.444	2.009	2.065	2.428	2.428	2.428	2.428	2.428	2.047	-0.566	-0.239	3.050	0.000	3.330	0.500	0 410	0 100	-1.552
	0.140	0.110	0.140	0.000	0.000	0.000	0.000	0.000	0.220	0.240	0.220	0.320	0.270	0.480	0.500	101	0.470	0.400
	42	40	15	0	1	4	3	3	22	33	11	15	30	2 2 2 5 5	2 109	2 (2 2	4 950	2 6 0 2
-60.00	3.734	2.774	2.201	2.428	2.428	4.188	4.029	2.581	2.428	2.428	-2.810	-3.423	1.990	2.395	3.140	3.033	4.850	3.602
	0.120	0.210	0.090	0.000	0.000	0.360	0.350	0.140	0.000	0.000	0.340	0.320	0.170	0.200	0.350	0.250	0.320	0.440
	93	40	15	0	0	6	484	484	0	0	15	3/8	366	40	109	211	155	22
-70.00	2.713	3.630	3.106	2.428	2.428	3.011	4.498	4.077	2.428	2.428	1.104	-2.741	-1.853	2.428	2.428	2.690	3.818	4.166
	0.340	0.180	0.360	0.000	0.000	0.600	0.730	0.660	0.000	0.000	0.470	0.760	0.570	0.000	0.000	0.230	0.220	0.220
	177	76	70	0	0	6	484	484	0	-0	15	378	366	0	0	46	269	231
-80.00	2.392	5.277	3.443	2.428	2.428	3.402	5.769	4.641	0.496	1.069	0.496	-4.826	0.305	8.626	6.735	2.336	1.486	18.393
	0.630	0.170	0.580	0.000	0.000	0.070	0.300	0.280	0.140	0.220	0.180	0.780	0.450	0.540	0.340	0.140	0.880	0.840
	127	73	65	0	4	16	28	43	51	36	58	987	1115	381	199	133	246	233

-180.00 -170.00 -160.00 -150.00 -140.00 -130.00 -120.00 -110.00 -100.00 -90.00 -80.00 -70.00 -60.00 -50.00 -40.00 -30.00 -20.00 -10.00 80.00 9.915 64.306 -38.678 -46.086 17.846 54.788 -41.452 -9.725 67.481 47.097 19.339 68.391 25.074 18.163 3.775 -18.507 70.546 -47.758 2.670 1.620 1.090 2.460 2.330 3.090 1.810 2.130 2.130 1.890 1.890 2.170 1.260 1.250 2.450 0.000 2.210 1.800 659 1555 567 331 270 1244 743 1071 421 211 220 242 343 0 197 251 107 461 15.938 5.523 44.391 -7.490 19.604 -11.890 -10.532 29.004 34.975 25.575 49.623 36.492 26.869 3.930 33.728 -6.609 -31.400 70.00 -6.615 2.220 2.220 2.720 2.500 2.550 2.420 2.560 1.880 2.440 2.610 2.590 2.370 2.530 2.380 2.300 2.340 2.550 2.520 274 933 2260 1739 2135 1171 308 201 331 593 712 398 1680 5993 7654 3187 2255 430 14.546 25.371 -0.286 -14.020 -22.094 -8.378 14.140 25.601 24.259 18.044 6.005 -3.632 -23.551 -20.227 -16.781 -15.799 60.00 -56.146 -44.327 1.560 1.100 1.350 1.370 1.480 1.340 1.490 1.360 1.720 2.360 2.470 1.840 1.780 1.190 1.570 1.520 1.930 1.940 993 1005 392 485 773 1345 5374 3960 2506 2039 2047 1251 438 402 10472 9901 8343 9997 6.675 9.440 -8.000 19.937 5.050 7.461 -33.273 -36.413 -52.986 -19.348 -1.198 3.498 50.00 -57.184 -55.226 -46.705 -23.338 -5.637 -34.347 1.370 2.590 1.430 1.050 1.510 1.810 1.270 1.050 1.120 1.230 1.640 1.690 1.290 2.600 1.810 1.720 2.570 1.330 328 505 694 689 8384 5554 2979 890 1411 1816 863 3733 5921 8192 8661 5258 3291 1391 10.412 25.985 -69.589 -16.317 55.575 -17.326 -56.965 -45.980 -41.465 -12.704 -6.770 -32.338 -15.611 23.246 40.00 -38.184 -29.156 -27.392 -15.941 1.180 0.920 0.820 1.290 2.680 1.250 1.040 0.780 1.030 1.240 1.610 2.540 2.160 1.710 1.260 1.350 1.460 1.590 464 2538 1758 375 285 480 746 4012 1092 705 53 11 64 5879 10644 9824 5566 2789 6.803 -20.046 -47.211 -26.574 -20.919 -2.489 -7.125 -15.489 5.214 -1.865 9.915 61.515 60.736 6.873 58.342 9,915 -4.302 -9.704 30.00 1.180 1.400 0.930 0.620 0.860 0.800 1.000 0.870 0.750 1.160 0.000 1.030 2.050 1.400 1.290 0.000 1.300 1.510 88 1 3206 6170 6563 4440 2477 1739 949 125 514 757 569 325 195 53 45 0 -6.979 -33.591 -10.300 -20.805 -20.018 -8.946 -13.113 -6.830 9.915 21.905 33.146 11.178 68.422 42.618 9.915 -1.525 -32.830 -34.077 20.00 0.860 0.980 0.920 0.710 0.840 0.750 0.710 1.140 1.300 1.550 0.000 0.530 0.590 1.270 1.520 1.330 0.710 0.000 2200 1446 1230 725 689 32 58 123 23 111 1550 3860 4244 63 123 84 0 0 -3.922 2.494 -17.675 -45.042 -36.665 63.599 -26.459 -56.394 -48.039 9.915 9.915 16.219 21.469 62.732 10.00 9.915 3.605 -27.476 -38.329 1.000 0.860 1.200 1.370 0.000 0.000 0.590 0.620 1.170 1.520 1.430 0.750 1.180 0.770 0.990 1.380 0.000 0.940 331 438 1638 1260 370 545 1286 3712 4986 5102 3756 14 51 43 0 0 6 0 11.289 -50.300 -50.988 9.915 9.915 9.915 9.915 9.915 16.327 12.240 14.179 17.020 15.980 -14.412 -23.960 -29.150 -7.049 9.759 0.00 1.040 0.750 0.950 0.960 0.910 1.320 1.030 0.650 0.780 0.930 1.030 1.150 0.000 0.000 0.000 0.000 0.760 0.000 235 358 1366 5193 4258 139 35 270 338 605 1743 0 0 0 0 0 14 34 -7.589 -19.708 -2.540 1.717 12.174 13.827 12.376 6.307 -12.509 8.754 -2.918 38.399 43.409 27.513 16.424 11.150 8.144 -10.00 47.010 0.850 0.780 0.820 0.760 0.650 0.890 0.700 0.640 1.020 0.510 0.860 0.990 1.040 1.130 1.000 1.090 0.860 0.740 44 473 436 4475 64 246 271 97 443 3077 3459 755 121 126 3083 2822 2597 6352 14.193 10.767 -1.499 13.915 9.915 7.618 60.948 45.469 29.096 20.286 11.728 2.021 -20.402 -22.768 16.829 -21.089 50.879 -20.00 44.489 0.550 0.670 0.000 0.590 0.600 1.430 1.720 0.900 0.760 1.030 1.040 1.150 1.040 0.810 1.530 0.700 0.770 0.840 320 329 4935 405 360 369 88 39 2371 4364 2326 120 119 1 6633 5595 2823 6684 9.915 10.834 9.915 11.030 27.651 26.529 18.689 9.845 -0.881 -11.472 -11.279 6.158 -30.00 -13.531 -8.316 1.464 10.774 33.871 34.970 0.980 0.850 0.700 1.260 0.800 0.530 0.000 0.000 0.190 0.350 1.300 0.600 0.440 0.830 1.020 0.890 0.880 1.020 234 158 45 2333 3905 2009 52 1 0 163 172 3283 301 408 410 341 150 4508 1.567 9.915 9.915 12.037 11.283 -2.744 9.915 9.915 9.915 9.915 15.046 15.613 17.052 12.828 6.307 -8.509 -6.917 -40.00 -0.608 0.000 0.250 0.220 0.670 0.1.20 0.590 0.620 0.700 0.470 0.000 0.900 0.000 0.000 0.000 0.000 0.570 0.790 1.420 66 66 392 49 0 0 1520 587 0 1 1 0 6 32 69 84 1125 1267 11.106 12.805 12.102 1.154 1.050 5.802 9.324 9.915 10.765 6.900 -0.599 -13.480 -13.972 0.137 -50.00 -7.518 9.915 9.915 7.971 0.560 0.490 0.520 0.720 0.450 0.310 0.290 0.290 0.340 0.250 0.340 0.450 0.000 0.640 1.200 0.000 0.000 0.300 115 55 15 13 1 41 75 66 63 50 52 497 540 72 518 0 4 69 5.869 7.134 8.508 9.915 9.915 9.915 6.235 -0.738 -17.564 -22.996 -4.479 8.240 10.596 9.915 9.915 9.915 9.746 7.463 -60.00 0.480 0.340 0.360 0.000 0.000 0.000 0.040 0.110 0.130 0.100 0.090 0.000 0.000 0.000 0.410 0.430 0.510 0.430 34 84 83 79 557 550 119 0 0 Δ 69 115 55 12 10 0 0 1 4.034 -4.904 -10.604 -4.411 3.844 9.915 9.915 9.776 8.015 -70.00 11.932 9.915 9.915 9.915 9.915 9.915 9.915 9.915 9.915 0.000 0.000 0.000 0.440 0.400 0.480 0.500 0.480 0.510 0.440 0.000 0.000 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80.00 90.00 100.00 110.00 120.00 130.00 140.00 150.00 160.00 170.00 40.00 50.00 60.00 70.00 10.00 20.00 30.00 0.00 2.345 30.376 -41.464 -56.627 -32.991 9.915 9.915 6.047 -2.461 -17.994 -17.487 23.452 80.00 -44.497 47.243 66.081 15.929 16.879 -3.471 2.540 0.000 0.000 1.590 1.500 2.440 1.820 1.320 1.100 1.750 2.420 1.350 2.290 2.520 2.390 2.250 1.240 2.150 0 133 162 174 341 324 157 35 4 167 66 47 75 90 111 420 249 790 10.133 -21.368 -48.809 -46.644 -20.634 9.915 18.669 15.596 10.477 -0.965 -7.821 -3.352 32.248 23.016 20.532 70.00 -4.638 -30.262 0.974 2.130 2.730 2.670 2.080 2.540 2.820 0.000 2.560 2.310 2.200 2.630 2.460 2.480 2.310 2.510 2.460 2.370 2.440 571 287 34 131 415 88 91 403 8 2 9 41 102 3617 2300 1355 1367 2652 3.475 -9.081 -18.508 -43.261 -59.131 -61.615 60.00 17.515 13.204 -50.691 -47.140 5.579 19.409 27.193 27.544 31.793 38.361 35.797 20.030 1.570 1.760 1.480 1.630 1.540 2.240 1.620 1.540 1.630 1.440 1.440 1.720 2.510 1.530 1.730 1.850 1.840 2.580 4799 1107 583 553 3030 5434 607 588 553 268 533 1007 1384 10215 14831 13266 5661 2247 6.323 -25.456 -47.278 -48.209 -64.105 18.013 21.990 28.715 42.114 55.256 68.711 70.000 43.897 64.692 35.115 -53.630 -12.539 50.00 40.687 2.430 2.160 1.400 1.900 2.500 1.870 1.800 1.510 1.760 2.490 1.780 1.910 1.160 1.540 1.640 1.810 2.540 2.710 5357 6299 2741 2509 1247 2001 2640 1942 2126 2425 3200 3100 16240 23484 11234 31775 17969 26766 16.488 -31.754 -28.803 -24.083 -21.186 -6.179 50.095 60.469 55.129 54.798 45.177 -25.572 14.377 27.747 -12.463 40.00 68.900 -57.752 -66.482 1.940 2.000 1.580 2.800 2.350 1.150 1,280 1.980 2.210 2.170 1.730 2.120 1.270 2.230 1.480 1.840 2.010 1.550 5512 7272 6821 8490 23627 25548 6968 584 2871 3489 2959 6399 7035 3548 10212 4071 19697 22306 32.123 -27.322 -43.145 -55.729 -42.426 -18.848 -3.551 9.915 30.00 22.884 -33.581 -59.925 -52.101 -40.935 -47.384 -10.994 -27.792 -52.736 -64.218 1.210 1.380 1.300 2.550 1.860 2.740 2.420 2.460 2.130 1.310 1.340 0.000 1.040 1.430 0.570 0.560 0.950 1.120 0 10144 6211 7 3787 6416 7579 6918 9249 9237 10775 11388 1345 2505 357 658 1248 1394 0.822 9.915 -31.971 -53.212 -55.176 -37.288 -24.059 -8.358 -43.971 -44.845 37.173 -51.620 -54.083 -54.821 -22.717 9.915 1.514 6.436 20.00 2.170 1.200 0.950 1.230 0.850 0.000 0.980 1.570 1.530 1.790 1.720 0.000 0.600 0.740 0.970 0.880 1.000 0.500 3416 57 0 4505 6898 6751 4749 8555 7752 4340 79 1 28 287 722 1827 2120 2787 4.403 -25.804 -43.121 -41.894 -25.346 -34.215 -46.511 -59.890 -47.646 2.559 9.915 6.947 3.013 7.050 19.541 10.00 -2.442 -12.736 -20.209 1.560 1.370 1.670 0.810 0.000 1.130 1.150 0.920 1.920 0.590 1.000 0.990 1.150 1.060 0.890 1.390 1.030 0.530 7375 3216 2774 212 0 324 603 884 1063 671 1659 1737 3977 5823 3989 7964 1298 252 26.408 30.037 24.791 -18.949 -20.576 -19.371 -53.121 -40.431 -11.055 -45.793 -12.608 29.212 21.171 47.233 0.00 -29.743 -10.509 -35.119 20.542 1.310 0.930 0.800 0.950 1.310 2.030 1.470 0.660 0.950 0.930 1.120 1.150 1.100 0.800 1.020 1.400 0.820 0.600 5152 9448 10057 6306 8014 5006 204 861 242 314 286 257 2805 5861 542 1143 1248 256 -1.340 -4.153 -40.668 -40.697 -56.256 -54.866 -19.933 65.161 67.348 25.615 28.259 36.269 7.779 -10.00 -12.472 9.915 9.479 12.119 17.570 1.300 1.200 0.850 0.770 0.900 0.940 1.120 2.040 1.660 1.410 1.820 1.050 0.540 0.000 0.570 0.840 0.890 1.080 7302 7685 8208 9736 5318 331 704 2095 2916 4972 13 349 934 817 247 456 607 1 11.722 70.038 1.965 11.589 30.320 15.288 7.776 17.964 21.230 18.268 7.036 2.032 -24.798 -55.101 -8.845 -55.492 -31.279 -20.00 4.398 2.420 1.700 0.980 1.630 1.380 0.960 0.690 0.870 0.590 1.200 1.770 0.690 0.720 0.960 1.290 0.510 0.560 0.640 1823 6176 6287 64 954 1671 4228 4553 203 2137 2242 730 252 332 426 124 66 13 9.233 16.112 -39.195 -21.915 20.299 -42.754 -5.388 10.008 0.727 -14.631 -10.191 11.790 8.754 13.998 13.669 9.915 -1.428 -30.00 7,997 1.410 1.520 0.890 0.940 0.000 0.770 1.780 0.610 0.580 0.720 0.930 1.010 0.950 0.670 0.540 0.420 0.850 1.230 191 65 55 24 0 1973 2557 2948 4146 2924 1364 1856 415 2529 2302 377 153 13 9.122 11.717 -16.850 -45.021 8.683 7.633 11.343 10.878 12.129 10.641 5.974 -2.888 12.309 9.915 7.269 0.558 -3.586 1.824 -40.00 0.610 0.400 0.390 0.360 0.540 0.530 0.620 0.690 0.560 0.660 0.790 0.590 0.830 0.750 0.780 0.940 1.420 0.000 1910 19 54 50 11 1507 1808 857 1857 398 1089 207 592 430 56 146 115 0 12.168 10.661 10.186 10.735 9.917 9.366 -0.149 -50.00 10.036 9.369 9.232 9.915 9.915 10.032 9.882 8.638 8.735 3.802 4.300 0.400 0.730 0.570 0.890 0.860 σ.710 0.830 0.790 0.300 0.000 0.000 0.440 0.330 0.440 0.450 0.380 0.200 0.230 55 114 184 253 652 6 23 28 11 15 30 3 10 6 41 43 19 1 11.962 13.531 11.895 9.915 9.915 14.061 14.525 12.281 9.778 9.915 -0.522 -1.928 8.711 9.366 10.758 10.403 9.660 -60.00 11.592 0.600 0.370 0.430 0.730 0.440 0.860 0.000 0.000 0.450 0.250 0.490 0.230 0.000 0.640 0.580 0.230 0.360 0.160 36 208 150 30 363 107 49 21 0 0 44 484 483 27 0 21 378 120 10.775 13.256 13.227 14.844 12.661 9.915 7.218 -0.181 1.288 9.915 9.915 -70.00 8.118 10.860 10.669 9.915 9.915 11.236 14.673 0.000 0.000 0.480 0.420 0.390 0.800 0.740 0.470 0.870 0.000 0.900 1.360 1.060 0.540 0.310 0.580 0.000 0.000 484 483 32 0 22 378 363 0 0 56 267 226 82 53 0 0 54 181 16.060 8.113 22.969 18.697 12.956 15.434 44.252 17.455 10.097 6.955 3.385 -3.544 -80.00 10.411 15.484 12.497 9.915 9.915 12.165 1.400 0.560 0.330 0.920 1.210 1.350 0.360 1.210 0.000 0.000 0.100 0.600 0.590 0.230 0.670 0.240 1.390 1.060 220 370 333 1039 630 215 78 46 0 4 16 30 54 47 40 56 802 99

Depth = 290 km

-180.00 -170.00 -160.00 -150.00 -140.00 -130.00 -120.00 -110.00 -100.00 -90.00 -80.00 -70.00 -60.00 -50.00 -40.00 -30.00 -20.00 -10.00 69.241 80.00 68.384 16.138 -55.297 -29.041 20.207 22.212 -42.761 14.318 45.343 29.919 43.060 2.117 -21.739 -26.193 71.867 31.655 4.326 2.060 2.610 2.160 1.390 1.330 1.250 1.370 1.190 1.480 2.360 2.250 1.400 1.710 1.580 1.150 1.790 1.570 2.370 1424 1265 362 453 626 315 304 371 347 107 737 778 1060 416 283 13 191 238 29.269 16.633 9.020 -4.863 -9.89438.903 40.950 -20.321 -24.794 -4.048 6.053 -19.755 -4.393 16.775 20.968 29.844 70.00 50.980 62.344 1.590 1.660 1.820 1.740 1.830 1.930 1.300 1.820 1.710 1.890 1.550 1.780 1.550 2.030 1.800 1.910 1.720 2.060 435 532 943 2143 1882 173 358 661 588 6336 2920 2039 1825 852 362 451 2253 5485 12.804 -6.592 -22.429 -21.397 -13.943 5.255 14.911 17.150 11.055 1.619 -5.208 -6.492 -17.442 -16.459 60.00 -4.498 23.259 51.331 17.294 1.190 1.520 1.420 1.400 1.210 1.490 1.380 1.540 1.320 1.320 1.230 1.340 1.390 1.360 2.070 1.960 1.630 1.700 535 768 1821 4987 2236 1862 1387 573 524 1072 827 432 10525 9398 3686 2511 10161 7830 -0.797 2.396 4.020 -2.068 -5.758 1.894 -35.700 -36.010 -52.480 -22.056 11.357 1.808 4.017 3.698 -17.455 16.125 50.00 -21.210 -21.557 0.850 1.010 1.230 1.180 1.030 1.020 1.860 1.580 1.200 1.480 1.830 2.000 1.720 1.360 1.450 1.710 1.320 1.090 1752 916 381 465 711 1225 8439 3182 1179 1376 3803 1808 4028 6018 5154 8213 8768 5818 -5.752 -23.545 -14.502 -11.998 13.817 20.331 44.468 -16.536 -55.940 -10.040 -33.728 -4.541 -7.310 -2.621 7.426 27.482 -64.823 40.00 3.819 1.330 2.350 1.040 1.090 0.750 1.120 1.060 0.750 0.770 0.910 1.000 1.640 2.030 2.020 1.480 0.860 1.200 0.880 458 298 533 736 539 4324 2542 1861 5891 10622 9376 5874 3149 1349 774 150 78 278 -7.029 -31.967 -43.778 -10.088 -17.818 -6.024 -6.880 -15.899 3.440 58.830 28.165 -32.701 45.456 -3.586 1.000 15.412 30.00 8.604 1.099 0.660 0.990 0.640 1.050 0.830 0.610 0.970 1.620 1.450 1.360 1.100 1.610 0.740 0.000 0.690 0.830 0.990 0.700 542 777 516 331 299 254 2 50 92 41 82 3122 6316 6462 4688 2674 1983 1199 -8.845 -38.674 -9.937 -16.064 -20.165 -11.740 -10.014 -4.195 8.604 19.628 -14.260 54.117 31.177 -4.974 -23.634 -21.233 19,289 20.00 8.604 0.610 0.640 0.820 0.690 0.740 0.620 0.510 1.190 1.600 1.210 0.800 0.790 0.000 0.830 0.750 1.250 0.000 0.610 792 766 115 49 131 112 378 1926 4340 4668 2605 1543 1247 67 123 62 0 2 -0.485 1.896 -17.410 -46.852 -22.767 60.733 -10.075 -50.420 -43.775 10.421 6.473 50.552 1.885 -30.841 -41.979 8.604 8.604 10.00 8.604 0.510 0.680 1.290 1.310 0.790 0.960 0.760 0.580 0.520 0.790 1.030 0.000 0.000 0.610 0.660 1.180 1.370 0.000 5019 5080 3645 1273 489 544 342 679 1687 74 1311 3736 21 48 31 0 0 0 8.785 9.527 -20.305 -13.499 -23.285 -4.524 8.167 -49.540 -53.501 9.030 7.801 8.604 8.604 8,604 8.604 8.604 14.286 9.811 0.00 0.860 0.840 1.050 1.200 0.940 0.720 0.640 0.640 0.650 0.770 1.220 0.000 0.000 0.000 0.650 0.710 0.000 0.000 200 43 276 349 801 1756 5122 4230 0 44 64 234 381 1463 0 0 0 0 10.555 5.511 -14.277 36.815 25.228 14.124 8.626 3.326 -18.962 -29.845 -31.152 -7.903 8.427 11.197 -10.00 26.813 0.673 -2.500 43.440 0.450 0.540 0.560 0.990 0.620 0.470 0.590 0.850 0.880 1.020 0.820 1.010 0.570 1.010 0.480 0.770 1.110 0.760 427 3462 773 120 111 27 430 3410 6299 3933 74 244 264 88 517 3182 3752 3350 -6.873 -43.933 -52.398 -31.779 4.126 10.718 8.604 9.068 4.488 8.174 57.742 40.287 25.877 17.209 1.444 -31.524 66.804 -20.00 8.393 0.950 0.780 0.630 0.000 0.430 0.460 0.980 0.770 1.390 1.730 1.500 0.760 0.630 0.760 0.810 1.010 0.920 0.800 2554 4370 2277 120 103 2 316 334 4347 384 345 365 83 98 3670 6741 7145 6078 -4.888 7.136 8.604 9.696 9.131 4.705 -13.014 -31.375 -34.630 31.355 24.472 22.519 15.648 -30.00 -36.704 -12.530 -0.657 10.044 39.717 0.000 0.330 0.380 0.810 0.830 0.840 0.880 0.780 0.700 1.130 0.840 0.850 0.680 1.360 0.940 0.350 0.750 0.930 159 173 3964 2032 70 15 0 319 151 231 151 54 2311 3447 467 630 401 4726 -6.665 8.604 10.604 9.983 1.706 -14.751 -15.871 8.604 -2.786 8.604 8.604 8.604 12.920 13.498 14.400 10.061 -40.00 -31.110 -16.068 0.620 0.700 0.590 0.000 0.000 0.170 0.290 0.590 0.800 0.580 0.700 0.560 0.590 0.630 0.000 0.000 0.000 0.940 68 1043 1270 462 49 0 4 69 8 35 69 87 1530 565 12 2 2 2.221 4.648 8.092 8.604 9.208 5.770 -1.429 -13.589 -16.213 -5.120 9.005 11.712 10.614 8.604 2.603 0.488 1.218 -50.00 -23.367 0.250 0.600 0.510 0.480 0.540 0.720 0.440 0.310 0.270 0.380 0.450 0.000 0.560 0.580 0.580 0.510 1.110 0.000 538 100 61 54 69 499 6 71 113 59 15 12 1 41 89 79 376 0 -0.476 -15.029 -21.602 -7.117 5.701 8.983 9.878 7.482 5.240 4.765 6.185 7.292 8.604 8.504 8.604 5.613 -60.00 8.604 8.604 0.340 0.370 0.450 0.490 0.480 0.370 0.310 0.130 0.000 0.000 0.000 0.000 0.000 0.060 0.200 0.220 0.180 0.180 38 81 90 93 564 551 171 71 113 55 12 7 0 0 3 0 0 6 -9.701 -5.287 2.237 8.604 8.528 7.105 3.714 -3.980 8.604 8.604 8.604 8.604 8.604 8.604 -70.00 10.503 8.604 8.604 8.604 0.400 0.420 0.440 0.400 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.310 0.310 0.360 0.430 0.000 0.000 0.000 93 96 167 10 26 34 25 0 0 0 0 2 17 0 0 0 0 0 8.604 8.604 8.604 8.604 8.604 8.604 13.391 -80.00 11.602 6.472 6.900 8.604 8.604 8.604 8.604 8.604 8.604 8.604 8.604 0.000 0.000 0.000 0.000 0.000 0.530 0.000 0.000 0.000 0.000 0.000 0.480 0.440 0.000 0.000 0.000 0.000 0.710 0 0 0 0 0 0 60 0 0 0 0 133 81 12 0 0 0 0

	0.00	10.00	20.00	30.00	40.00	50.00	60.00	70.00	80.00	90.00	100.00	110.00	120.00	130.00	140.00	150.00	160.00	170.00
80 00	-59.761	-15.170	63.633	17.061	23.092	10.006	-23.286	2.047	11.824	-0.533	3.875	24.273	64.826	22.564	-5.893	-2.006	38.638	68.622
00.00	2 280	1 410	1 610	1 510	2.330	1.670	1.090	1,160	1.720	2.200	0,960	2.390	2.790	1.510	2.130	1.530	2.140	1.370
	1005	501	3/1	253	2.330	79	94	139	159	131	123	161	200	222	142	87	37	11
70 00	1005	22 109	22 241	10 272	15 569	10 326	15 886	_0 741	2 960	8,918	5.033	4.146	12,607	39.420	28.853	10,916	3,980	21.606
/0.00	50./1/	-22.108	-23.34I	1 7 2 0	1 670	1 070	1 750	1 790	1 650	2 010	1 490	1.830	1.820	1.800	1.690	1,860	1.670	1,950
	1.860	2.000	1.580	1./30	1.070	1.970	1.750	1.750	1.050	116	110	135	289	380	198	82	138	436
	18/3	2914	2946	2905	1003	209	10 (01	4 /	16 166	17 270	10 772	9 046	0 500	-6 529	7 913	17 987	8.431	-4.732
60.00	3.986	33.401	-38.394	-49.895	-9.725	9.544	18.091	1 460	1 700	1 420	1 720	1 420	1 370	1 410	1 350	1 410	0.970	1.090
	1.390	1.630	2.370	2.000	1.570	1.520	1.320	1.460	1.780	1.430	1.720	1.420	1151	1.410	1.550	2030	1906	5400
	11955	18290	14306	7350	2736	/83	605	560	369	524	809	1292	L L L L	26 940	42 944	22 102	28 781	-8 348
50.00	41.482	48.583	60.179	-48.071	-19.677	/ . 4 / /	10.519	17.093	26.482	25.756	40.244	46.102	0.914	-20.049	-42.044	-22.192	1 640	1 150
	2.170	2.570	2.370	1.680	1.710	1.370	0.900	1.970	1.490	1.570	1.890	1.690	1./50	1.450	1.350	2.220	11526	5625
	25338	31358	20117	8349	3345	2563	1740	2285	2536	2176	2270	2554	31/4	3418	1/350	24087	11520	16 122
40.00	63.591	-32.422	-67.354	57.287	-16.270	-2.344	12.879	-20.764	-3.104	36.788	40.439	18.521	-1.076	-27.698	-46.534	-34.035	-0./4/	16.123
	1.340	1.760	2.300	2.710	1.610	1.870	1.560	2.270	1.410	1.690	1.910	1.660	1.850	1.890	2.500	1.890	0.980	0.790
	17158	19982	11008	4871	3354	3619	4580	6415	6878	4227	5607	7248	7037	9570	25310	26098	7462	1116
30.00	14.448	-21.102	-49.952	-47.208	-35.804	-47.942	-34.723	-45.133	-42.756	-62.343	37.533	-18.915	-32.899	-56.769	-33.184	-19.769	-3.333	8.604
	0.550	0.620	0.760	1.200	1.150	1.260	0.970	1.660	1.490	2.420	1.730	2.540	1.920	2.210	1.890	0.850	0.780	0.000
	611	834	1308	1434	1579	2470	4656	6147	7399	7279	9668	9208	11885	13018	11597	6405	58	0
20.00	3.469	-9.698	-21.568	-39.351	-54.196	-21.100	-26.601	-12.157	-31.107	-38.366	8.274	41.509	-28.805	-42.537	-53.007	-13.855	-0.335	8.604
	0.570	0.590	0.510	0.560	0.760	0.730	0.750	0.920	1.500	1.810	1.560	1.420	1.930	1.190	1.100	1.230	0.770	0.000
	133	29	102	296	713	1800	1983	2080	4328	6952	7273	5359	9246	8427	4625	3338	138	0
10.00	1,955	-13,204	-20.321	11.765	7.564	5.840	19.540	5.019	-11.574	-25.644	-34.490	-15.128	-12.327	-28.304	-45.678	-49.556	-6.674	8.604
	0.820	0.620	0.600	0.740	0.790	0.920	0.760	0.850	1.290	1.220	1.140	0.860	1.640	1.500	1.170	1.330	0.820	0.000
	1309	205	339	683	938	1064	672	1123	1710	4147	6018	4245	8247	7780	3422	2814	348	0
0.00	-34.017	-13,181	-29.541	18,504	43.795	22.527	25.489	23.154	-14.505	-15.001	-9.233	-55.589	-39.287	-35.519	-26.284	-13.726	0.007	13.710
0000	0.650	0.580	0.620	0.790	0.830	0.870	0.790	0.820	0.890	1.020	1.330	0.990	1.180	1.910	1.130	1.190	0.780	0.800
	1253	208	545	1162	870	276	320	298	313	2761	5830	5188	9494	10282	6657	8386	5487	428
-10.00	-18,198	-5.082	4.113	12,119	13.739	22.134	23.399	31.283	8.744	1.684	6.639	-38.441	-36.949	-47.556	-56.416	-22.843	33.203	16.239
10:00	0 610	0.590	0.570	0.760	0.830	1.090	1.130	0.930	0.720	0.880	0.850	0.980	1.140	2.020	1.600	1.330	1.690	1.030
	66	12	356	887	810	274	451	606	345	667	2159	3030	5121	7657	7924	8452	10085	5488
_20_00	1 862	-0 106	5.448	20.446	11.610	5.325	15,193	17.462	15.666	6.690	4.953	-11.629	-47.820	-1.956	-40.805	-49.781	-42.422	38.895
20:00	0 450	0 510	0.560	0.610	0.730	1.000	1,250	1.230	0.780	0.710	0.940	0.640	1.030	1.550	2.090	1.400	0.870	1.480
	12	191	1971	2220	862	219	341	419	139	65	79	1050	1925	4472	4969	2547	6317	6348
30 00	6 146	_0 071	_8 122	-11 586	7 931	6.649	6.606	11,912	13,688	11.836	8.604	2.646	-13.408	-21.799	19.999	-53.869	-59.133	-47.880
-30.00	0.140	0.360	0.780	1 030	0 500	0 620	0 910	1,110	1.020	0.590	0.000	0,660	1.590	0.840	1.500	1.410	1.160	1.080
	1.400	0.300	2110	2220	5/6	18/	156	68	60	33	1	1786	2509	3070	4130	3285	1585	2038
40.00	0 604	6 007	0 251	2 5 2 2	0 765	7 5 9 1	5 501	7 356	9 592	9.124	10.017	7.891	5.411	-3.578	-2.583	-2.105	-48.202	-63.980
-40.00	0.004	0.007	0.331	-2.575	0.705	0 390	0 480	0 690	0 700	0.840	0.770	0.450	0.740	0.780	0.800	0.820	0.690	1.400
	0.000	0.300	0.410	0.310	0.470	1/5	120	25	54	A7	11	1235	1650	946	1838	1790	440	1124
F 0 0 0	1	203	7 5 2 5	532	0 0 0 0	0 611	0 612	7 174	7 368	3 258	2 252	8 653	7.780	7.958	6,218	4.824	3.835	-8,786
-50.00	8.689	8.128	1.525	0.0/9	0.004	0.044	0.013	0 240	7.500	0 420	0 470	0.580	0 450	0 780	0 860	0.670	0.750	0.870
	0.210	0.260	0.320	0.280	0.000	0.390	0.330	0.340	0.440	0.420	0.470	10	30	57	116	199	283	516
	44	45	24	0.001	4	13	10 120	10 025	0 450	2 4	0 176	1 0 1 7	7 200	7 699	8 794	0 033	10 474	10 200
-60.00	9.816	9.002	8.4/6	8.604	8.604	12.088	12.430	10.835	8.400	0.004	-0.176	-1.017	7.200	7.000	0.754	0 270	0 5/0	0 790
	0.230	0.270	0.140	0.000	0.000	0.370	0.190	0.410	0.190	0.000	0.490	0.400	0.310	0.370	0.010	102	146	0.790
	134	59	23	0	1	74	484	466	87	0	28	3/8	361	30	104	192	11 7 7 7	11 220
-70.00	6.433	8.924	9.089	8.604	8.604	9.822	12.580	12.678	11.015	8.604	6.524	0.598	1.232	8.604	8.604	9.294	11./3/	11.330
	0.410	0.260	0.410	0.000	0.000	0.630	0.570	0.360	0.700	0.000	0.730	0.900	0.810	0.000	0.000	0.410	0.340	0.350
	183	88	48	1	1	75	484	468	92	0	28	378	359	0	1	60	255	213
-80.00	9.224	12.750	11.032	8.604	7.960	10.920	15.210	13.471	8.695	6.262	3.538	-0.329	10.457	21.329	16.561	13.345	13.312	45.206
	1.320	0.180	0.650	0.000	0.650	0.820	0.370	0.650	0.170	0.750	0.150	1.050	1.350	1.460	0.510	0.510	0.620	1.230
	89	70	40	1	7	26	55	63	43	32	35	520	1013	646	112	203	411	353

Depth = 410 km

-180.00 -170.00 -160.00 -150.00 -140.00 -130.00 -120.00 -110.00 -100.00 -90.00 -80.00 -70.00 -60.00 -50.00 -40.00 -30.00 -20.00 -10.00 -4.388 -6.751 -19.906 -30.053 11.872 29.638 70.837 80.00 44.220 -11.019 -50.016 -1.552 13.360 -17.517 -22.318 13.126 15.133 26.016 22.007 1.470 1.940 2.100 0.720 1.020 1.070 2.620 0.830 0.780 1.020 1.570 0.580 0.760 1.150 1.450 1.010 1.040 0.980 317 315 485 576 744 1291 1472 833 514 475 540 339 365 600 839 58 150 175 6.037 -0.215 -9.787 -17.525 -1.717 11.804 16.387 -7.632 -15.487 -2.832 4.167 12.952 17.995 -16.035 -7.256 2.521 70.00 39.489 43.316 1.230 1.160 1.240 1.650 1.390 1.090 1.110 1.420 1.350 1.310 1.240 1.300 1.030 1.130 1.100 1.330 1.300 1.340 496 616 684 953 1623 2195 1272 654 452 199 437 666 5357 2905 1980 3392 5507 788 5.903 1.827 -2.466 -9.144 -4.755 -3.707 -15.107 -13.390 -11.776 -0.129 9.452 -0.298 47.048 30.722 13.538 2.398 60.00 4.887 33.689 1.100 1.210 1.340 1.370 1.030 0.780 1.040 0.920 1.030 1.090 1.130 1.110 1.060 0.980 1.030 1.420 1.240 0.940 1826 5172 1140 798 490 562 667 584 667 3861 3000 2620 1678 1364 7902 11277 10947 8330 1.793 -38.354 -14.957 -0.835 0.134 -1.508 -8.433 22.472 30.607 22.802 0.531 -20.472 -21.988 33.393 51.237 42.047 50.00 -23.727 0.014 0.570 0.680 0.900 0.590 0.870 0.930 0.900 0.880 0.830 1.160 0.950 1.070 0.970 1.130 0.950 0.920 0.850 1.240 1927 8770 839 433 474 712 1599 8959 6303 3924 2395 4687 6328 4579 3349 1493 1455 8339 25.546 -18.633 -36.543 3.857 -23.138 -11.990 -7.276 -12.161 -9.740 4.283 48.142 -16.875 54.325 8.705 23.189 36.204 -1.222 40.00 3.399 0.700 0.510 0.780 0.880 0.570 0.750 0.920 0.830 1.250 1.150 0.920 0.910 1.220 0.850 0.900 0.750 0.800 1.250 388 622 721 1084 5100 10618 8654 5860 3395 2569 1756 516 357 275 1164 5946 1431 825 -4.486 -14.076 -12.922 -8.547 -13.128 1.725 -4.953 -35.427 -22.687 3.211 40.530 3.077 7.090 17.567 43.306 41.965 30.00 3.563 2.753 0.760 0.700 0.520 1.180 0.590 0.550 0.830 0.560 0.750 0.720 0.640 0.950 1.010 0.830 1.060 0.910 0.650 0.000 2176 1388 524 666 827 506 309 514 4981 3194 87 42 629 3087 6512 6370 48 4 -7.209 -0.778 -8.895 -11.145 -18.235 -13.898 23.606 -4.140 -29.585 3.563 -6.164 -13.098 -7.026 3.563 10.187 10.159 4.643 47.919 20.00 1.250 0.890 0.710 0.490 0.530 0.490 0.580 0.520 0.590 0.580 0.000 0.490 0.620 0.690 0.720 0.650 0.000 0.520 936 757 221 76 264 1649 1266 253 743 2227 4738 5334 3181 4 71 123 60 0 -6.523 -0.747 -14.487 -43.023 3.563 1.345 0.437 32.552 47.884 4.413 -27.483 -30.432 -0.166 -3.124 -30.327 -40.326 3.563 3.563 10.00 0.680 0.560 0.450 0.410 0.820 0.630 0.720 0.400 0.610 0.810 0.980 0.930 0.700 0.000 0.000 0.000 0.440 0.740 527 364 1065 1685 1297 618 40 21 0 0 132 1220 3727 5277 5330 3536 23 1 2.447 -12.380 -4.052 -11.539 -3.751 4.105 2.089 -41.872 -52.061 -1.131 -6.278 3.563 7.450 3.792 1.893 0.179 -0.950 0.00 3.563 0.490 0.890 0.780 0.740 0.790 0.680 0.440 0.650 0.750 0.820 0.400 0.460 0.550 0.000 0.300 0.440 0.600 0.000 1601 5031 4126 244 40 259 335 1151 1741 49 91 237 490 6 4 0 5 11 -9.536 3.460 4.866 4.800 1.231 -13.128 -2.401 -22.957 -24.110 -31.063 15.187 6.898 2.936 -10.00 -2.955 5.122 10.634 26.970 18.541 0.620 0.710 0.630 0.470 0.410 0.360 0.410 0.430 0.480 0.580 0.510 0.760 0.660 0.530 0.760 0.410 0.790 0.710 763 116 70 33 336 476 584 3377 3637 89 242 251 129 3860 3831 6148 3096 4613 2.323 -10.511 -47.279 -54.348 -30.959 -1.668 4.318 3.563 3.668 -0.256 -20.00 -30.573 -13.890 22.503 61.268 35.507 24.394 14.361 9.251 0.430 0.880 0.620 0.590 0.450 0.000 0.340 0.350 0.580 0.500 0.510 0.440 0.390 0.970 0.860 0.540 0.920 1.010 4475 126 62 4 285 321 239 2749 2135 327 347 92 8415 6827 4192 6732 3477 285 2.565 4.572 3.563 3.496 18.549 7.917 -0.587 -13.782 -21.116 -28.831 -7.559 2.998 21.193 30.231 13.851 11.676 -30.00 -26.668 -17.157 0.000 0.330 0.320 0.470 0.380 0.440 0.650 0.480 0.650 0.330 0.500 0.580 0.470 0.460 0.450 0.560 1.080 0.780 0 150 168 2180 3964 1953 69 16 559 761 403 245 162 234 153 174 3565 5165 6.615 -2.225 -10.326 -12.154 -7.664 3.563 5.438 5.430 4.799 6.654 3.708 -3.971 3.563 3.563 3.563 6.241 -9.083 -40.00 -4.309 0.290 0.320 0.230 0.440 0.440 0.360 0.460 0.000 0.400 0.650 0.590 0.550 0.000 0.000 0.000 0.430 0.500 0.390 123 864 1267 487 34 0 -5 69 67 13 40 78 1475 517 29 4 1 1 -6.777 3.428 6.623 5.473 3.581 1.744 -2.207 -8.713 -11.365 0.810 3.291 3.855 -50.00 -13.199 3.563 0.266 -1.104 -2.148 -1.296 0.350 0.300 0.270 0.280 0.490 0.310 0.360 0.290 0.320 0.340 0.470 0.400 0.380 0.000 0.520 0.520 0.440 0.890 488 501 196 11 44 104 98 71 67 111 15 9 31 75 111 55 201 4 -8.949 -13.401 -6.169 1.228 4.478 1.853 -1.259 4.062 1.035 0.941 1.941 2.661 3.563 3.563 3.137 3.563 2.632 -60.00 3.563 0.280 0.290 0.420 0.350 0.360 0.380 0.370 0.280 0.000 0.000 0.000 0.060 0.200 0.210 0.140 0.170 0.100 0.000 9 43 80 98 134 550 563 290 0 32 75 111 54 12 6 1 3.563 3.563 3.366 2.674 0.970 -3.045 -6.255 -4.120 -0.090 3.563 3.563 3.563 3.563 3.563 3.563 3.563 3.563 -70.00 4.194 0.280 0.420 0.340 0.380 0.420 0.360 0.000 0.000 0.390 0.000 0.000 0.000 0.000 0.000 0.260 0.000 0.000 0.000 24 24 23 88 138 188 0 0 0 1 4 11 31 0 0 0 0 0 3.563 7.381 6.568 3.563 3.563 3.563 3.563 3.563 3.563 3.563 3.563 3.563 3.726 2.987 3.563 3.563 3.563 -80.00 8.320 0.240 0.550 0.000 0.000 0.000 0.000 0.000 0.370 0.280 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.390 0 0 0 0 0 1 2 5 59 0 0 98 27 0 0 0 0 153

	0.00	10.00	20.00	30.00	40.00	50.00	60.00	70.00	80.00	90.00	100.00	110.00	120.00	130.00	140.00	150.00	160.00	170.00
80 00	-37 382	-51 553	22 205	10.043	3.796	-23,155	-4.116	8.996	10.650	6.576	-1.828	14.943	33.865	5.822	3.149	10.129	35.332	55.281
00.00	1 240	1 450	1 460	1 670	1 900	1 370	0.710	0.780	1.040	0.640	1.190	0.990	2.400	1.130	1.320	0.840	0.840	1.050
	1120	1.400	1.400 E27	1.070	1.000	256	147	150	126	144	129	143	153	149	101	94	77	53
70 00	1128	6 1 0 7	27 526	405 E 026	0 644	2 1 1 9	9 3 9 7	_5 225	2 130	6 481	6 708	2.338	7.543	18,680	11.260	6.770	7.929	21.819
/0.00	52.698	6.193	-2/.520	-5.020	1 200	2.447	1 260	1 220	1 070	1 250	1 040	1 190	1 180	1.470	1.230	1.290	1,190	1.210
	1.540	1.420	1.410	1.430	1.300	1.370	1.300	1.230	1.070	122	1.040	100	289	342	168	112	193	467
	2532	3195	3011	333/	1869	1005	208	1 0 2 0	/0	1 2 2 5 2	0 0 2 7	C 165	0 405	3 / 99	1 1 4 1	6 142	4.198	-0.394
60.00	-7.972	19.626	-3.078	-42.171	-20.514	-2.3/8	3.329	1.929	-0.115	3.850	1 550	1 000	1 210	- 3.400	1 290	0 980	1 060	0.850
	1.440	1.510	1.540	1.150	1.400	1.160	1.130	1.140	1.330	1.150	1.550	1105	1105	1.1/0	1.290	2512	5288	5185
	13156	19655	15045	9549	3738	1619	834	562	631	589	619	1185	1100	17 560	22 226	10 907	14 256	5 080
50.00	37.361	17.856	34.937	-1.660	-14.663	-3.145	2.941	7.186	7.529	3.506	13.134	20.312	2.080	-1/.560	-22.330	-10.807	1 220	-3.080
	1.490	2.100	1.720	1.270	0.930	1.080	0.860	1.360	1.140	0.800	0.840	1.190	1.310	0.850	1.030	1.000	1.000	0.070 E021
	23195	29252	22498	11224	4656	2668	2320	2253	2586	2261	2235	2825	3040	4237	184/1	24191	12003	11 242
40.00	45.185	10.184	-58.123	37.939	7.003	-11.398	-3.148	-3.387	7.654	20.002	29.111	10.293	-14.737	-18.124	-19.514	5.616	10.394	11.243
	0.940	1.240	1.640	1.980	0.980	1.090	1.250	1.310	1.000	1.060	1.340	1.070	1.310	1.630	1.650	1.340	1.130	0.820
	14632	16465	11471	5687	3904	3808	5425	6227	6094	4910	5775	7156	7654	11099	27080	25937	7798	1463
30.00	9.970	-2.981	-16.815	-22.614	-24.164	-36.248	-45.619	-40.179	-4.725	-48.538	33.702	12.855	-19.883	-43.409	3.176	-5.288	6.479	8.167
	0.470	0.580	0.530	0.770	0.810	0.880	0.760	1.170	1.130	1.610	1.120	1.570	1.260	1.480	1.560	1.080	0.950	1.000
	988	1151	1474	1455	1748	2462	4888	5736	6067	7773	9730	9042	12691	15064	13535	6614	400	7
20.00	5.536	-2.161	-3.632	-6.128	-46.035	-8.989	-22.823	-8.441	-8.799	-13.544	21.361	30.727	14.286	-8.146	-25.178	5.373	-1.573	3.563
	0.490	0.500	0.470	0.340	0.490	0.520	0.510	0.760	0.960	1.290	1.150	0.790	1.200	1.050	1.050	1.330	1.190	0.000
	275	67	176	404	659	1585	1825	1786	3498	6835	7860	6545	10367	9829	6178	3827	214	1
10.00	5.809	-6.098	-10.794	10.785	8.081	2.872	10.471	2.122	2.806	-1.747	-2.061	15.816	13.859	5.757	-4.343	-30.260	-9.628	1.023
10000	0.560	0.500	0.490	0.450	0.470	0.560	0.540	0.580	0.770	0.820	0.650	0.710	1.070	1.070	0.940	1.150	1.010	0.890
	1273	253	429	891	1060	1090	722	703	1738	4333	6213	4663	8766	8210	3758	3080	468	8
0.00	-22.216	-8.776	-16.130	11.008	26.657	11.707	13.330	13.571	-9.156	-8.236	-7.605	-35.599	-8.356	-27.323	10.560	-8.611	-15.345	0.929
0.000	0.510	0.560	0.510	0.540	0.460	0.420	0.440	0.480	0.680	0.500	0.590	0.670	0.820	1.230	1.060	1.240	0.930	0.550
	1212	248	605	1129	872	283	325	344	398	2683	5810	5203	9667	10537	7079	8658	5936	797
-10.00	-17,270	-5.885	-0.250	7.990	7.182	11.959	11.850	16.910	5.271	1.116	8.775	-24.475	-14.038	-31.571	-49.209	-3.322	17.117	-22.740
10100	0.520	0.490	0.480	0.580	0.480	0.440	0.500	0.480	0.470	0.390	0.460	0.790	0.910	1.330	1.160	1.150	1.200	0.950
	141	48	370	819	799	283	422	598	375	630	2182	3215	5334	7941	8434	8799	10273	5825
-20.00	-1.687	-1.301	1.576	7.643	4.293	1.721	7.463	8.699	7.737	2.705	2.510	-5.014	-28.768	-12.193	-1.042	-48.104	-19.115	-20.815
20000	0.370	0.470	0.520	0.480	0.440	0.510	0.540	0.550	0.450	0.460	0.490	0.510	0.770	0.950	1.280	0.970	0.810	1.100
	60	177	1791	2187	1045	230	314	394	165	76	136	1304	2314	4546	5391	3320	6158	6488
-30.00	1.789	-1.420	-1.781	-8.899	2.171	1.842	1.555	5.634	6.741	5.690	3.563	1.237	0.289	-24.957	13.533	-24.194	-45.150	-18.542
50:00	0.370	0.330	0.580	0.630	0.310	0.410	0.390	0.620	0.550	0.330	0.000	0.460	1.050	0.670	1.000	0.940	0.840	0.810
	21	493	2305	2321	752	187	149	74	65	39	4	1512	2433	2994	4176	3534	1800	2389
-40 00	3 491	2.093	-0.272	-2.231	-1.753	2.309	0.029	0.900	3.547	3.673	4.391	2.541	1.082	-6.846	-15.361	-5.303	-33.032	-53.676
10.00	0 300	0 320	0.250	0.230	0.340	0.270	0.250	0.330	0.480	0.530	0.460	0.380	0.470	0.580	0.530	0.440	0.540	0.950
	15	308	786	622	122	144	119	2.9	54	48	12	813	1395	972	1589	1504	618	1160
-50 00	4 086	3 476	2 708	2.151	2.768	2.872	2.250	0.061	-1.146	-1.403	-0.549	3.518	2.717	2.111	-0.099	-2.490	-1.828	-6.676
- 50 . 00	0 240	0 230	0 260	0.220	0.240	0.260	0.180	0.220	0.230	0.350	0.340	0.400	0.560	0.360	0.610	0.580	0.430	0.740
	0.240 AA	51	27	10	7	15	14	12	12	17	11	24	30	59	122	208	280	334
60 00	4 910	1 302	1 008	3 563	3 563	5 063	5.065	3.725	0.750	-2.098	-4.519	-4,489	2.571	3.140	3.394	3.735	3.281	3.234
-00.00	4.010	9.372	0 200	0 000	0 000	0 230	0 260	0 230	0.250	0.280	0.260	0.310	0.300	0.410	0.320	0.240	0.420	0.460
	145	0.340	0.230	0.000	0.000	0.230	430	410	199	8	31	379	353	24	110	181	143	30
70 00	140	/ 002	4 401	د مدد ۸	1 220	1 7 3 1	5 726	5 548	4 280	2 047	-0 617	-3.239	-2.423	3.563	4.056	4.099	5.096	4.615
-70.00	2.031	4.093	4.401	4.328	4.328	4./31	0 200	0 400	0 340	0 330	0 410	0.270	0.430	0.000	0.260	0.260	0.140	0.300
	0.3/0	0.270	0.430	0.340	0.430	0.420	0.290	411	202	0.550	20	379	350	0.000	8	66	246	208
0.0 0.0	18/	94	4/	4 244	4 000	6 1 2 1	400	411	2 505	2 6 2 1	0 907	1 390	8 1 3 0	15 420	10.551	8.622	4.292	24.694
-80.00	4.162	0.100	0.070	4.244	4.000	0.131	0 560	0.339	0 300	0 160	0.307	0 400	1.140	1.260	1.390	1.330	0.440	0.610
	0.930	0.190	0.070	0.680	0./10	0.200	0.500	U • / 0 U	0.590	0.100	12	120	1003	710	2.550	132	316	348
	82	60	43	44	29	20	/ 4	20	21	20	72	720	1000	120	00	192	010	0.0

Depth = 551 km

-180.00 -170.00 -160.00 -150.00 -140.00 -130.00 -120.00 -110.00 -100.00 -90.00 -80.00 -70.00 -60.00 -50.00 -40.00 -30.00 -20.00 -10.00 -3.332 -14.749 -28.551 -6.222 17.461 8.064 34.515 80.00 6.268 -26.751 -17.553 -8.084 -4.054 -19.529 -5.753 -2.693 1.364 16.178 15.300 1.470 0.570 1.290 0.940 2.330 1.000 1.210 0.410 0.560 0.920 1.050 0.620 0.500 1.480 0.710 0.430 0.860 1.940 277 350 431 593 663 739 984 1245 949 534 623 489 397 786 897 146 199 356 3.295 -5.494 -16.059 -9.956 3.102 4.271 4.745 9.318 -9.631 -7.198 -4.039 -1.874 -6.804 -5.366 -4.003 -11.527 70.00 25.546 17.743 0.900 0.920 1.540 1.080 1.100 0.690 0.620 0.620 0.780 1.030 0.970 0.650 0.680 0.650 0.900 0,750 0.700 0.860 542 782 608 826 856 863 1153 2061 794 451 335 3978 2853 1948 1160 1785 3548 5183 4.152 -0.564 -6.940 -7.736 -1.935 0.438 -6.391 -10.735 -11.548 -12.341 -5.042 5.001 29.827 30.400 26.075 19.818 9.826 60.00 13.580 0.690 0.800 0.960 1.270 1.190 0.720 0.550 0.740 0.670 0.870 0.990 0.750 0.830 0.710 0.750 0.700 1.020 0.910 664 783 1802 5498 820 1037 748 618 617 6792 4088 3316 2926 1897 1361 9338 11479 10865 -1.057 -5.097 -10.482 7.295 -6.605 -14.079 -17.124 -22.959 -11.392 -1.849 34.550 51.392 54.454 42.526 27.311 14.135 50.00 -19.257 9.916 0.530 0.560 0.640 0.950 0.840 0.910 1.090 0.530 0.630 0.710 0.780 0.820 0.680 0.710 1.100 0.960 0.710 0.880 1374 790 466 484 1019 3309 8900 1815 1527 9007 9237 6841 4074 3293 5675 6975 4628 3441 -1.476 -21.614 -12.459 -10.440 -10.161 -12.206 7.661 -24.124 -16.293 4.018 27.644 53.871 0.879 13.597 28.936 43.666 51.566 1.479 40.00 0.680 0.480 0.560 0.760 0.670 0.760 0.720 0.530 1.010 0.890 0.740 0.920 0.800 0.620 0.790 0.720 1.060 0.930 448 872 2464 5512 7783 5539 3393 2355 1511 588 663 840 590 498 2144 6056 10096 1429 -4.390 -12.948 -19.742 -18.972 -17.787 -2.211 -1.892 -26.539 -1.205 28.853 30.792 7.354 16.091 15.208 38.860 30.00 4.419 2.190 2.969 0.570 0.580 0.620 0.550 0.940 0.820 0.870 0.610 0.540 0.630 0.740 0.720 0.730 1.080 0.760 1.220 0.760 0.770 2406 1617 828 775 753 595 421 823 5545 3721 139 44 1150 3075 6149 6211 170 62 -5.955 -16.660 -21.909 -14.709 -3.905 20.958 -17.849 -27.456 -8.584 20.00 -2.323 -9.943 -15.783 -6.365 0.512 1.305 -1.562 16.842 51.364 0.550 1.010 1.110 0.760 0.550 0.640 0.680 0.710 0.640 0.580 0.670 0.650 0.840 0.820 0.730 0.890 0.720 0.760 415 133 379 2147 1273 982 697 6090 4283 53 295 700 1219 2891 5359 20 75 121 -3.015 -17.529 -46.152 21.145 -13.916 -28.025 -3.301 -7.634 10.00 -5.575 -13.372 -44.454 -52.479 -1.613 -2.631 -8.514 -1.205 25.999 48.554 1.020 0.760 0.670 0.770 0.820 0.750 0.660 0.630 0.760 0.840 0.820 0.000 0.620 0.840 0.860 0.920 0.970 0.940 1213 658 486 390 1136 1629 5686 5956 3647 10 26 35 12 0 15 227 1051 3695 -4.191 -4.278 3.977 9.432 5.793 -3.251 -5.685 -1.068 -5.544 -35.765 -48.751 -1.170 -2.809 0.00 -3.441 -6.438 -28.352 -53.197 -19.671 0.760 0.790 0.780 0.710 0.670 0.720 0.820 0.800 0.740 0.940 0.860 0.550 0.330 0.700 1.430 1.420 1.210 0.850 49 153 283 1266 1685 115 53 116 282 771 1754 5091 4238 326 24 76 104 197 -7.297 -22.106 -15.663 -24.195 1.701 0.280 -0.696 -5.615 -19.263 -2.638 -6.313 -7.957 1.711 -0.087 -2.435 -10.00 -8.793 10.684 6.459 0.690 0.610 0.450 0.660 0.800 0.750 0.750 0.720 0.820 1.540 1.360 1.210 0.930 0.610 0.570 0.620 0.690 1.420 690 3814 4243 1108 110 53 47 365 558 124 256 257 352 4482 5996 2599 6351 5444 -1.769 3.800 -2.560 -14.142 -40.619 -43.105 -13.964 -1.032 0.648 0.059 -5.863 -20.00 -24.796 -1.840 36.594 44.444 13.173 11.188 5.415 0.520 0.490 0.630 0.770 0.590 0.560 0.610 0.690 0.700 0.490 1.040 0.980 0.890 0.990 0.740 0.700 1.290 1.160 5215 2556 134 51 17 234 307 345 354 168 480 3183 2954 214 10700 9172 4863 6572 -1.719 -5.228 -0.745 -0.029 0.088 22.224 9.436 4.243 2.178 -5.004 -13.542 -11.496 -18.563 -30.00 -1.788 1.906 16.596 19.186 6.067 0.500 0.470 0.490 0.820 0.590 0.200 0.500 0.500 0.530 0.460 0.460 0.910 1.060 1.030 0.900 0.870 0.730 0.780 66 15 6 102 171 146 481 2148 4067 2011 4370 601 772 450 173 191 232 6144 -1.863 -3.805 -8.106 -10.219 -8.618 -1.613 0.196 0.537 0.062 3.929 1.991 1.028 0.203 0.118 1.524 3.854 4.405 -40.00 0.431 0.370 0.490 0.530 0.520 0.370 0.430 0.360 0.520 0.000 0.810 0.660 0.540 0.530 0.630 0.680 0.690 0.770 0.870 241 780 1201 493 28 2 9 68 66 58 13 1418 47 86 1396 452 7 -4.488 -8.489 -11.051 -9.927 -2.489 0.842 0.750 -1.300 -2.119 -2.957 -3.146 -4.054 -2.476 -1.214 -1.077 -50.00 -14.290 -2.371 -3.347 0.390 0.490 0.370 0.320 0.310 0.390 0.350 0.440 0.480 0.490 0.540 0.400 0.410 0.340 0.400 0.400 0.620 0.460 109 107 81 135 396 446 263 53 16 7 17 35 96 43 77 102 137 13 -4.326 -8.962 -11.858 -8.069 -3.868 -0.442 -2.299 -1.613 -1.613 -1.613 -2.054 -2.771 -60.00 -0.958 -4.655 -2.888 -2.699 -3.831 -3.326 0.000 0.000 0.000 0.220 0.310 0.350 0.290 0.310 0.390 0.410 0.390 0.180 0.180 0.180 0.460 0.370 0.250 0.190 154 471 579 394 3 0 1 13 45 78 94 103 53 13 5 9 42 77 -5.352 -7.236 -6.246 -3.985 -1.613 -1.613 -1.613 -1.613 -1.613 -1.613 -1.598 -1.786 -2.225 -3.107 -70.00 -0.669 -0.302 -1.613 -1.613 0.250 0.260 0.310 0.330 0.000 0.160 0.180 0.230 0.270 0.000 0.000 0.000 0.000 0.390 0.280 0.000 0.000 0.000 76 203 222 2 8 11 21 19 21 33 11 0 0 0 0 0 0 0 -1.613 -1.613 -1.613 -1.613 -1.613 -1.613 -1.613 -1.613 -1.613 -1.613 0.192 1.433 0.349 1.346 0.978 0.528 -80.00 4.164 1.563 0.000 0.000 0.000 0.000 0.000 0.660 0.580 0.900 0.000 0.000 0.000 0.560 1.310 2.360 1.120 0.810 0.000 0.000 29 14 0 0 0 0 1 1 1 0 1 3 17 22 54 139 103 185
	0.00	10.00	20.00	30.00	40.00	50.00	60.00	70.00	80.00	90.00	100.00	110.00	120.00	130.00	140.00	150.00	160.00	170.00
80 00	25 699	-54 273	-28.751	-13.288	-11.823	2,934	1.800	0.106	2.641	4.195	1.198	6.873	3.441	-9.681	-0.119	18.208	33.040	28.591
00.00	1 5 2 0	1 250	0 900	1 050	1 880	0.590	0.670	0.860	0.890	0.980	0.610	1.140	0.960	0.960	1.270	0.650	1.140	0.690
	1105	079	791	690	638	471	272	148	133	140	134	135	126	80	54	78	107	126
70.00	16 571	10 201	20 512	25 722	20 000	15 65/	-6 152	_2 117	-0 782	1 370	3.446	2.655	4.602	3.759	-2.944	-1.525	8.069	20.819
/0.00	10.5/1	18.281	-20.513	-23.722	-20.098	-17.024	-0.152	0 730	0 750	0 850	0 890	0 800	0.720	0.830	0.740	0.950	0.740	0.850
	1.240	1.270	0.030	0.790	2005	1650	747	190	111	168	208	240	326	305	194	129	354	606
	3275	336/	3099	3607	2885	16 620	10 202	1 1 2 5	0 570	2 073	6 477	8 758	5 281	4 007	2.145	-1.070	-2.645	1.882
60.00	-8.005	0.850	8.182	-24.08/	-29.791	-10.029	-10.302	-4.133	-0.570	2.075	0.4//	0.750	0 800	0 800	0 920	0 800	1.010	0.840
	1.380	1.500	1.420	1.180	1.200	0.970	0.960	0.950	0.000	0.030	0.990	1005	3106	1024	1596	1981	6316	5326
	13523	19533	17493	11546	6114	2437	1223	707	/9/	782	15 105	1000	1190	1034	2 945	11 460	13 163	-15 266
50.00	27.884	7.077	2.016	39.553	-4.537	-7.160	-2.394	2.131	6.403	8.726	15.125	23.022	22.452	5.000	2.005	1 200	1 200	0 740
	1.210	1.620	1.260	1.270	1.010	1.150	1.130	0.800	1.040	0.670	0.950	0.940	1.040	0.840	1.000	1.390	12227	6411
	19471	25056	24079	14713	7297	3211	2744	2818	2746	2408	2350	2828	3150	4604	18/95	23/33	12321	10411
40.00	16.880	11.691	-16.091	15.969	32.080	-4.302	-4.990	5.089	15.726	20.056	42.062	36.937	23.809	24.994	4.688	36.441	26.683	13.581
	0.720	0.900	1.060	1.150	0.870	0.860	1.040	1.000	0.920	0.780	0.780	0.820	0.920	1.200	1.310	1.090	0.890	0.760
	9841	11341	11124	7361	4865	4062	5994	6376	5133	5291	5580	6976	8510	12387	27252	25006	//52	1857
30.00	3.863	-0.809	6.541	-3.265	-16.848	-15.222	-43.611	-30.322	1.621	-9.819	38.730	53.016	25.635	12.136	26.800	-0.098	14.557	10.686
	0.560	0.580	0.480	0.550	0.560	0.730	0.830	0.840	0.840	1.150	0.960	0.900	0.950	1.080	1.180	0.990	0.980	0.860
	1170	1439	1822	1588	1802	2534	4836	5637	4938	8390	9300	9338	13498	15797	13976	6582	706	100
20.00	5.183	1.404	5.203	5.696	-23.274	-10.609	-21.195	-12.197	-6.227	-2.694	28.755	49.314	53.888	30.382	16.833	13.387	-3.302	0.936
	0.470	0.560	0.480	0.400	0.470	0.410	0.600	0.740	0.570	0.900	1.050	0.790	0.920	1.050	0.800	1.040	0.950	0.980
	485	286	441	776	836	1544	1869	1869	3186	6643	8267	8184	12127	10794	7099	4363	312	59
10.00	1.382	-5.161	-7.983	8.292	8.759	1.223	1.611	-3.313	5.355	7.608	18.630	42.103	45.416	37.779	18.403	-9.636	-9.732	-6.034
*****	0.550	0.450	0.600	0.560	0.560	0.560	0.630	0.690	0.700	0.750	0.680	0.780	0.950	1.000	0.790	0.800	0.720	0.930
	930	511	566	1076	1101	1144	843	581	1807	4369	6476	5309	9635	8963	4921	3799	642	130
0.00	-14,166	-9.346	-11.747	5.436	14.569	4.714	5.121	6.192	-10.870	-7.525	-3.370	1.954	15.003	12.174	48.265	0.937	-14.395	-7.375
0000	0.550	0.540	0.540	0.630	0.710	0.720	0.780	0.800	0.760	0.700	0.760	0.810	0.820	1.040	0.760	0.970	1.040	1.290
	866	311	652	1201	903	309	380	420	572	2502	5489	5479	10252	10877	7807	9173	6424	1620
-10.00	-18,511	-8,105	-5.947	2,567	2.670	4.519	4.017	7.275	1.165	-2.062	7.110	-8.183	1.477	-18.588	-20.663	22.530	31.008	-17.171
10100	0.460	0.450	0.410	0.530	0.740	0.770	0.830	0.810	0.880	0.660	0.710	0.780	0.670	0.860	0.830	0.800	1.120	1.320
	234	89	408	861	772	353	467	586	400	585	2182	3676	5982	8300	9242	9525	10248	6485
-20.00	-8.520	-5.219	-3.170	-2.942	-2.086	-2.843	1.354	1.700	1.218	-1.135	0.025	-1.874	-14.140	-14.196	6.118	-29.490	-8.273	18.028
20100	0.420	0.450	0.430	0.430	0.630	0.700	0.750	0.790	0.840	0.750	0.660	0.600	0.610	0.670	0.940	0.820	0.750	1.120
	147	291	1483	2140	1170	287	289	349	171	78	218	1464	2644	4582	5724	3974	6111	7565
-30 00	-2.908	-4.666	-1.612	-10.974	-4.322	-3.250	-3,916	-0.462	0.107	-0.205	-1.005	0.514	4.629	-18.091	-2.991	16.282	-24.122	-3.559
50.00	0.490	0.470	0.580	0.530	0.510	0.650	0.630	0.720	0.750	0.740	0.640	0.610	0.770	0.680	0.670	0.700	0.610	0.730
	142	865	2048	2308	880	203	157	79	68	49	15	1284	2446	2947	4054	3601	2202	3237
-40 00	-0 677	-1.569	-1.375	-3.512	-5.422	-3.060	-5.083	-4.950	-3.167	-3.219	-2.235	-2.126	-0.924	-5.259	-14.450	-3.728	-5.237	-42.830
10:00	0 600	0 560	0.480	0.470	0.440	0.550	0.590	0.570	0.580	0.570	0.660	0.600	0.580	0.590	0.600	0.550	0.600	0.720
	118	600	842	634	143	141	110	4.0	64	48	18	416	1083	968	1284	1328	854	1223
-50 00	_0 197	-0 402	-0.649	-0.855	-1.244	-1.696	-2.562	-5.067	-6.725	-7.898	-8.589	-5.332	-3.469	-2.326	-2.452	-4.127	-3.620	-3.788
- 50 : 00	0.510	0 530	0 510	0.470	0.450	0.460	0.470	0.500	0.470	0.480	0.520	0.560	0.570	0.570	0.620	0.640	0.590	0.570
	74	82	57	35	35	19	16	12	22	17	12	24	34	62	142	212	232	239
60 00	_0 011	_0 097	0 003	0 215	0.462	0.370	-0.020	-1,223	-4.090	-7.162	-10.316	-12.937	-8.632	-5.338	-3.402	-1.663	-1.481	-1.468
-00.00	-0.011	0.480	0.005	0.215	0.460	0 440	0.020	0.450	0.470	0.450	0.440	0,450	0.520	0.560	0.550	0.520	0.560	0.600
	164	70	21	10	15	79	315	406	285	59	38	380	350	65	109	178	139	35
70 00	1 0 1 7	0,777	-0 318	-0.061	0 301	0 711	0 785	0.466	-0.722	-2.787	-5.379	-8.348	-10.572	-8.231	-5.773	-3.888	-1.785	-1.094
-/0.00	-1.01/	0 370	0 410	0 400	0.301	0.440	0.430	0.410	0.420	0.460	0.460	0.460	0.450	0.460	0.410	0.380	0.420	0.430
	104	100	53	4.0	10	83	329	408	289	66	34	378	347	38	13	83	237	196
80.00	0 355	_0 243	_0 062	-0 418	_0 282	0 355	0.483	0.487	-1.489	-1,913	-4.150	-2,494	-1.444	4,430	0.393	2.008	-0.511	11.990
-00.00	0.040	0.243	0.790	0 310	0.202	0.520	0.500	0.260	0.310	0.380	0.570	0.490	1.160	0.580	0.380	0.840	0.300	0.400
	0.940	0.000	67	0.510	71	100	0.500	37	27	32	58	327	989	811	118	127	300	300
	/3	10	0 /	02	/ 1	107	24	57	21	52	50	521	202					

-180.00 -170.00 -160.00 -150.00 -140.00 -130.00 -120.00 -110.00 -100.00 -90.00 -80.00 -70.00 -60.00 -50.00 -40.00 -30.00 -20.00 -10.00 4.718 1.321 9.163 9.832 7.637 -5.417 -9.599 1.411 14.096 -0.697 -14.072 -12.001 -7.036 -7.107 -5.465 3.887 80.00 -23.368 -33.221 0.680 1.310 0.740 0.440 0.650 1.170 0.660 0.480 0.830 0.830 0.540 0.640 0.500 0.660 0.730 0.610 1,160 1.030 500 669 926 435 463 584 544 619 677 706 599 487 463 1081 1198 313 501 961 3.099 6.835 5.445 -7.776 0.238 3.435 -0.567 -4.673 -0.816 -4.155 -1.565 -7.218 -10.180 -9.380 -8.840 70.00 12.910 -2.958 -16.023 0.670 0.830 0.710 0.700 0.800 0.640 0.670 0.740 0.670 0.640 0.670 0.880 0.550 0.570 0.930 0.800 0.670 0.800 923 922 792 1324 2058 719 855 817 1483 1100 960 527 562 4458 3435 2533 2731 4014 2.526 6.487 5.831 1.502 3.363 2.411 60.00 31.186 28.605 6.520 5.945 -2.171 -8.015 -9.801 -10.891 -13.177 -6.260 17.087 6.788 0.900 0.590 0.690 0.950 0.770 0.650 0.670 0.880 0.580 0.700 0.750 0.640 0.890 0.860 0.800 0.910 0.890 0.820 725 1005 2298 5456 893 860 3023 2009 1236 846 1003 1104 10430 11956 9773 6334 4065 3738 -7.296 -1.043 22.149 -9.558 -12.287 -15.634 -16.193 -8.043 -3.237 -2.618 36.491 34.245 23.391 20.679 15.441 3.139 23.122 50.00 12.478 0.720 0.940 0.700 0.790 1.020 0.580 0.560 0.560 0.660 0.510 0.490 0.680 0.720 0.610 0.660 0.810 0.660 0.820 8736 1622 5455 4200 6206 7022 4746 3060 2085 1505 1312 877 573 548 10085 7041 4333 9917 -8.231 -18.182 -16.810 -19.242 -22.819 -24.309 0.464 -5.243 -24.515 -10.345 12.138 25.119 26.373 39.040 16.965 21.066 40.00 18.566 12.265 0.530 0.420 0.390 0.320 0.490 0.590 0.720 0.730 0.720 0.590 0.640 0.610 0.820 0.800 1.050 0.790 0.690 0.780 2254 1464 679 453 701 1412 4292 5477 6186 8274 6867 4950 3309 834 852 3125 1421 907 -9.028 -23.725 -54.247 -42.678 -16.333 -2.257 39.399 16.335 -20.137 -11.217 10.404 9.279 7.215 4.100 3.879 3.786 -32.873 21.814 30.00 0.780 0.720 1.290 0.760 0.670 0.520 0.400 0.280 0.370 0.530 0.430 0.480 1.040 0.920 0.800 0.740 0.610 0.760 771 928 720 686 1210 5446 6239 5140 2873 1925 984 1720 3144 4802 472 443 332 134 -6.285 -1.055 -9.820 -37.258 -53.494 -12.927 -5.082 -4.170 -7.373 -12.276 20.989 50.992 29.843 -55.377 -24.708 20.00 -2.233 -4.550 -5.508 0.510 0.560 0.500 0.490 0.470 0.330 0.820 1.080 0.810 0.590 0.900 0.770 0.770 0.850 0.780 0.710 0.890 0.970 506 456 714 5781 6779 5414 2988 1420 914 631 68 94 48 838 1356 1435 3142 28 24.981 49.288 33.527 -13.001 -25.986 -4.214 -2.278 -19.434 -53.629 -19.609 -9.167 -8.472 -14.683 0.679 10.00 -5.799 -10.071 -24.735 -21.505 0.660 0.730 0.580 0.590 0.420 0.780 0.920 0.670 0.560 0.940 0.940 0.940 0.910 0.800 0.640 1.140 0.990 0.930 1154 604 409 482 1183 1464 11 17 140 370 790 3509 6272 6807 3929 29 31 45 -5.125 -2.959 -9.778 -27.903 -38.424 19.889 21.091 4.224 -2.303 -24.415 -54.827 -15.223 -5.819 -5.895 -8.643 -3.877 11.182 0.00 -3.507 0.660 0.650 0.500 0.660 0.660 0.760 0.980 0.910 0.970 0.930 0.880 0.760 0.710 1.010 0.770 1.390 1.210 0.960 4148 586 89 147 387 1288 1388 104 218 430 842 1867 4849 937 339 266 415 729 -5.506 -15.039 -15.927 -9.905 -15.598 2.454 -1.726 -3.468 -9.439 -24.168 6.791 -10.00 -1.968 11.863 8.455 -7.001 -13.285 -1.458 -3.468 0.900 0.750 0.800 0.720 0.770 0.850 0.770 0.720 0.810 0.760 0.640 0.460 0.850 0.940 0.920 0.820 1.040 0.990 128 53 129 458 642 533 823 3719 4201 1383 4798 5794 2172 573 333 455 7159 6671 -7.643 -23.687 -27.071 -33.676 -10.358 -2.525 -4.104 27.377 4.342 5.702 1.793 1.498 -1.012 -1.169 -7.771 16.830 21.502 -20.00 9.073 0.780 0.770 0.820 0.780 0.730 0.540 0.650 0.760 0.730 0.790 1.030 0.990 0.840 0.780 0.680 0.770 0.950 1.070 440 53 32 177 303 5046 2391 5196 6355 2489 726 378 391 517 622 3398 10418 9461 -5.317 -15.988 -6.358 -2.368 -1.210 -1.876 -3.302 10.573 4.308 1.831 0.282 -1.658 -11.932 -14.792 17.988 12.830 -30.00 12.255 15.648 0.750 0.780 0.780 0.700 0.650 0.660 0.700 1.290 1.060 0.940 0.770 0.530 0.670 0.670 0.730 0.730 0.830 1.000 12 93 118 191 212 240 316 589 2024 3549 1804 409 18 625 740 579 5596 3764 -9.402 -10.051 -5.235 -1.439 0.429 -0.451 3.212 1.372 0.753 -0.757 -1.856 -2.875 -3.764 -5.661 -7.217 2.363 3.094 -40.00 -13.651 0.750 0.750 0.740 0.700 0.720 0.410 0.600 0.730 0.760 0.870 0.950 0.870 0.750 0.670 0.390 0.510 0.590 0.350 95 29 50 117 149 21 39 86 294 591 969 553 398 133 8 35 32 1193 -8.467 -11.788 -12.433 -6.114 -0.601 2.547 -2.793 -2.997 -3.651 -4.1.3 -4.159 -5.219 -8.450 -4.813 -4.913 -4.248 -3.270 -50.00 -15.490 0.360 0.420 0.440 0.310 0.370 0.480 0.550 0.620 0.690 0.740 0.330 0.360 0.440 0.420 0.460 0.370 0.460 0.370 137 81 153 255 380 274 14 24 34 88 166 53 79 87 49 14 156 62 -6.708 -4.766 -3.695 -3.331 -3.254 -3.254 -3.759 -4.129 -9.403 -11.018 -9.452 -5.876 -1.623 -5.207 -5.302 -6.194 -5.717 -60.00 -2.476 0.270 0.380 0.470 0.550 0.620 0.210 0.300 0.260 0.290 0.210 0.170 0.150 0.120 0.120 0.000 0.000 0.500 0.420 81 89 167 320 550 436 15 57 40 40 50 79 83 43 10 6 4 4 -3.755 -4.373 -6.239 -7.446 -7.191 -5.498 -3.254 -3.254 -3.254 -3.254 -3.232 -3.454 -70.00 -2.145 -1.818 -3.177 -3.254 -3.254 -3.254 0.200 0.220 0.260 0.350 0.460 0.550 0.000 0.000 0.000 0.000 0.000 0.000 0.090 0.140 0.440 0.360 0.250 0.000 2 0 1 2 3 8 12 18 18 22 84 212 237 38 30 8 1 0 1.447 -3.254 -3.254 -3.254 -3.254 -3.254 -3.254 -3.254 -2.609 -0.824 0.473 -1.701 0.484 0.161 0.955 0.578 1.543 -80.00 -0.008 0.000 0.000 0.640 0.770 0.690 1.230 1.130 2.000 1.340 0.490 0.940 0.000 0.000 0.000 0.000 0.000 0.170 0.570 27 41 85 3 2 9 153 122 99 32 13 3 4 4 3 4 152 201

	0 00	10 00	20.00	30.00	40.00	50.00	60.00	70.00	80.00	90.00	100.00	110.00	120.00	130.00	140.00	150.00	160.00	170.00
80 00	-5 578	-18 077	-44.368	-5.409	-11.440	-0.261	0.165	-2.366	-0.373	2.512	2.628	4.079	4.164	-3.153	6.252	23.090	22.037	1.301
00.00	-J.J/0	1 270	0 830	0 580	0 470	0 770	0.620	0.660	0.530	0.530	0.750	0.640	0.740	0.990	1.340	0.960	1.360	0.780
	2.000	1102	1205	1202	1192	822	537	385	148	120	114	108	82	43	35	95	165	224
70 00	5 010	1 1 7 1	10 656	20 022	10 207	15 525	-7 976	_3 837	-3.002	-1.576	0.665	1,907	3.198	3.961	1.194	4.882	15.498	20.000
/0.00	5.019	-1.1/1	-10.050	-20.932	-10.397	-10.525	0 700	0 740	0 760	0 710	0.610	0.680	0.600	0.660	0.730	1.020	0.750	0.930
	0.930	1.5/0	0.940	1056	1665	2972	1510	713	206	164	284	406	461	312	270	264	570	1118
<pre></pre>	3723	4191	4907	4000	4000 20 052	20/2	11 976	.6 040	-2 500	-0 650	1 235	3,313	3.267	3.369	7.059	9.139	13.054	23.806
60.00	-0.520	2.505	2.844	-/.191	-29.052	-20.103	-11.070	0,770	0 640	0.810	0 600	0.680	0.600	0.640	0.640	0.770	0.890	0.770
	0./10	0.910	0.960	1.200	0.930	1670	2102	1/10	1024	0.010	782	884	1202	1271	5223	8672	7558	6512
50.00	12215	1/653	19/80	14309	3400	4070	2 0 0 0	0 264	2 863	2 252	10 768	17 132	17.527	7.307	0.313	26.688	40.898	12.322
50.00	25.220	20.073	-2.132	44.881	23.353	-1.907	-3.009	0.204	1 050	3.333	0.810	0 750	1 050	0 730	0.930	1,170	0.870	0.590
	0.970	0.910	1.130	1.100	1.130	0.000	0.930	1570	2940	2570	2514	2955	3424	5217	18677	23046	12278	7926
	14581	20108	24068	18223	10982	12 200	4040	4370	2040	2 J / J	15 077	12 812	46 815	38,839	12.096	36.534	36.544	29.352
40.00	-0.944	13.411	21.620	11.494	42.767	13.200	3.09/	-1.701	0 770	0.014	13.077	0 020	0.750	1 010	1 010	0.910	0.750	0.770
	0.840	0.850	0./80	0.930	0.990	0.780	0.920	0.900	0.770	0.520	6340	6200	8929	13/2/	25663	23086	7091	2414
	5916	//89	9961	8984	6488	5399	0195	0100	4912	1 670	17 422	E2 424	51 906	18 609	11 215	5 047	14.591	13.023
30.00	-1.607	0.//6	21.892	/.39/	-11.66/	-9.320	-28.242	-23.554	-14.233	1.0/0	1/.422	0 9/0	0.000	0 840	0 870	0.740	0.880	0.800
	0.810	0.710	0.720	0.540	0.580	0.530	0./50	0.700	0.700	0.700	0.020	9520	13673	15561	13911	6828	1433	613
	1136	1506	2155	2261	23/1	2987	4621	4980	45/5	0 216	22 057	5520	13013	53 955	19 117	27 789	0 164	0.021
20.00	7.981	15.036	13.672	4.226	-11./51	-1/.5//	-19.500	-14.309	-5.818	0.210	23.057	27.100	1 200	1 140	40.117	0 900	0.264	0.880
	0.430	0.700	0.610	0.420	0.390	0.390	0.540	0.640	0.510	0.830	0.800	0.000	12446	12001	8262	1539	756	143
	859	657	871	1070	101/	1339	164/	1624	3322	16 120	10 077	10 127	13440	52 724	30 137	6 206	-5 926	-9.632
10.00	-1.779	0.666	0.865	9.661	9.961	4.643	-1.823	-3.62/	4.544	10.139	10.073	4 7 . 1 3 /	1 170	1 440	0 890	0.200	1.040	1.160
	0.420	0.470	0.620	0.530	0.4/0	0.490	0.580	0.650	1060	1272	6500	6/02	10477	10326	6910	4793	1006	221
	729	571	877	1310	1137	1068	911	213	11 200	42/3	6 J J F	12 209	10 006	51 611	53 807	7 264	-19,142	-10.814
0.00	-10.005	-8.071	-5.817	/.154	9.630	3.399	4.004	3.405	-11.299	-3.002	0 7 9 0	1 010	1 090	1 210	1 160	1 070	1 090	1.220
	0.430	0.520	0.550	0.580	0.700	0./50	0.810	0.760	0.800	0.000	0.780	1.010	1.000	1.210	0626	0113	6580	2506
	544	318	649	1099	852	330	486	223	1 7 2 5	2572	474/	0 010	2 0 2 2	12 716	15 854	30 522	22 819	-38,611
-10.00	-14.234	-10.998	-8.600	-0.598	2.931	4.009	3.122	4.200	1./30	-2.503	2.313	-0.910	- 3.033	0 910	0 850	0 920	0 900	1 170
	0.420	0.430	0.420	0.540	0./40	0.890	0.900	0.910	0./90	0.740	0.040	2010	6147	0.910	0.050	10014	9893	7798
	315	159	505	1057	850	354	491	551	453	010	2009	1 402	10 014/	7 062	11 210	_7 207	-29 353	20 634
-20.00	-9.885	-3.173	-6.621	-9.667	-3.680	-0.441	0.840	0.03/	-0.795	-0.848	-0.729	-1.492	-12.270	-7.002	0 750	0 770	0 760	0 890
	0.500	0.450	0.460	0.470	0.670	0.850	0.890	0.920	0.800	0./90	0.730	1552	2004	4611	5077A	1196	6223	8999
	238	474	1278	1979	1231	3/8	308	312	136	101	207	100	2904	11 470	12 757	12 535	13 630	_39 837
-30.00	-4.306	-3.939	1.817	-10.915	-/.880	-3.865	-3.440	-2.074	-1.054	-1.921	-2.229	-0.110	0 710	-11.470	-13.737	0 560	0 650	0 770
	0.590	0.520	0.570	0.520	0.570	0./50	0.//0	0.880	0.840	0./00	0.700	1104	2207	2011	2026	3170	2453	3828
	272	1118	1775	2036	966	270	165	97	66	5/) C	1104	1 5 4 1	2011	11 402	0 162		_47 205
-40.00	-1.353	-1.153	0.146	-2.422	-6.241	-4.587	-5.689	-6.0/1	-4.819	-5.006	-4.484	-4.025	-1.541	-2,001	-11.402	- 3 . 102	-13.732	0 630
	0.720	0.630	0.610	0.600	0.580	0.680	0./30	0.680	0./40	0.660	0.610	0.550	0.510	0.510	1250	1150	0.430	1257
	340	824	883	379	150	159	116	52	49	38	10 020	7 0 6 2	5 1 0 7	2 0 0 4	1 952	2 5 2 5	5 5 5 5 7	5 664
-50.00	0.701	-0.925	-1.274	-1.629	-2.516	-2.951	-3.504	-5./42	-/.353	-8./34	-10.030	-/.962	-2.10/	-3.004	-1.000	-3.525	- 5.552	- 5.004
	0.730	0.710	0.670	0.640	0.600	0.570	0.620	0.610	0.580	0.580	0.610	0.550	0.520	0.570	172	0.000	215	200
	256	234	187	39	42	45	27	23	24	20	10 276	97	11 204	7 0 /	1 962	200	213	203
-60.00	0.323	0.241	-0.404	-0.895	-1.206	-1.593	-1.874	-2.581	-4.844	-/.398	-10.276	-13.550	-11.304	-/.2/1	-4.002	-2.521	-2.110	-2.757
	0.680	0.690	0.680	0.660	0.640	0.600	0.570	0.580	0.590	0.560	0.520	0.510	0.510	0.480	0.530	0.540	0.000	0.000
	299	76	34	24	31	53	184	367	360	117	52	369	355	1/6	14/	1/0	2 251	49
-70.00	-2.928	-1.178	-0.398	-0.423	-0.678	-0.966	-1.281	-1.473	-2.318	-3.855	-5.783	-8.145	-10.590	-10.257	-/.832	-5./40	-3.351	-2.3/4
	0.580	0.620	0.640	0.630	0.630	0.590	0.540	0.510	0.520	0.540	0.510	0.480	0.460	0.440	0.390	0.380	0.410	174
	168	97	69	45	79	83	228	385	362	156	55	368	349	142	50	1 710	221	1/4
-80.00	-0.044	-1.044	-0.830	-1.826	-1.916	-1,952	-2.504	-1.532	-1.930	-3.648	-4.867	-1.862	-2.304	4.351	-1.039	-1./10	-2.031	0.927
	0.690	0.530	0.570	0.470	0.370	0.470	0.110	0.060	0.250	0.470	0.480	0.400	1.190	1.050	0.220	0.260	0.280	0.130
	98	77	108	97	119	98	83	23	45	69	70	230	966	859	379	102	281	262

-180.00 -170.00 -160.00 -150.00 -140.00 -130.00 -120.00 -110.00 -100.00 -90.00 -80.00 -70.00 -60.00 -50.00 -40.00 -30.00 -20.00 -10.00 34.452 29.654 -13.072 1.784 23.822 24.045 -11.950 -25.260 -22.026 -9.094 -7.494 9.726 -11.169 9.558 9.838 80.00 -54.279 4.825 60.900 1.510 1.400 1.500 2.110 0.710 1.160 1.770 1.110 1.240 0.840 1.880 1.680 2.140 1.300 1.870 1.170 1.280 1.840 783 694 764 638 548 447 531 784 639 512 344 427 649 1322 974 718 1105 1197 -6.954 -0.255 4.213 18.619 22.900 3.484 1.080 5.781 -10.700 -17.201 -14.275 -12.789 -2.709 70.00 -9.680 -38.809 -15.031 25.550 24.394 1.450 1.240 1.110 1.520 1.430 1.460 1.380 1.320 1.400 1.300 1.250 1.730 1.580 1.620 1.720 1.640 1.990 1.800 958 921 973 876 884 898 1578 2677 1074 968 862 954 3087 3080 2307 1579 3801 3108 20.046 -4.789 -0.462 5.126 13.787 -1.677 -8.282 -15.199 -19.274 -27.604 -9.988 8.648 8.938 -9.988 -3.660 18.967 22.793 60.00 31.176 1.960 1.360 1.870 1.940 1.710 1.910 2.040 1.730 1.890 1.950 1.520 1.990 1.570 2.040 1.420 1.700 1.850 1.930 960 921 1807 3202 5110 1299 1205 1082 1015 1414 5927 4316 3879 2921 2171 11079 11741 8392 15.548 -8.025 -26.570 -29.058 -27.352 -20.283 -7.552 -4.353 -2.999 -5.430 41.012 6.135 6.228 14.066 19.162 8.535 3.141 50.00 26.237 1.100 0.980 1.000 1.220 1.270 1.490 1.230 1.210 1.140 1.080 1.360 1.360 1.290 1.080 1.610 1.190 1.280 1.050 871 729 1010 3341 6310 7754 2288 1461 1243 10015 6731 4591 4724 6521 6571 4951 2991 10676 -49.044 -30.103 -12.518 -13.056 -27.217 -17.275 -27.233 -20.918 -0.316 -45.544 -21.226 -1.263 -29.639 -7.146 -13.359 28.399 21.016 40.00 48.719 0.660 0.760 0.930 0.850 0.990 0.820 0.850 0.850 1.250 1.210 0.910 0.970 1.540 1.500 1.300 0.970 1.250 1.290 810 525 1082 2734 5044 5068 6621 5850 4242 3100 1887 1301 1295 1351 1522 3676 6206 1413 4.753 -7.927 -13.554 -45.024 -49.725 -44.380 4.463 -33.545 -59.727 -10.328 -25.370 -31.475 -50.841 -1.689 21.689 20.444 30.00 35.134 28.824 0.720 0.650 0.770 0.550 0.700 1.400 1.040 0.820 0.830 0.590 1.370 1.240 1.060 1.110 1.510 0.890 0.890 1.280 6288 4056 2080 1196 748 841 1215 1485 1502 4430 6030 697 490 807 2330 3254 3275 890 -1.538 -23.514 -35.325 -19.440 3.389 -1.406 -0.481 23.017 -11.158 11.690 -39.180 20.00 11.717 15.494 14.923 9.421 -7.721 -24.774 -23.380 0.500 0.810 0.600 0.470 0.930 0.790 1.220 1.750 1.130 1.030 0.710 0.650 1.130 0.940 0.790 1.080 1.120 1.100 1811 894 598 542 687 919 7250 6529 3858 1499 2857 5461 212 496 1588 2004 117 180 6.349 -29.490 -21.453 -23.381 -4.546 11.515 -45.995 19.189 -14.631 14.862 16.794 11.894 2.678 -17.571 -24.804 -2.469 4.300 10.00 5.899 0.940 1.370 0.980 0.720 0.690 0.550 0.570 0.680 0.890 0.920 0.660 0.530 1.220 1.070 0.840 0.720 1.700 1.480 387 737 1224 1286 7133 4474 1715 575 3144 6151 185 77 42 110 349 409 492 884 -0.370 -14.961 -23.982 -15.235 1.371 -15.871 1.557 22.396 3.438 0.183 -15.712 -31.940 -14.738 11.437 0.00 -1.673 27.301 44.099 32.452 0.790 0.830 0.750 0.770 0.560 0.970 0.570 0.780 0.480 0.470 1.100 1.010 0.690 0.700 1.720 1.540 1.340 1.120 1232 173 221 620 1244 1363 257 456 700 888 2072 4422 4033 1335 1800 1447 544 967 21.282 13.012 3.345 -6.343 -24.109 -48.113 4.522 -12.279 -28.189 -37.918 -15.186 -20.247 2.257 64.526 67.860 28.042 -10.00 -13.214 15.797 0.670 0.920 0.740 0.390 0.740 0.820 0.550 0.640 0.660 1.140 1.420 1.030 0.780 0.770 0.680 0.730 0.900 1.100 951 3476 4039 1577 314 133 247 543 671 591 694 629 5351 5129 1977 1004 8066 7350 8.275 4.744 -2.161 -13.377 -5.781 15.153 10.000 -3.999 -27.080 -35.676 -11.054 -20.00 3.055 7.395 51.424 64.729 35.871 9.162 1.532 0.830 0.940 0.950 0.610 0.630 0.620 0.840 0.870 0.860 0.840 0.850 0.890 0.970 0.750 0.680 0.680 1.210 0.910 3222 4432 2114 823 86 62 143 308 726 689 788 1996 1259 547 10263 8456 5138 5259 5.640 9.419 11.217 10.729 6.791 15.244 6.729 -3.561 -15.150 -9.566 3.874 -1.460 -30.00 14.113 20.496 20.578 31.374 30.996 4.579 0.940 1.000 0.910 0.960 0.740 0.600 0.690 0.730 0.610 0.750 0.810 0.890 0.730 0.780 0.930 0.610 0.690 0.740 940 51 24 92 212 599 696 1880 2802 1594 597 667 658 487 220 411 4667 2340 4.865 1.884 1.345 -7.871 -5.058 1.668 8.729 15.533 18.103 7.263 5.635 5.139 10.879 11.331 12.458 11.195 -40.00 -5.762 7.716 0.970 0.990 1.050 1.090 0.690 0.790 0.690 0.710 0.820 0.900 0.700 0.650 0.840 0.720 0.950 0.880 0.830 0.910 171 382 234 296 476 756 621 441 78 109 142 38 55 41 23 48 1005 381 5.084 2.926 -3.872 -13.206 -12.420 -6.948 16.308 4.525 4.420 5.431 5.108 -0.139 2.754 5.214 6.219 6.026 -50.00 -21.205 -7.345 0.980 1.010 1.050 0.850 0.740 0.740 0.760 0.850 0.670 0.710 0.870 0.920 0.840 0.820 0.750 0.680 0.710 0.710 174 138 154 226 360 335 22 25 31 120 232 69 74 48 20 203 117 62 3.459 4.922 2.321 -4.020 -6.502 -6.276 -2.698 5.443 5.325 5.444 -8.475 -4.817 -2.240 -0.161 4.020 5.588 5.909 -60.00 -5.856 0.620 0.670 0.690 0.710 0.650 0.650 0.690 0.740 0.820 0.930 1.010 0.550 0.610 0.640 0.620 0.620 0.610 0.540 312 521 449 12 5 5 * 9 23 65 75 84 166 52 21 72 53 52 70 5.954 1.601 -0.135 -1.035 -0.227 6.598 6.598 6.598 6.598 6.188 5.828 5.519 4.334 1.216 -1.351 -0.597 2.255 -70.00 4.541 0.700 0.980 1.150 1.190 0.000 0.480 0.570 0.590 0.840 0.000 0.000 0.000 0.330 0.590 0.570 0.530 0.440 0.330 122 224 239 7 18 16 16 28 32 20 18 9 2 2 2 2 7 52 6.957 6.870 6.498 7.407 7.875 15.079 15.420 8.627 24.178 8.792 8.143 7.349 12.197 13.200 12.685 16.592 19.259 -80.00 8.880 3.520 0.230 0.420 0.850 2.560 2.040 4.180 1.950 3.440 1.820 0.160 0.710 0.890 0.100 0.720 1.360 3.250 2.670 122 86 24 6 6 5 5 6 10 14 44 81 113 201 181 139 134 140

	0.00	10.00	20.00	30.00	40.00	50.00	60.00	70.00	80.00	90.00	100.00	110.00	120.00	130.00	140.00	150.00	160.00	170.00
80.00	-12.519	13.484	-31,941	-37.577	18,921	5.608	3.256	-2.109	-6.108	-0.558	6.534	13.569	8.112	-4.390	6.642	27.048	2.911	-34.339
00.00	2 020	2.370	1.800	1.280	1,240	1.200	1.070	1.480	1.180	1.130	1.640	3.070	2.060	2.760	3.360	2.220	2.330	2.010
	1073	1528	1681	1850	1900	1741	1287	679	423	257	154	149	136	165	202	247	363	490
70 00	0 1/3	5 350	2 343	_17 244	_31 224	-10 256	-4.628	-0.879	-0.866	-2.941	-2.057	0.879	5.044	4.396	-1.020	3.024	16.653	10.906
70.00	9.143	-3.330	1 0 2 0	1 050	1 620	1 230	1 260	1 310	1 400	1 360	1 360	1.440	1.970	1,990	1.890	2.430	2.090	1.990
	1.520	1.740	1.920	0141	1.030	5169	3006	1535	7.400	514	509	566	602	601	527	575	992	1953
<pre>co oo</pre>	4265	0002	7 1 2 5	9141	16 047	26 521	16 714	1 167	1 0/1	1 719	-2 066	-8 046	-14 346	-16.846	-12,103	-3.852	7.236	31,762
60.00	-/.528	-2.828	-/.135	2.070	-10.947	-30.331	-10./14	1 700	1 220	1 720	1 430	1 510	1 600	1 420	1 810	1.600	1,990	1.800
	1.480	1.850	1.600	2.120	1.810	1.830	1.120	1.700	1.230	1240	1072	1002	1211	2015	8263	11518	8560	8562
	9/10	14938	18/91	1/544	13183	8/69	4384	2038	1004	1240	1 0 0 5	12 004	20 541	1E 0E2	51 067	11 771	33 906	13 521
50.00	2.990	2.297	-32.755	-13.272	59.410	23.190	-10.801	-4.028	1.528	3.542	1.905	-12.004	-29.541	-45.052	-51.907	-11.771	1 0 2 0	1 250
	1.490	1.060	1.570	1.580	2.020	1.480	1.290	1.410	1.500	1.100	1.360	1.400	1.400	1.4/0	10540	1.010	10125	0001
	9437	14488	20376	19175	13719	9243	6037	5337	3174	2777	2726	3031	3425	8/10	18542	22100	12135	5001
40.00	-23.068	-3.585	-0.673	-31.060	-18.423	44.024	43.345	-36.225	-4.752	21.746	-12.616	-22.345	-35.03/	-1/.465	-48.89/	-13.990	27.066	5/.//2
	1.040	1.090	0.920	1.350	1.680	1.970	1.620	1.570	1.690	1.180	1.790	1.590	1.240	1.450	1.460	1.010	1.290	1.740
	3004	3670	7070	8512	7687	6903	6131	6019	4377	5301	5061	5337	7766	14290	22027	19137	6999	3002
30.00	-28.624	-5.092	33.367	31.041	-21.396	-57.678	-16.149	-40.723	-50.222	-12.698	-14.055	2.006	-34.970	-20.506	36.364	-26.905	-4.085	24.939
	0.880	0.990	1.060	1.070	0.980	0.930	1.180	0.710	1.250	1.500	1.280	1.090	1.210	0.990	1.460	1.070	1.080	1.280
	1000	1434	2117	2642	2805	3333	4044	3906	4359	7032	7650	8855	12736	14620	13142	7118	2336	1159
20.00	-48.612	-8.620	39.398	50.889	12.048	-37.170	-49.220	-25.816	-20.959	-10.205	7.438	36.861	60.551	4.197	8.097	20.226	4.394	5.218
	0.800	0.920	1.000	0.960	0.820	0.950	0.770	0.870	0.740	1.090	1.140	1.160	1.770	1.740	1.270	1.270	1.030	1.330
	1101	947	1314	1472	1394	1375	1485	1361	3750	6497	7926	9437	13235	12154	9323	5293	1468	340
10.00	-36.903	-27.392	23.786	52.573	40.408	27.272	-6.352	-23.076	-8.791	17.501	8.936	25.055	64.754	20.400	15.855	1.084	-6.651	-4.363
	0.590	0.670	0.890	0.960	0.890	0.640	0.710	0.800	0.720	1.020	1.170	0.850	1.360	1.970	1.510	1.140	1.170	1.660
	935	685	1139	1443	1287	1223	1142	708	2259	4000	6260	7359	11107	11575	9125	6522	2077	422
0.00	-16.345	-15.338	4.748	33,110	27.331	12.626	13.287	-4.841	-28.440	-6.388	21.524	24.257	28.634	28.415	13.953	11.615	-50.871	-17.746
	0.650	0.640	0.890	1.030	0.660	0.630	0.600	0.880	0.680	0.650	0.670	0.700	1.260	1.400	1.660	1.390	0.960	0.890
	529	220	678	1017	936	593	605	667	824	2562	4098	5328	9296	10493	9034	8890	6734	3337
-10.00	-12.824	-19.487	-5.677	4.956	11.406	8,872	11.122	10.028	5.596	3.443	19.344	11.760	-22.627	20.963	11.312	-4.082	1.060	-62.465
10100	0.610	0.680	0.580	0.710	0.790	0.550	0.580	0.630	0.630	0.480	0.680	0.650	1.020	0.970	1.280	1.180	1.270	1.060
	365	193	600	1225	997	466	488	512	447	622	1565	3377	6258	7981	9365	10231	9609	9045
-20 00	-14 585	-10.042	-10.705	-20.886	-11.066	3,410	5.741	8.395	7.129	9.872	11.493	10.513	-49.670	-34.606	14.232	-10.247	-44.300	-34.483
20.00	0 700	0.460	0.640	0.530	0.440	0.360	0.580	0.620	0.520	0.490	0.430	0.760	0.850	1.080	1.090	1.270	1.700	1.880
	319	450	986	1598	1288	655	336	259	118	214	443	1458	2981	4904	5966	5284	6562	9320
-30 00	0 259	12 345	11.574	-9.243	-12.353	-2.551	4,460	4.531	7.765	7.128	5.461	7.558	6.975	-29.091	-38.678	-0.548	-12.000	-23.523
- 50 . 00	0.235	0 890	0.490	0.710	0.500	0.630	0.560	0.580	0.640	0.530	0.650	0.600	0.820	0.890	0.800	0.680	1.370	1.360
	699	1110	1408	1441	957	503	177	124	68	72	128	931	2269	2476	3151	3335	2773	3828
_40_00	13 502	13 820	16 652	8 510	-1.176	1.321	2.438	1.603	2.529	1.582	0.112	-1.173	4.121	6,194	-11.925	-24.062	-37.364	-40.464
10:00	0 970	1 020	0 860	0 800	0.770	0.680	0.670	0.540	0.670	0.580	0.650	0.550	0.510	0.650	0.600	0.650	0.660	0.670
	790	943	792	194	171	162	115	70	45	4.0	39	78	550	831	1121	983	949	1198
-50 00	25 120	19 589	14 101	12 105	8 637	7.678	7.510	4.392	1,161	-2.402	-6.591	-7.758	-3,906	2.647	7.270	2.518	-9.528	-22.782
-30.00	1 070	1 020	1 020	0 860	0.037	0 760	0 710	0 660	0.530	0.630	0.600	0.540	0.510	0.530	0.550	0,610	0.560	0.710
	1.070	1.020	1020	0.000	6.070	68	61	36	24	21	34	170	233	190	200	217	176	186
CO 00	203	15 064	15 042	12 000	11 616	10 200	10 210	0 772	6 310	2 2 2 1 2	2 1 9 2	-10 221	_12 089	_6 962	-0 681	5 253	6 218	1 304
-60.00	9.098	1 1 1 1 0	10.043	1 050	11.010	10.300	0 700	9.772	0.310	2.7.2	-5.105	-10.221	-12.005	0.510	0.560	0 570	0.590	0 630
	1.070	1.110	1.070	1.050	0.900	0.000	0.790	0.720	0.700	0.030	0.590	201	260	252	146	144	126	0.050
70 00	300	74	32	12 070	44	11 205	10 766	10 707	0 0 0 0 0	202	F 100	2 002	2 071	6 002	6 195	2 102	2 0 2 0	5 5 2 1
-/0.00	2.52/	5.996	10.116	12.070	12.101	11.395	10.766	10.797	9.828	7.342	5.123	2.092	-2.00/1	-0.903	~0.400	-2.402	3.029	0.570
	1.210	1.290	1.240	1.150	1.080	0.950	0.820	0.750	0.//0	0.790	0.660	0.610	0./50	0.810	0.720	0.020	0.530	1.40
	164	94	86	111	82	73	126	318	394	241	131	312	3/1	12 469	10 050	1 050	206	20 020
-80.00	10.132	5.119	8.145	8.128	8.445	7.548	7.419	11.116	12.613	4.902	6.011	18.033	20.582	13.468	10.950	1.050	/.013	20.838
	2.190	2.870	2.650	1.220	1.160	0.670	0.090	0.180	0.460	1.870	0.910	1.170	2.680	3.280	2.130	1.650	0.550	0.620
	130	111	111	133	104	73	16	24	74	86	99	216	773	926	612	173	234	240

		170 00	160 00	150 00	140 00	-130 00	-120.00	-110.00	-100.00	-90.00	-80.00	-70.00	-60.00	-50.00	-40.00	-30.00	-20.00	-10.00
	-180.00	-1/0.00	-160.00	-150.00	15 750	23 036	-24 190	-17.196	-14.248	4.104	12.533	6.869	6.170	-4.502	-24.750	-27.351	6.856	17.527
80.00	-1.839	38.///	39.066	18.000	-13.733	1 050	0 900	1 340	0.490	0.460	0.980	0.710	0.380	0.420	0.620	0.700	0.920	0.610
	0.900	0.980	1.370	1.070	1.090	1.010	524	738	880	951	926	744	617	631	623	725	802	949
	1114	1151	1158	1063	/42	2 4 0	0 671	16 222	16 926	-16 068	-6.619	1.781	3.439	4.489	-0.077	-12.393	-19.922	-7.250
70.00	-17.716	-7.646	15.910	27.003	22.675	3.924	-0.0/1	-10.222	0 950	0 750	0.700	0.800	0.860	0.720	0.690	0.720	0.740	0.730
	1.040	1.050	0.990	0.710	0.880	1.030	1.010	1000	1156	1262	1239	951	888	929	1045	1532	2521	3752
	2909	2726	2984	2950	2190	1529	12/3	1009	1120	15 9/0	_18 857	-10.572	-5.328	-0.352	4.640	6.008	-1.744	-10.944
60.00	9.520	6.651	6.994	14.382	21.781	20.870	10.485	-0.220	-9.033	0 650	0 830	0.670	0.720	0.640	0.890	0.780	0.650	0.690
	0.720	0.860	0.820	0.810	0.//0	0./10	0.690	1070	1712	1531	1303	992	956	865	1513	2630	4051	4731
	10617	9945	7144	5297	4150	3413	2720	10/0	1/12	14 71	_13 208	-11.283	-7.557	-4.025	0.977	13.560	19.876	6.892
50.00	27.991	29.261	25.328	17.512	9./18	8.423	15.415	0.995	0.550	0 510	0.500	0.450	0.540	0.620	0.510	0.480	0.790	0.630
	0.680	0.570	0.680	0.520	0.630	0.650	0.590	0.440	2110	2223	1413	1000	902	893	2366	5069	5775	6372
	10385	8724	6342	4772	4595	5/55	11 042	4010	22 260	11 737	_15 607	-4.333	-3.430	-11.711	-10.178	5.956	19.240	6.573
40.00	30.603	24.967	21.263	9.044	5.519	3.545	11.043	3.055	-22,209	0 530	0 490	0.500	0.320	0.470	0.490	0.430	0.570	0.310
	0.630	0.610	0.490	0.390	0.620	0.490	0.510	1577	2570	2426	1514	1117	934	943	2175	4654	4714	3681
	1678	2045	1946	2323	3502	5263	5051	4.577	כוככ רדי דר	2920	_7 181	-4.161	-5.391	-10.391	-33.364	-13.483	-1.498	6.721
30.00	27.466	20.534	17.905	-1.712	-11.712	-11./19	5.538	-2.839	-2/.//2	-20,500	0 600	0.450	0.450	0.420	0.420	0.390	0.350	0.430
	0.340	0.530	0.460	0.390	0.450	0.480	0.550	0.450	1500	5036	4126	2546	1521	1099	1367	1743	1565	1092
	1218	987	803	1513	2603	2949	21/9	2000	9152/	-36 968	10.232	22.778	-7,150	-16.691	-24.537	-33.188	5.678	24.667
20.00	16.941	17.419	13.581	3.709	-30.260	-6.851	-0.356	-2.341	-29.709	0.860	0 600	0.600	0.330	0.380	0.350	0.400	0.280	0.330
	0.440	0.470	0.510	0.590	0.690	0.580	0.470	10510	1100	6226	6341	4053	2430	1047	767	579	615	780
	706	653	606	1232	2129	2199	1216	1904	10 004	11 723	0 217	23 167	14.550	0.798	-2.199	-8.215	3.544	26.376
10.00	12.481	17.672	18.166	11.380	0.384	-14.959	-8.485	-1./18	-10.094	-44.723	0.217	0 650	0.400	0.320	0.230	0.330	0.360	0.360
	0.550	0.640	0.560	0.550	0.620	0.400	0.600	0.580	0.540	4120	6016	4393	2490	792	486	557	876	918
	585	510	655	834	889	636	613	1010	21/3	22 617	22 /1/	17 045	18.059	9.493	0.665	-5.331	-3.763	14.429
0.00	7.793	23.042	32.805	23.526	5,974	-8.194	-12.766	-6.697	-8.510	-23.317	- 52.414	0 620	0.470	0.420	0.320	0.400	0.300	0.380
	0.490	0.600	0.520	0.690	0.510	0.490	0.430	0.600	0.530	0.400	1021	3911	1484	428	473	649	884	807
	2245	2478	2456	1543	605	487	628	890	903	2247	37 260	16 457	8 872	4.269	-1.534	-9.205	-15.841	-9.000
-10.00	8.221	17.728	41.769	37.447	12.337	-15.458	-26.168	-16.507	-/.04/	-0.040	- 52.500	0 690	0.400	0.420	0.440	0.370	0.290	0.390
	0.500	0.720	0.650	0.530	0.580	0.360	0.620	0.530	0.540	110/	2115	3785	1397	579	332	382	544	527
	7786	6938	5548	3474	1654	1187	/82	832	14 200	L 104	9 607	-5 613	0.335	3,140	-1.523	-5.014	-19.447	-20.861
-20.00	24.975	14.844	35.297	33.421	15.352	-13.529	-25./81	-25./3/	-14.200	-5.401	-0.007	0 420	0.450	0.490	0.300	0.300	0.320	0.260
	0.600	0.580	0.640	0.590	0.570	0.500	0.660	0.820	0.510	0.470	2527	3191	1556	868	468	155	198	361
	8900	6642	4221	2605	1656	1351	99/	12 001	0 / 1 1	0 7 - 4	_1 412	-13.023	-3.730	-0.988	0.515	-0.318	-5.612	-12.219
-30.00	9.230	14.094	13.552	18.419	14.300	4.368	-8.188	-12.981	-9.411	0.704	0 440	0 350	0.450	0.370	0.420	0.250	0.260	0.300
	0.530	0.590	0.530	0.590	0.620	0.640	0.580	0.000	0.750	730	1281	1643	1385	975	568	56	232	585
	3193	1365	408	348	58/	566	507	523	0 553	2 912	2 950	-2.072	-7.988	-6.852	-6.194	-2.861	0.106	-8.017
-40.00	1.695	2.696	5.947	7.277	8.15/	6.202	3.004	0.990	0.552	0 670	0.480	0.390	0.450	0.520	0.440	0.300	0.340	0.360
	0.380	0.450	0.550	0.620	0.640	0.680	0.070	107	225	258	359	576	711	728	390	119	303	664
	728	298	62	51	67	4/	55	18/	1 505	1 1 1 6 A	4 356	2.373	-4.669	-6.677	-6.798	-10.469	-3.432	-1.406
-50.00	-5.457	-3.209	9 -2.158	1.386	4.06/	5.155	4.54/	4.004	4.070 0.500	0 5 8 0	0 610	0.540	0.390	0.400	0.390	0.430	0.370	0.380
	0.400	0.470	0.530	0.650	0.690	0.650	0.650	0.040	0.000	21	132	290	259	209	164	217	196	303
	210	126	5 54	49	9 67	4.8	t 1 ع	1 21) 5 173	5 014	4 839	3.486	0.550	-0.465	-0.899	-2.683	-0.845
-60.00	-1.207	-4.016	5 -5.039	-5.278	3 -1.276	5 2.630	4.930	4.85/	5.085	5.1/3	0 470	0.500	0.500	0.430	0.420	0.400	0.410	0.410
	0.360	0.390) 0.450	0.520	0.600	0.590	0.540	0.500	. 0.500) 0.490	50	75	7:	77	148	216	245	231
	81	. 42	2 31	. 29	9 23	3 15	9	5			E 107	, 5133	5 088	4.698	3,448	2.354	1.508	0.297
-70.00) 1.580	0.144	1 -2.073	-3.26	3 -2.876	5 -0.460) 2.468	4.953	5.080) 0.120	0.250	0 370	0 400	0.430	0.420	0.500	0.630	0.630
	0.380	0.380	0.410	0.400	0.380	0.320	0.210	0.000	0.180	. 0.290	0.550	1 15	10) 2	7 49	138	208	217
	37	20	26	34	4 31	1 22	13				1 0 5 3	2 5 114	5 223	5.78	8.335	7.848	4.884	4.742
-80.00	5.578	3.353	1 2.487	3.14	1 5.281	9.423	10.592	9.325) /.448	5) 1. C	4.903	0 100	0 180	0.450	0.630	0.350	2.770	2.230
	0.040	0.290	0.770	0.600	0.190	0.870	1.940	3.600	2.330	, 0.070	0.000	0.100	0.100	7 1	1 15	57	96	132
	86	100	9 113	138	8 190	175) 135) 72	2 I.	1 (, 4	r 0		Τ.	- 10	5,		

Depth = 1095 km

	0.00	10.00	20.00	30.00	40.00	50.00	60.00	70.00	80.00	90.00	100.00	110.00	120.00	130.00	140.00	150.00	160.00	1/0.00
80.00	-10.039	6.161	7.701	-26.390	-28.842	7.317	11.100	10.377	7.485	-0.035	-4.806	-6.199	-2.846	7.521	3.887	2.532	-18.168	-32.100
	1.180	0.780	0.730	1.660	0.760	0.790	1.440	0.980	0.740	0.920	0.510	0.690	0.590	0.540	1.660	0.580	0.640	1.290
	984	1488	2287	2873	2812	2306	2153	1803	1288	807	495	305	350	406	444	544	595	797
70.00	3.704	-5.103	-1,162	2.514	-12.515	-22.233	-9.798	-1.438	3.132	4.604	2.214	-0.926	-3.190	-3.058	2.103	3.367	3.767	-7.414
,0:00	0 780	0.840	0.760	0.690	1.080	0.990	0.810	1.070	1.030	0.960	0.970	0.780	0.750	0.760	0.790	1.080	0.820	0.750
	1219	6871	11435	13334	11863	8873	6356	3815	2428	1553	1142	799	770	910	1220	1698	1912	2300
60 00	-10 364	-1 787	-8 560	-3.661	1.898	-12.675	-21.397	-14,201	-7.544	-3.608	-1.012	0.335	-1.017	-5.259	-6.814	2.511	8.902	12.179
00.00	0 770	0 750	0 890	0 690	0.940	0.830	0.870	1.030	0.830	1.010	0.840	0.940	0.990	0.730	0.900	0.740	1.020	0.830
	5647	10554	14867	17009	15433	12093	8424	4663	3056	2185	1585	1300	1472	7621	10774	12076	9203	9138
50 00		7 134	_9 139	_32 492	-5.861	1.446	-22.133	-18,983	-9.563	-6.482	-9.892	-10.946	-11.222	-15.137	-23.567	-2.894	30.738	32.697
10.00	0.510	0 190	0 500	0 710	0 700	1.000	0.700	0.650	0.740	1.030	0.700	0.770	0.890	0.680	0.970	0.620	0.700	0.650
	4320	8226	12185	13704	11822	9772	7610	4813	3304	2878	2554	2347	3112	13350	17909	18860	11384	9865
40.00	6 090	_1 245	-5 066	-13.945	-16.943	5.754	-0.617	-34.046	-14,718	9.311	-9.784	-30.851	-27.751	-17.021	-19.172	-9.431	15.389	29.632
40.00	0.030	0 520	- 3.000	0 550	0 610	0 710	0.660	0.530	0.760	0.700	0.790	0.750	0.780	0.850	0.680	0.600	0.470	0.490
	0.440	1379	235/	5758	6384	6230	5645	4492	4276	4644	4036	3961	6291	13107	16471	12412	6216	3235
20 00	0 5 6 1	3 440	0 954	2 1 3 2	-6 090	-22 585	_12 390	-17.782	-21.568	6.404	3.473	-13,553	-29.497	-36.846	-9.557	-1.296	-2.773	26.516
30.00	0.304	0 450	0.354	0 490	0.000	0 560	0 410	0.520	0.460	0.520	0.690	0.640	0.830	0.860	0.890	0.730	0.460	0.390
	674	1077	1031	2395	2451	2565	2378	2016	3883	5491	5006	6526	9289	11519	11075	6304	3080	1523
20 00	10 202	2 5 2 1	1 1 2 2	_0 124	-5 901	_9_030	_32 385	_13 148	-11,192	-9.037	10.444	19.331	18,572	-10,145	-17.748	-20.052	5.808	7.953
20.00	19.292	-2.521	-1.120	-0.124	0 550	0 510	0 450	0 400	0 520	0.420	0.550	0.640	0.840	0.860	0.850	0.860	0.520	0.490
	0.440	0.440	1460	1709	1448	1257	1285	1013	3402	5293	5454	7572	9895	9745	8943	5842	2315	894
10.00	17 614	2 401	10 441	7 994	2 828		-18 073	_21 612	-10 286	7 035	12.568	24.587	36.777	-2.862	7,928	-14.881	2.187	13.048
10.00	1/.014	0 250	0 200	0 510	-5.050	0 700	0 510	0 380	0 390	0 580	0.570	0.800	0.740	0.850	1.020	0.740	0.690	0.940
	706	610	1240	1240	1000	1096	1088	805	2252	3363	4627	5691	8096	9861	9139	6672	2775	1095
0 00	11 270	E 000	1 1 4 9	7 222	0 100	0 9/9	-2 504	-10 357	_14 067	2 985	18 576	28.240	27.712	-12,131	-9.633	17.447	-20.386	0.482
0.00	11.3/8	5.099	4.400	7.252	5.400	0.049	0 5 8 0	-10.337	0 390	0 520	0 510	0.600	0.760	0.650	0.820	0.830	0.710	0.470
	0.390	1.04	0.400	1126	0.030	0.000	7/0	999	957	2146	2961	3910	6821	8630	8743	9094	6498	4249
10 00	400	104	0 0 1 0	1 712	2 000	1 624	1 155	3 2/1	-0 596	1 893	8 483	18 547	13.088	-5.120	-10.018	-0.470	-3.023	-6.588
-10.00	4.0/1	3.009	-0.010	-1./13	2.550	4.024	4.400	0 400	0 350	0 450	0.460	0 470	0.580	0.630	0.730	0.630	0.680	0.680
	0.340	0.270	0.210	1220	1111	0.550	528	607	514	601	1127	2283	4696	6436	7255	8729	8428	8818
20.00	1 (1 1	194	0 202	11 706	0 126	0 903	3 85/	5 118	5 047	4 354	5.449	11.273	1.710	7.230	5.050	-5,902	-7.505	-3,881
-20.00	-1.041	2.03/	-0.295	-11.790	-9.120	0.805	0 400	0 330	0 260	0 430	0 450	0 410	0.430	0.550	0.600	0.490	0.630	0.640
	0.320	0.230	672	1220	1172	775	173	202	2/3	311	537	1257	2650	4422	5207	5059	6029	8016
20.00	10 420	1 2 2 7	0/J E (10	1 240	6 501	2 261	1 / 1 2	2 1 5 9	3 870	1 482	3 282	4 471	12 778	10.218	1.953	-6.731	-11,951	7.435
-30.00	-10.439	0 240	0 240	-1.240	-0.301	-3.201	0 450	0 330	0 340	0 370	0.490	0.440	0.330	0.430	0.510	0.380	0.490	0.680
	0.200	0.340	0.240	0.520	0.510	5.17	3/5	133	80	97	199	763	1745	2178	2455	2497	2588	2982
10 00	11 202	0 001	6 000	1 1 1 2	0 8/5	0 202	1 701	1 958	1 625	1.238	0.322	-0.105	2,900	6.987	5,911	0.061	-10,126	-10.773
-40.00	-11.292	-0.091	0.090	4.442	0.040	0.202	0 320	0 350	0 380	0 300	0.350	0.370	0.360	0.310	0.390	0.460	0.380	0.390
	0.410	0.510	102	112	137	112	9.520	67	0.500 44	50	74	114	286	685	784	698	771	866
F0 00	0 1 2 0	0 1 1 6	2 201	1 552	1 222	2 5 4 7	3 070	3 683	2 134	0 6.94	_1 925	_4 555	-3.428	0.272	3.348	4.311	1,207	-3.978
-50.00	0.139	-0.440	2.501	4	4.525	0 420	0 350	0 330	0 330	0 380	0 350	0 310	0 310	0.310	0.320	0.370	0.400	0.370
	0.420	0.440	0.410	0.430	67	0.430	0.550	75	57	30	65	218	304	230	211	153	120	161
(0.00	2/3	1 211	2 100	2 1 1 7	1 267	1 000	5 254	5 772	5 0/9	3 / 1 8	1 376	_2 123	-5 300	_3 973	-1.922	0.500	2.342	1.854
-60.00	0.495	1.811	2.100	3.11/	4.207	4.070	0 420	0.200	0.260	0 320	0 240	0 350	0 350	0 340	0 350	0 370	0 380	0 370
	0.420	0.440	0.460	0.450	0.450	0.450	0.430	0.390	0.300	0.520	202	264	367	274	180	150	155	120
70.00	140	54	20	20	48	4 205	F 0 C A	239	540 E 070	E E 2 2	1 957	1 0 2 2	1 1 2 6	1 103	_1 801	_3 048	_1 596	0 815
-/0.00	0.58/	1.3/0	2.284	2.924	3.605	4.385	5.064	5.54/	0 200	0.250	4.007/	4.022	1.120	0 510	0 510	0 550	0.510	0.420
	0.580	0.570	0.590	0.570	0.490	0.430	0.400	0.400	0.300	204	250	235	504	704	582	755	177	142
0.0.00	148	126	125	7 540	7 222	2 ک د د د ع	7 402	7 650	202	7 604	7 800	10 810	14 810	-6 604	25 187	-7.596	-8.093	4.525
-80.00	5.789	0.385	1 (20	1.549	1.333	0.038	0 200	0 440	0 550	0 120	0 120	0 350	1 120	2 050	1 460	1 960	2.060	0.200
	1.390	1.280	1.620	1.6/0	0.8/0	0.330	0.390	0.440	0.550	70	100	152	5/2	2.000	601	455	2.000	170
	129	134	14/	130	99	19	31	30	20	19	109	100	740	163	0.74		201	110

-180.00 -170.00 -160.00 -150.00 -140.00 -130.00 -120.00 -110.00 -100.00 -90.00 -80.00 -70.00 -60.00 -50.00 -40.00 -30.00 -20.00 -10.00 1.282 -17.251 -41.912 -28.571 8.448 4.314 3.618 -8.495 -29.035 -24.154 10.525 44.540 28.279 80.00 41.789 33.335 21.714 13.948 4.881 0.940 0.730 0.780 1.040 1.010 1.080 1.270 0.920 0.840 1.020 0.970 1.460 1.050 0.810 1.740 1.460 1.260 1.180 992 957 1023 1184 1406 1718 1849 1505 1113 1117 862 646 894 1161 1185 1251 1242 1172 -0.850 -4.054 -15.058 -18.849 -5.274 17.073 -4.126 -25.268 -27.984 -11.139 -4.618 33.086 27.496 21.555 13.910 8.187 70.00 24.916 33.706 1.060 1.400 1.270 1.300 1.450 1.320 1.160 1.210 1.110 1.180 1.490 1.380 1.300 1.700 1.460 1.130 1.330 1.140 1177 1130 1317 1570 2023 2716 3650 3723 3173 2948 2176 1950 1489 1406 1496 1461 2489 2682 11.967 7.180 21.072 15.543 3.830 -13.786 -19.958 -18.361 -9.831 3.519 -7.262 -13.154 60.00 25.007 30.150 31.190 29.903 29.029 25.895 1.090 1.090 0.770 1.110 0.830 1.380 1.100 1.220 1.120 0.970 1.110 1.050 0.980 1.090 0.880 1.070 0.990 1.510 1726 1400 1050 1156 1670 2245 3010 4192 3876 4331 3285 2520 2075 2017 10313 8374 6390 5343 -5.504 -9.818 -16.521 -16.938 -1.876 22.837 36.931 21.344 -6.153 50.00 38.656 40.909 29.795 18.042 17.175 24.328 22.441 11.451 9.172 0.550 0.600 0.850 1.080 0.730 0.730 1.070 0.860 0.780 0.750 0.590 0.840 0.770 1.180 0.910 0.910 0.970 0.780 1234 2679 4007 4740 4618 2595 3566 2959 1958 1376 1015 10170 8436 6465 4851 4569 4392 4051 1.383 -5.026 -8.085 -11.883 -7.022 -17.449 -24.724 -6.055 26.955 19.679 10.600 40.00 29.164 28.846 23.868 10.817 17.759 12.236 11.658 0.570 0.640 0.920 0.690 0.590 0.730 0.650 0.790 0.610 0.800 0.660 1.000 0.720 0.510 0.670 0.640 0.950 0.790 2961 2754 2578 2958 3260 3679 3459 3311 3093 2721 1896 1257 1494 2859 4612 4708 3900 1480 4.755 -23.329 -43.208 14.091 -15.549 -21.076 -18.250 -8.922 -46.181 -45.774 -29.406 -2.095 20.653 11.597 7.650 14.945 30.00 30.078 30.326 0.950 0.540 0.700 0.820 0.860 0.880 0.810 0.620 0.730 0.560 0.510 0.460 0.890 1.070 0.810 0.790 0.950 0.980 1061 1754 3116 3927 3765 2899 2634 2140 2411 2306 1411 453 1695 1963 2564 2043 1464 1660 -49.671 -45.126 -34.194 -24.519 -14.878 6.182 -43.424 -35.995 -2.797 21.434 -7.386 -1.664 -1.798 22.476 26.342 20.00 35.073 27.242 15.957 0.930 1.050 1.100 0.990 0.860 0.630 0.530 0.680 0.840 0.610 0.530 0.500 0.630 0.600 0.560 0.880 0.790 0.930 3652 1911 1297 641 338 361 2814 1849 820 1183 3126 4919 5126 4459 1243 1220 1670 2645 22.879 3.185 -3.551 -1.333 -3.871 10.00 28.532 26.659 18.259 -16.561 6.213 6.196 10.910 17.394 - 29.745 - 57.908 - 33.140 11.441 -6.514 0.540 0.910 0.650 0.480 0.490 0.580 0.570 0.540 1.080 1.100 0.770 0.840 0.990 0.880 0.700 0.960 0.890 0.840 656 501 421 346 977 1764 2690 3996 3847 2756 1251 1277 1225 2001 2370 2071 1043 674 23.310 -2.159 2.224 2.217 14.193 -1.293 -49.327 -52.610 -2.257 7.835 12.199 5.661 4.805 3.493 2.049 0.555 16.556 33.491 0.00 0.650 0.560 0.760 0.740 0.920 1.090 0.960 0.710 0.810 0.660 0.680 0.650 0.620 0.450 0.790 0.600 0.840 0.620 4091 4101 3267 2556 848 610 722 847 1100 2099 2998 3260 1502 710 527 574 546 381 2.833 0.484 14.442 12.234 -6.776 -24.583 -1.352 9.572 7.935 0.686 -11.109 -6.794 1.158 -2.718 39.623 30.560 24.314 -10.00 39.538 0.910 1.050 0.900 0.610 0.620 0.660 0.570 0.620 0.650 0.600 0.520 0.500 0.920 1.200 0.760 0.820 0.790 0.760 1010 796 752 558 1439 2551 2931 1081 634 423 390 357 342 7439 6586 5215 3180 1260 7.884 14.697 -2.428 9.741 3.712 -9.703 -19.782 -28.511 -0.461 35.934 34.882 26.142 15.096 0.266 5.369 9.456 -20.00 54.306 37.137 1.050 0.870 0.910 0.900 0.790 0.900 0.750 0.560 0.550 0.540 0.600 0.670 0.430 0.510 0.480 0.490 0.840 0.860 997 865 689 755 1912 2064 1016 819 591 355 289 280 7136 5142 3083 1522 1292 1274 -2.581 -11.249 -26.181 -41.322 -30.00 22.685 26.008 23.295 25.743 24.691 24.645 20.979 18.679 22.433 15.553 2.241 -8.547 0.297 -7.606 0.860 1.000 1.110 1.150 0.970 0.930 0.860 0.910 0.700 0.450 0.420 0.530 0.570 0.560 0.500 0.500 0.510 0.630 271 239 460 556 542 554 594 481 771 866 1105 990 838 597 772 891 1845 889 16.697 17.145 17.798 18.474 16.300 7.680 -12.658 -22.736 -14.347 -27.913 -42.210 -40.406 -30.966 5.709 11.894 13.930 15.568 17.451 -40.00 1.190 1.210 1.060 0.980 0.860 0.810 0.720 0.470 0.380 0.570 0.540 0.430 0.450 0.550 0.970 1.070 0.620 0.760 597 68 68 85 169 237 241 204 196 396 715 835 793 669 810 880 324 48 8.930 10.775 12.161 12.931 13.902 14.638 15.007 13.920 7.795 -7.459 -3.958 -5.194 -19.334 -20.634 -15.687 -50.00 0.982 3.711 6.635 0.570 0.690 0.820 0.950 1.060 1.130 1.160 1.120 1.040 0.940 0.840 0.720 0.580 0.520 0.510 0.560 0.500 0.520 28 47 61 42 23 26 21 50 142 290 321 338 291 239 235 251 205 110 4.077 6.844 10.518 11.640 12.555 13.299 14.061 14.222 12.347 6.971 7.099 5.690 -0.527 -3.249 -60.00 -2.287 -1.361 0.993 8.908 0.860 1.030 1.050 1.050 1.020 0.950 0.860 0.760 0.660 0.620 0.550 0.550 0.560 0.640 0.700 0.770 0.960 0.610 16 18 19 10 8 6 25 47 103 121 85 108 121 125 134 96 77 22 -70.00 -3.769 -4.018 -2.456 0.632 3.874 6.815 9.257 10.698 11.453 12.100 12.631 13.273 13.816 13.470 11.107 10.185 9.224 5.952 0.770 0.700 0.640 0.680 0.770 0.780 0.780 0.740 0.700 0.680 0.680 0.730 0.810 0.840 0.840 0.850 0.850 0.830 24 27 27 82 132 205 198 62 14 18 39 37 29 23 27 36 14 32 15.101 20.296 20.191 13.706 12.744 11.912 12.711 14.344 14.462 14.374 15.768 -80.00 -10.404 -1.722 4.387 8.621 13.736 11.847 13.477 1.090 0.850 0.330 0.370 0.730 0.490 0.140 0.120 0.190 0.250 0.210 0.300 0.180 0.670 2.130 2.610 3.220 1.910 50 41 82 109 117 191 193 147 92 24 7 5 8 14 23 60 120 156

90.00 100.00 110.00 120.00 130.00 140.00 150.00 160.00 170.00 70.00 80.00 0.00 10.00 20.00 30.00 40.00 50.00 60.00 -5.091 -13.729 -31.375 -5.069 -0.392 18.479 3.839 2.149 -7.222 37.250 16.883 -41.365 -55.196 -41.286 -10.159 23.207 80.00 -10.246 -18.438 2.100 2.070 1.410 1.310 1.230 1.400 1.260 0.940 1.400 0.920 1.170 1.080 1.920 1.500 2.000 1.330 1.450 1.350 1058 785 669 670 803 953 5419 5739 5793 4959 3747 2631 1676 1368 1183 1428 2963 4596 11.247 -15.624 -44.344 -43.463 -33.354 -18.767 -11.663 -11.942 -11.011 -14.082 -22.546 -12.969 -4.864 9.342 70.00 20.568 4.209 -8.478 5.918 1.380 1.640 1.520 1.370 1.260 1.500 1.680 1.520 1.470 1.320 1.360 1.300 1.600 1.440 1.230 1.560 1.360 1.370 8226 5845 3912 3020 2727 4303 4232 3498 2673 2559 13707 10941 3123 5312 10022 13692 15149 14826 -3.782 8.148 -3.594 -32.821 -40.181 -39.326 -31.574 -25.464 -26.363 -33.049 -27.910 -22.107 60.00 -5.521 8.613 1.478 -12.184 -0.843 15.271 1.250 0.900 0.990 1.050 0.840 1.020 1.120 1.180 1.060 1.210 1.110 1.130 1.120 1.110 1.130 1.250 1.240 1.080 4877 3867 3391 5455 10797 12337 9859 8669 8995 10179 6696 10603 13968 15745 15258 13091 3265 5531 -2.006 -17.036 -43.582 -27.058 -11.248 -6.737 -27.321 -27.993 -35.844 -40.401 -44.285 -51.145 -52.218 -39.671 3.595 38.467 50.00 -7.982 -8.180 0.990 1.000 1.020 1.050 0.930 0.900 0.900 0.890 1.050 1.020 0.870 0.850 1.120 0.840 0.800 1.020 0.660 0.810 14975 17668 12983 10054 9505 2886 2385 2289 4669 1356 1955 4358 6053 7258 7744 7054 6076 4048 -9.739 -14.622 -25.674 -43.316 -44.522 -34.287 2.707 -4.439 -22.473 -45.165 -49.679 -50.585 -55.015 -52.364 -39.624 7.936 40.00 -0.326 -5.860 1.140 1.110 0.910 0.770 0.740 0.880 0.920 0.960 1.000 0.710 0.690 0.650 0.840 0.640 0.990 0.630 0.680 0.480 12432 5417 3751 2803 4082 4274 4274 4154 4288 3971 2920 3943 6064 11587 7160 306 536 1487 -36.498 -42.210 -44.977 -28.044 19.085 -2.432 13.200 2.993 -31.812 -38.956 0.347 -11.665 -16.324 -16.594 -18.247 -39.970 -46.260 -34.735 30.00 1.160 0.910 0.830 0.940 1.000 0.820 0.740 1.040 1.150 0.550 0.570 0.430 0.490 0.620 0.530 0.510 0.660 0.740 4326 3480 5506 7410 9390 9126 5867 3372 1775 2592 3763 289 573 993 1364 1782 2072 1984 -6.840 -10.603 -20.749 27.464 47.210 47.530 7.914 -26.538 -25.548 10.775 -9.337 -33.692 -28.740 -20.508 -23.968 -45.865 -43.573 20.00 -2.035 0.730 0.650 0.820 0.830 0.740 0.920 0.790 0.860 0.730 1.070 1.070 1.270 0.980 0.520 0.390 0.430 0.640 0.550 6882 3739 1790 3727 6455 7935 8344 8937 1315 2945 4052 860 1181 1043 983 1008 401 545 40.413 44.967 67.278 18.019 -4.18924.651 10.00 -5.160 -0.470 -19.141 -38.618 -39.235 -36.940 -35.218 -54.043 -44.809 -12.890 -11.185 18.076 0.650 0.760 0.700 1.040 0.990 0.960 0.850 1.900 0.850 0.610 0.610 0.860 0.750 0.550 0.570 0.680 0.470 0.540 6861 8644 8720 7243 4441 2309 982 998 850 2155 2836 3388 4861 383 429 824 925 889 -0.664 -36.755 -39.177 -31.419 -14.336 -21.553 -29.620 -14.358 -4.393 -4.811 10.168 -12.096 29.750 13.167 10.808 -17.340 0.00 1.570 3.415 0.630 0.900 0.680 0.890 1.070 0.810 0.480 0.630 0.810 0.570 0.490 0.530 0.550 0.550 0.680 0.770 0.510 0.580 7587 8315 8635 6834 5457 518 972 899 1034 929 803 886 1384 1926 3263 5584 322 163 20.272 8.803 3.633 30.002 -6.189 -5.119 0.267 -6.981 8.036 12.167 29.602 6.320 -24.741 -41.163 -20.121 -4.673 -10.00 6.818 4.835 1.040 0.490 0.6:0 0.590 0.470 0.640 0.530 0.770 0.800 0.650 0.540 0.500 0.500 0.580 0.560 0.690 0.720 0.610 746 546 599 752 1545 3292 5175 5447 6880 7841 7706 993 965 970 602 269 168 445 3.151 15.735 44.798 52.222 24.478 5.747 4.563 23.949 -6.203 -20.452 -17.611 -3.210 2.650 2.363 1.949 -20.00 11.932 11.419 7.995 0.580 0.570 0.500 0.660 0.620 0.530 0.500 0.530 0.460 0.470 0.660 0.460 0.890 0.590 0.660 0.530 0.600 0.530 592 1023 2351 3752 4109 4214 5276 6186 1051 741 643 466 394 423 223 192 421 884 38.635 29.558 -1.284 -12.410 3.092 18.532 12.703 5.954 -2.579 -4.793 -2.362 1.851 1.967 1.355 0.519 3.972 22.181 -30.00 18.677 0.550 0.530 0.650 0.540 0.640 0.660 0.550 0.580 0.530 0.470 0.640 0.520 0.440 0.440 0.690 0.670 0.640 0.650 1974 2241 434 312 183 171 233 588 1284 1685 1925 2077 834 689 169 243 551 505 4.111 0.555 -0.172 1.813 11.704 16.127 10.043 -2.914 -5.429 7.435 2.979 3.375 2.162 -0.562 -40.00 -0.958 15.116 14.974 11.433 0.710 0.740 0.660 0.520 0.570 0.430 0.470 0.550 0.480 0.470 0.640 0.770 0.750 0.740 0.680 0.720 0.790 0.800 93 85 70 55 40 58 110 195 245 407 600 595 595 628 786 623 69 64 -3.457 -1.798 1.935 3.793 4.653 3.239 1.199 6.359 6.202 5.130 2.650 -1.000 -50.00 -7.720 3.325 9.705 11.214 10.714 8.336 0.550 0.550 0.500 0.500 0.530 0.560 0.570 0.680 0.780 0.830 0.840 0.840 0.830 0.790 0.760 0.740 0.640 0.560 88 216 297 244 224 113 76 150 24 42 64 86 107 164 140 144 60 19 -2.884 0.391 1.707 0.647 -0.595 -1.920 9.767 10.623 10.090 9.401 9.406 7.346 4.844 1.253 -60.00 -2.948 -0.600 3.616 7.481 0.700 0.760 0.790 0.810 0.820 0.790 0.750 0.720 0.670 0.630 0.620 0.590 0.580 0.550 0.560 0.650 0.610 0.640 299 244 140 150 21 30 71 85 205 337 382 301 394 448 140 41 36 61 3.356 5.434 4.580 0.704 -1.688 7.246 9.534 10.748 10.974 10.900 10.836 9.744 8.422 5.567 -70.00 3.185 2.202 2.760 4.626 0.750 0.740 0.680 0.680 0.650 0.650 0.680 0.710 0.790 0.670 0.730 0.700 0.710 0.680 0.630 0.650 0.670 0.730 787 524 276 187 330 340 296 320 484 651 127 143 130 147 126 100 46 47 14.204 16.189 17.647 16.116 18.009 1.320 37.089 34.212 -2.009 -10.040 15.262 15.840 14.608 14.603 16.366 16.346 14.064 -80.00 13.317 0.240 0.100 0.830 0.860 1.460 2.570 0.560 2.450 2.840 1.810 1.220 1.120 1.510 0.520 0.340 0.680 0.330 0.570 139 120 99 46 39 56 52 60 89 137 385 763 765 567 254 89 137 126

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	-180.00	-170.00	-160.00	-150.00	-140.00	-130.00	-120.00	-110.00	-100.00	-90.00	-80.00	-70.00	-60.00	-50.00	-40.00	-30.00	-20.00	-10.00
80.00	0.810	-9.790	-14.392	-1.029	14.252	5.864	-4.081	-16.193	17.983	25.016	14.133	7.394	-0.277	-3.803	-7.918	-12.611	-23.732	9.100
00000	1.020	0.870	0.800	0.720	0.780	1.070	1.330	0.760	0.520	0.600	0.750	0.880	0.750	1.310	1.770	0.890	2.030	0.950
	904	820	796	973	1460	1654	1818	1830	1757	1619	1658	1688	1813	2249	2814	3182	2950	1954
70.00	20.620	11.424	1.467	-5.497	-2.540	6.094	5.562	-0.384	-9.625	2.615	11.990	11.854	9.429	4.953	0.762	-3.934	-9.260	-18.106
	1.220	1.170	1.020	1.000	0.860	0.830	1.040	0.860	0.870	0.940	0.750	0.890	0.970	1.000	1.040	1.350	1.150	1.500
	2981	3325	3316	2862	2291	1986	2037	1929	1859	1742	1755	1891	1998	2606	3234	3684	3507	2997
60.00	34.328	26.462	16.752	9.881	7.344	6.134	6.607	5.608	-0.193	-7.594	-6.014	1.196	8.863	13.918	11.797	4.467	-2.818	-10.219
	1.030	1.000	0.920	0.960	0.930	0.960	0.780	0.770	0.710	0.740	0.760	0.670	0.450	0.680	0.700	0.580	0.650	0.750
	8753	7106	5807	4956	3655	2465	2331	2019	2026	1878	1488	1521	1693	1865	1968	2302	2621	2575
50.00	41.641	34.809	16.532	5.269	6.771	9.609	-1.649	-2.401	-1.339	-9.328	-16.377	-7.990	8.239	25.992	28.418	18.749	7.859	-0.820
	0.780	0.810	0.670	0.820	0.830	0.750	0.850	0.710	0.860	0.770	0.780	0.660	0.470	0.480	0.580	0.480	0.440	0.390
	9308	7866	5620	4090	3649	2779	2505	2458	2262	1840	1366	1842	2570	3194	3624	3671	1825	426
40.00	13.354	14.441	5.611	7.495	3.948	-2.606	-16.259	-14.827	-7.278	-14.238	-18.117	-0.748	24.895	45.152	46.809	31.125	13.590	3.483
	0.880	0.670	0.620	0.620	0.650	0.770	0.810	0.720	0.770	0.970	0.820	0.770	0.620	0.650	0.690	0.530	0.410	0.340
	3169	2977	2776	2287	2388	1864	1663	1902	1920	2231	2303	2835	3324	4238	4409	3811	2054	130
30.00	8.186	16.149	18.688	7.981	5.107	-1.467	-23.424	-30.428	-3.936	-4.265	-2.588	26.220	39.331	25.672	10.734	0.150	5.354	0.263
	0.530	0.820	0.710	0.710	0.660	0.650	0.840	0.730	0.620	0.640	0.810	0.890	0.760	0.680	0.510	0.480	0.370	0.400
	1998	2088	1910	1670	1977	1230	564	783	1570	2562	2896	3448	3872	3797	3058	2031	927	110
20.00	23.011	27.578	21.708	29.995	7.895	15.393	-11.005	-17.151	2.371	11.586	9.773	17.999	20.951	11.890	-14.941	-11.377	-7.877	-4.842
	0.600	0.400	0.610	0.740	0.780	0.690	0.740	0.760	0.620	0.560	0.570	0.600	0.680	0.590	0.420	0.320	0.360	0.420
	1697	2018	2577	2847	2376	1390	609	650	1546	2846	3110	3724	3187	2543	1824	620	207	142
10.00	1.072	26.366	42.670	45.283	34.621	12.491	5.357	3.745	2.390	9.230	14.989	15.751	15.799	6.362	-1.791	-9.119	-8.850	-5.864
	0.830	0.650	0.670	0.710	0.620	0.820	0.800	0.740	0.600	0.590	0.650	0.710	0.670	0.540	0.510	0.500	0.430	0.420
	2349	2413	3673	3118	1915	925	653	779	1177	1611	1824	2312	2186	1233	619	341	120	153
0.00	-53.963	13.790	24.001	47.731	21.178	6.741	3.436	11.279	1.394	-2.088	11.167	21.167	7.791	3.746	1.264	0.256	-0.221	-0.441
	0.810	0.680	0.890	0.530	0.510	0.570	0.820	0.730	0.600	0.580	0.630	0.680	0.690	0.570	0.460	0.530	0.520	0.490
	4142	4170	3622	2901	1339	602	693	714	931	1448	1790	1590	1096	569	435	243	150	119
-10.00	-38.331	-22.662	9.431	12.052	18.840	10.056	3.518	6.855	4.525	-8.801	0.716	12.243	7.515	1.02/	1.505	2.160	4.082	3.554
	0.620	0.510	0.610	0.490	0.500	0.690	0.750	0.770	0.640	0.580	0.590	0.550	0.610	0.620	0.610	0.420	0.460	0.480
	5545	5576	4124	2443	716	761	586	570	485	1123	1577	1191	496	41/	309	206	213	7 0.00
-20.00	5.172	-1.566	2.647	3.415	5.648	11.990	12.423	10.240	8.282	1.994	1.109	4.384	2.221	-0.955	4.150	2.012	0.0/3	/.900
	0.560	0.390	0.670	0.590	0.560	0.590	0.580	0./30	0.690	0.540	0.550	0.580	0.550	0.460	0.4/0	0.490	0.400	0.400
	3954	3456	1836	84/	598	852	628	518	304	63/	969	/3/	292	2 202	2 402	6 256	1 407	14 201
-30.00	9.293	5.212	1.930	3.570	3.976	6.//4	13.504	15.439	11.803	8.928	0./33	4.994	2.398	-2.293	2.492	0.500	0.420	0 / 20
	0.510	0.450	0.440	0.590	0.660	0.840	0./50	0.560	0.540	0.500	0.500	106	0.000	0.550	0.440	680	788	926
	1139	643	1/5	2 1 7 9	185	397	1 5 2 1	7 616	0 071	0 107	1/4 0 501	190	204 5 777	0 359		_9 075	-7 050	2 959
-40.00	0.553	5.400	3.810	3.1/9	3.384	3.220	4.531	/.015	0.0/1	0.402	0.521	0.723	0 370	0.330	0 420	0 410	0.430	0.460
	0.480	0.440	0.510	0.510	0.530	100	0.740	0.730	170	0.570	1/2	313	417	697	774	747	828	825
F 0 0 0	2 210	1 210	2 201		2 601	2 756	107	4 410	5 306	6 53/	7 647	0 333	8 799	8 086	4.401	0.170	-2.418	-1.458
-50.00	-2.210	1.210	3.204	3.309	0 510	0 510	0 5 2 0	4.410	0 590	0.540	0 500	0 480	0 450	0.000	0 400	0.370	0.400	0.410
	0.400	122	0.430	0.500	0.510	0.510	0.530	0.570	0.530	50	178	284	296	331	321	235	217	172
60 00	239	123	1 704	2 9 7 7	2 2 2 0	3 633	3 9/7	1 227	4 481	4 955	5 814	6 567	7.466	7.771	7,939	6.448	3.972	1.821
-00.00	0.4/9	0.003	0 440	0 110	0 450	0 470	0 500	0 530	0 540	0 550	0.520	0.470	0.440	0.430	0.410	0.400	0.410	0.440
	102	10	11	12	0.400	10	0.500	11	46	61	142	178	126	137	139	137	98	54
70 00	3 031	2 255	1 976	2 178	2 607	2 960	3 705	4 672	4.996	4.831	4.802	5.157	5.657	6.263	6.645	7.016	6,487	5.035
-70.00	0 340	0 340	0 330	0 340	0 360	0.370	0.400	0.440	0.470	0.460	0.460	0.450	0.430	0.420	0.450	0.470	0.510	0.520
	60.540	0.540	11	21	21	21	22	22	29	30	40	29	29	73	99	116	129	124
-80.00	4.124	4.816	5.352	4.604	3.254	2.292	2.605	11,105	11.896	6.304	4.438	3,913	4.208	4.142	3,952	3.471	5.834	3.258
00.00	0.320	0.190	0.200	0.160	0.280	0.390	0.390	0.530	0.640	0.170	0.150	0.150	0.190	0.280	0.590	1.190	1.060	1.860
	47	41	35	51	81	110	219	200	147	88	7	10	19	36	54	81	122	125

70.00 80.00 90.00 100.00 110.00 120.00 130.00 140.00 150.00 160.00 170.00 50.00 60.00 0.00 10.00 20.00 30.00 40.00 3.372 33.354 23.257 -16.148 -60.794 -63.407 -57.322 -52.493 -44.556 5.210 -11.933 34.117 34.280 12.703 4.514 80.00 9.663 -6.521 -16.577 1.660 1.250 0.900 1.090 1.190 1.250 1.270 1.630 1.280 1.520 1.230 1.960 0.710 1.070 0.730 1.370 0.900 1.570 6527 5329 3736 2022 1084 819 759 906 7975 7722 7367 951 900 2703 5017 6325 7185 7679 -2.638 -3.427 -44.867 -56.012 -56.579 -55.024 -51.598 -30.806 -1.501 1.208 17.511 26.317 70.00 -5.973 0.849 -3.539 - 10.723-3.851 8.952 1.460 1.370 1.310 1.040 1.360 1.000 0.960 1.210 1.150 1.220 1.360 1.500 0.920 0.930 1.060 1.220 1.160 1.280 11723 10805 9696 6273 4150 3298 2972 16043 16144 15089 13631 12600 1828 2229 5145 9821 12841 14877 -2.843 -31.240 -48.216 -50.563 -51.136 -51.388 -42.834 -17.229 14.631 -5.095 29.454 -6.080 -6.933 -13.485 -8.008 5.572 60.00 -20.159 -13.251 1.150 0.780 0.970 0.930 0.870 0.860 0.790 0.900 1.110 1.010 0.650 0.750 0.730 0.880 0.940 0.880 0.810 0.990 13419 6881 6784 7999 10171 12531 13504 12937 11692 10079 9479 10249 11381 12882 1610 2039 4514 8222 -7.493 -15.654 -28.062 -33.216 -27.477 -22.225 -29.870 -22.481 -6.327 9.196 -9.942 -9.777 -14.903 -30.297 -19.304 33.736 50.00 -7.569 -11.185 1.010 0.720 0.770 0.770 0.770 0.750 0.560 0.690 0.790 0.990 0.880 0.880 0.550 0.550 0.610 0.590 0.550 0.790 2214 2570 7541 14623 15899 6972 7350 8962 1958 3217 5319 6194 6507 5755 3758 320 342 826 -13.791 -20.853 -10.664 -14.813 -42.441 -51.283 -37.627 -0.456 8.719 -19.072 -14.039 -8.527 -4.542 40.00 -2.381 -4.938 -5.771 -10.603 -17.438 0.720 0.690 0.700 0.660 0.680 0.830 0.900 0.930 0.910 0.690 0.710 0.590 0.350 0.430 0.450 0.540 0.560 0.270 5219 9341 9215 4890 4645 3898 4809 4294 3236 2614 3662 177 576 1359 2315 3358 4345 104 -10.827 21.123 22.579 -14.569 -3.857 8.506 30.00 -5.812 -8.658 -5.371 -4.201 -20.648 -30.645 -22.285 -9.212 -8.959 -29.033 -47.410 -51.984 0.930 0.800 0.820 0.850 0.690 0.580 0.550 0.700 0.900 0.220 0.360 0.440 0.510 0.580 0.560 0.540 0.490 0.270 6421 5105 3521 2258 3265 3811 3252 3153 4660 5968 6680 108 213 534 803 1124 1677 2320 -14.585 -44.467 -25.199 2.537 -18.209 -34.933 -22.378 -9.037 22.225 37.042 20.302 -16.763 8.635 -8.944 1.703 20.00 -8.154 -9.950 0.217 0.480 0.490 0.400 0.660 0.740 0.810 0.820 0.790 0.900 0.600 0.610 0.300 0.450 0.510 0.570 0.600 0.400 0.260 442 662 639 724 1180 1837 2407 2812 2606 4100 5214 5852 6720 6261 4129 2645 164 238 1.590 -14.038 -38.822 -23.264 -15.100 -28.007 -32.370 -19.207 -5.477 24.824 18.587 -20.680 -37.010 0.415 10.00 -5.634 -4.244 -5.694 2.333 0.570 0.590 0.720 0.750 0.940 0.930 0.890 0.410 0.320 0.370 0.550 0.580 0.640 0.690 0.580 0.410 0.330 0.430 2200 3448 4950 6042 7115 6495 4672 3079 678 760 945 1772 2159 156 198 395 486 697 -8.021 -13.504 -11.573 -12.489 -27.283 -25.710 4.590 10.165 -0.375 -13.664 -59.571 0.00 -0.574 0.235 2.307 2.729 -1.287 -4.331 -1.240 0.550 0.590 0.490 0.370 0.320 0.340 0.380 0.520 0.640 0.730 0.760 0.820 1.070 0.490 0.520 0.490 0.580 0.630 5394 6690 6417 6212 4505 287 532 631 730 735 622 539 680 1038 2106 3760 126 142 17.191 4.844 1.706 2.754 2.334 3.103 3.037 -3.604 -5.362 -9.892 -11.070 -5.108 -5.186 -7.617 -4.936 1.523 24.819 31.037 -10.00 0.640 0.680 0.570 0.880 0.630 0.610 0.500 0.370 0.370 0.370 0.260 0.420 0.360 0.500 0.500 0.510 0.640 0.480 4930 5358 410 536 691 608 497 497 451 446 1024 2060 3594 4200 6078 145 143 205 2.025 0.398 -6.615 -10.594 -8.161 -6.202 -3.195 -2.236 1.493 13.356 19.728 8.730 7.414 1.494 6.752 4.768 3.369 1.798 -20.00 0.380 0.560 0.620 0.630 0.530 0.480 0.480 0.460 0.390 0.350 0.460 0.420 0.420 0.560 0.560 0.650 0.520 0.530 120 241 489 615 582 514 422 400 406 680 1473 2438 2532 2826 3504 4079 134 110 -2.683 -5.192 -3.555 -1.528 -0.607 2.322 2.997 11.018 5.987 -6.923 -13.423 -2.408 2.159 0.324 -4.015 -30.00 9.356 4.214 2.828 0.500 0.360 0.390 0.420 0.460 0.440 0.360 0.330 0.520 0.730 0.520 0.580 0.610 0.620 0.570 0.570 0.540 0.530 220 388 785 1142 1306 1515 1679 1507 174 43 46 168 351 386 326 234 195 566 -0.601 2.598 3.546 -0.837 -7.194 -12.243 4.045 3.368 3.126 2.204 0.468 -0.467 -0.646 -0.966 -1.276 -1.363 -40.00 8.803 6.089 0.560 0.530 0.520 0.500 0.510 0.510 0.300 0.300 0.290 0.340 0.410 0.350 0.360 0.420 0.520 0.600 0.630 0.600 249 313 314 362 450 525 27 60 66 62 52 49 55 132 234 549 162 22 2.551 2.370 -0.481 -4.275 -50.00 2.116 4.432 4.343 3.983 4.115 4.520 4.071 3.261 0.915 -1.154 -1.593 -2.661 0.891 2.461 0.370 0.410 0.420 0.420 0.610 0.570 0.550 0.560 0.540 0.460 0.290 0.350 0.340 0.350 0.350 0.430 0.500 0.580 272 281 248 126 101 192 52 87 167 223 192 241 83 25 15 16 26 38 3.848 2.066 -1.165 0.173 2.276 3.203 2.862 1.315 3.988 4.470 4.858 4.885 5.004 1.268 -60.00 1.056 1.702 2.853 3.486 0.540 0.510 0.520 0.510 0.470 0.410 0.390 0.400 0.410 0.420 0.420 0.420 0.440 0.460 0.440 0.450 0.510 0.550 41 35 31 27 43 62 76 167 248 347 363 414 513 507 409 233 199 147 3.075 2.791 1.469 2.983 5.183 4.947 3.432 2.243 1.949 2.421 3.821 4.348 4.672 4.826 4.953 4.494 3.527 4.163 -70.00 0.460 0.380 0.420 0.430 0.380 0.340 0.360 0.460 0.420 0.410 0.430 0.470 0.470 0.460 0.450 0.440 0.440 0.410 616 452 91 63 63 100 191 243 299 348 462 651 805 126 114 111 103 77 2.905 3.681 5.414 6.028 5.222 5.085 5.296 5.558 6.602 5.960 2.993 7.885 34.570 13.350 6.961 -80.00 3.655 2.779 2.616 0.050 0.330 0.420 0.110 0.360 0.540 0.380 0.440 1.190 0.430 0.390 0.210 0.520 0.410 0.680 0.420 0.170 0.070 43 35 34 78 118 263 528 772 623 405 64 103 98 103 84 84 65 64

-180.00 -170.00 -160.00 -150.00 -140.00 -130.00 -120.00 -110.00 -00.00 -90.00 -80.00 -70.00 -60.00 -50.00 -40.00 -30.00 -20.00 -10.00 3.358 -22.909 -51.055 -51.343 -4.644 10.214 -4.635 -10.679 -12.446 -18.815 -33.422 -46.181 -48.004 -33.199 -1.760 80.00 10.088 -7.319 -4.783 1.020 0.980 1.420 1.970 1.760 0.790 1.290 1.080 0.920 1.250 1.020 1.350 1.440 1.070 2.400 1.430 1.000 2.470 3011 2828 2551 2250 1308 2354 2186 2244 2459 2750 3102 3161 3139 839 867 1046 1924 2267 -9.026 -37.482 -45.173 -27.944 -9.243 -6.962 -8.349 -9.662 -13.155 -21.460 -35.395 -42.080 -37.686 -0.556 70.00 15.255 11.674 2.411 2.645 1.270 1.220 1.540 1.420 1.360 1.150 1.220 1.270 1.470 1.440 1.230 1.370 1.460 1.290 1.460 1.470 1.740 1.410 2876 2590 2329 1543 2814 2582 2208 2051 2121 1945 2066 2269 2427 2828 4762 3751 3493 2882 -2.809 2.446 -18.782 -32.223 -25.361 -12.348 -4.233 -2.875 -4.125 -7.080 -13.291 -20.316 0.073 12.915 16.150 16.736 14.330 60.00 -4.084 0.900 0.830 0.920 0.770 0.760 0.940 0.790 0.860 0.880 1.040 1.130 1.180 0.990 0.830 1.100 0.970 0.880 0.840 1347 1388 1362 1318 897 568 725 652 3854 2728 1635 1401 1509 1636 1405 6970 5758 5095 15.059 8.658 6.217 3.274 21.261 5.473 3.336 -3.070 -7.575 -9.632 -6.914 10.622 16.850 11.601 50.00 -46.697 -41.998 -13.968 17.678 0.530 0.690 0.680 0.880 0.640 0.860 0.840 0.890 0.820 0.710 0.500 0.430 0.470 0.750 0.840 0.830 0.670 1.020 123 2500 2030 582 112 1203 1303 1420 1299 1320 1761 2122 3390 2614 1882 1190 7474 5829 17.069 10.089 6.920 40.00 -47.966 -41.054 -17.074 1.706 -1.208 -13.922 -15.500 -7.490 -1.956 -4.032 -0.520 12.551 41.179 44.825 29.344 0.510 0.530 0.520 0.940 0.890 0.880 0.940 0.770 0.540 0.520 0.570 0.640 0.700 0.810 1.170 0.660 0.610 0.640 1423 122 40 779 1242 1822 2308 2816 3338 2944 2965 2731 1911 1340 860 385 520 646 6.507 -38.486 -20.356 -10.115 -0.358 3.486 14.779 33.429 39.643 34.363 19.039 1.094 -0.436 -3.987 -11.498 -14.220 -32.576 30.00 -9.986 0.910 0.970 0.880 0.660 0.610 0.590 0.650 0.530 0.530 0.550 0.550 0.560 0.460 0.550 0.550 0.830 1.030 0.780 1493 811 604 308 212 231 481 1209 1896 2497 3290 2753 1980 1020 126 39 2308 2135 -6.704 9.378 26.191 25.447 13.723 2.459 -2.875 -19.333 -24.470 -47.010 -47.143 -23.579 -5.682 1.194 6.945 8.293 37.749 20.00 -16.453 0.440 0.510 0.490 0.550 0.470 0.370 0.860 1.100 0.780 0.460 0.530 0.740 0.850 1.060 1.010 0.840 0.650 0.490 565 1447 1892 1628 1094 290 74 60 1346 523 184 196 338 450 2247 2164 1893 2130 9.459 10.979 12.280 7.018 -1.218 -1.989 6.673 -34.928 -33.250 -43.146 -38.788 -15.343 4.788 12,954 11.464 12.282 10.00 9.030 18.036 0.340 0.550 0.650 0.690 0.840 0.970 0.820 0.640 0.500 0.420 0.360 0.320 0.250 0.430 0.970 0.880 0.660 0.950 74 790 293 147 65 400 330 511 619 519 883 1139 2234 1359 610 2496 2600 3035 3.305 2.894 0.00 35.735 53.125 -12.147 -39.996 -27.282 -20.788 -7.473 2.904 9.593 18.910 14.076 11.902 6.189 0.397 -1.218 1.491 0.380 0.330 0.520 0.560 0.650 0.700 0.650 0.530 0.480 0.450 0.430 0.450 0.860 0.750 0.590 0.710 0.690 1.010 389 408 644 648 258 218 186 144 52 43 64 3366 2837 2753 1906 1138 577 485 10.860 12.399 13.785 13.215 6.316 3.126 -2.171 -6.999 0.038 3.332 4.918 58.221 0.494 -30.302 -15.047 6.403 7.284 -10.00 44.458 0.530 0.530 0.540 0.510 0.520 0.640 0.610 0.580 0.760 0.660 0.740 0.550 0.700 0.670 0.470 0.690 0.730 1.050 46 39 56 3002 2320 1085 550 546 427 316 194 475 526 215 108 101 77 3522 8.920 2.278 -1.034 -2.473 1.910 6.213 7.510 6.631 -7.276 6.531 16.970 16.572 14.178 12.560 -20.00 20.209 40.693 24.290 -8.762 0.680 0.670 0.600 0.680 0.740 0.710 0.490 0.530 0.530 0.510 0.670 0.580 0.650 0.810 0.810 0.730 0.680 0.640 97 109 110 74 75 64 350 288 386 284 211 173 201 206 125 1852 1404 1038 -0.535 4.353 11.154 12.883 9.675 5.837 12.351 17.714 17.620 15.817 11.037 4.331 -3.345 -30.00 13.151 13.787 11.250 5.461 1.328 0.670 0.720 0.850 0.880 0.840 0.760 0.690 0.670 0.760 0.830 0.590 0.600 0.680 0.750 0.730 0.640 0.760 0.650 251 185 157 104 95 100 88 148 259 243 226 750 523 80 73 107 190 202 5.457 9.533 12.105 11.157 13.246 7.472 6.282 6.360 6.682 7.958 11.737 14.533 15.840 14.810 11.610 6.834 2.855 -40.00 10.677 0.800 0.710 0.700 0.750 0.720 0.780 0.760 0.780 0.810 0.730 0.670 0.750 0.720 0.700 0.730 0.720 0.740 0.730 300 280 161 168 300 290 690 461 33 45 68 75 86 92 59 30 101 179 9.134 9.556 10.193 11.246 13.037 15.447 17.642 19.017 14.928 12.063 10.427 9.960 10.276 10.513 -50.00 10.910 12.131 11.718 9.625 0.620 0.620 0.650 0.670 0.680 0.700 0.780 0.780 0.770 0.810 0.830 0.770 0.710 0.660 0.590 0.650 0.710 0.760 18 38 56 65 53 51 185 232 186 128 181 133 113 78 351 172 11 12 15.929 10.761 10.750 11.156 12.203 14.090 16.249 18.581 18.609 17.118 13.777 11.916 10.915 -60.00 14.018 12.859 12.593 12.233 11.307 0.550 0.550 0.580 0.650 0.710 0.750 0.770 0.780 0.800 0.810 0.780 0.730 0.660 0.600 0.570 0.590 0.630 0.660 52 176 206 140 104 100 92 75 38 142 47 8 11 13 12 21 37 45 11.667 14.729 15.531 16.628 17.014 16.622 15.920 14.330 12.641 -70.00 15.831 14.375 13.388 12.895 12.476 10.848 11.090 12.585 13.973 0.680 0.680 0.620 0.540 0.540 0.550 0.420 0.440 0.460 0.510 0.570 0.630 0.680 0.650 0.630 0.650 0.460 0.430 97 81 88 72 20 20 22 28 21 21 19 26 82 144 136 67 69 88 11.600 11.144 7.298 7.328 20.094 31.108 23.689 14.494 12.658 12.589 12.447 13.735 11.741 9.220 10.993 11.160 -80.00 8.260 9.264 0.210 0.470 0.450 0.860 0.770 0.500 0.250 0.490 0.760 0.800 0.300 0.200 0.720 0.870 0.570 0.290 0.240 0.300 41 40 42 40 34 78 98 207 190 125 90 76 58 60 61 67 89 76

80.00 90.00 100.00 110.00 120.00 130.00 140.00 150.00 160.00 170.00 50.00 60.00 70.00 20.00 30.00 40.00 0.00 10.00 43.816 -12.386 -47.637 -49.236 -52.805 -52.347 -51.171 -42.853 -19.202 45.923 51.794 9.253 -1.589 -5.021 -8.627 -30.692 26.573 80.00 1.204 2.570 2.070 1.890 1.880 1.500 2.420 1,900 2.710 1.160 0.970 1.390 2.090 2.780 2.150 2.800 1.430 0.700 0.750 7787 6841 5502 3999 3013 1961 1292 899 4663 6137 7463 8205 8307 2376 3482 541 356 1313 2.378 -29.105 -42.873 -48.396 -50.477 -51.288 -48.405 -39.503 2.123 26.017 -8.645 -10.844 -21.980 0.784 20.661 70.00 -20.521 -11.459 -8.348 2.120 2.000 2.060 1.640 1.780 1.540 1.690 1.720 1.590 1.550 1.670 1.650 1.180 1.340 1.690 1.320 1.390 1.220 10625 5841 4041 3508 3867 14893 14090 13288 12168 5552 7694 10363 12749 14261 653 516 1539 3319 60.00 -24.236 -23.624 -19.947 -16.459 -17.134 -22.993 -29.669 -13.518 -0.927 -11.173 -27.239 -39.706 -43.988 -44.998 -46.838 -44.510 -30.952 -18.456 1.340 1.200 1.170 1.150 1.080 1.230 1.210 1.190 0.970 0.950 1.030 1.130 1.300 1.410 1.080 1.190 0.800 0.840 4610 10738 11563 11720 11830 12883 13178 9036 4883 5852 386 323 706 1680 2890 4808 7790 9498 -6.705 -10.012 -11.241 -11.440 -20.669 -44.653 -54.194 -51.720 -43.907 -29.470 -17.236 -19.147 -34.813 -27.202 -23.843 -27.939 -43.298 50.00 -1.329 1.050 0.930 1.450 1.070 0.840 1.060 1.050 0.710 0.800 0.630 0.980 1.120 0.930 0.770 0.740 0.780 0.770 0.700 975 1829 3267 4450 4767 4797 5062 5727 9243 10151 8045 3463 4211 6294 78 102 321 76 -2.913 -21.896 -14.791 -22.627 -47.121 -0.399 9.145 -31.648 -54.553 -59.146 -58.061 -40.227 -0.271 -2.907 -4.949 9.035 40.00 5.883 2.842 1.030 1.150 1.040 0.540 0.820 0.570 0.590 0.640 0.770 0.780 0.710 0.760 1.020 1.060 1.280 1.240 0.470 0.540 7070 6435 2887 3351 3270 3359 3327 3200 3283 4029 5360 317 964 1814 2498 36 42 63 -2.192 -11.600 -15.145 -8.179 -37.022 -51.740 -48.778 -12.570 8.918 18.295 0.826 0.543 -1.943 -2.006 -9.137 -16.574 28.476 33.688 30.00 0.550 0.770 0.910 1.080 1.090 1.190 0.940 0.960 0.900 0.970 0.860 0.660 0.480 0.540 0.570 0.520 0.580 0.660 1901 2796 3602 4131 3648 3834 3361 2777 2474 1594 2212 2472 52 55 73 322 671 1192 3.169 -11.228 -18.862 19.419 12.580 -14.249 -26.113 -42.451 -32.000 -10.952 26.966 39.851 38.432 13.682 20.00 -4.603 -2.615 -4.790 0.988 0.790 0.890 0.860 1.120 1.110 1.000 0.740 0.730 0.580 0.540 0.500 0.390 0.430 0.520 0.860 0.540 0.560 0.500 2157 2580 3023 3914 3900 3161 2639 68 60 84 282 444548 1051 1447 1685 1:95 1647 -9.909 -27.262 -42.908 -31.879 -15.538 -1.114 3.772 32.890 13.897 8.849 8.888 0.012 2.007 6.212 10.00 -1.202 0.338 1.993 3.871 1.020 1.120 0.950 0.800 0.710 1.080 0.560 0.570 0.560 0.540 0.550 0.690 0.860 0.940 0.410 0.560 0.670 0.580 160 367 421 500 536 915 952 1059 1497 2050 3216 4130 4045 3467 2802 80 87 68 -1.911 -11.113 -29.084 -30.635 18.386 18.587 -12.513 2.538 39.246 10.671 9.027 7.462 5.185 4.652 7.996 9.913 0.00 4.383 4.196 0.820 0.720 0.780 1.020 1.200 0.620 0.760 0.740 0.600 0.560 0.560 0.630 0.670 0.590 0.550 0.710 0.780 0.520 3320 3379 3516 2913 286 312 158 178 281 352 837 1723 2784 77 187 74 58 53 -1.497 -5.192-4.742 7.611 7.499 3.945 -5.714 -7.831 1.797 16.999 42.934 -10.00 5.814 4.788 5.939 8.596 11.302 9.572 6.744 0.500 0.620 0.710 0.690 0.460 0.350 0.520 0.640 0.700 0.470 0.550 0.970 0.590 0.680 0.860 0.850 0.710 0.590 2920 3066 169 217 249 511 1157 2135 2550 2483 71 56 58 38 63 128 125 154 0.319 -17.172 -19.674 -26.719 5.386 6.646 8.590 9.280 7.372 4.696 3.441 3.277 3.946 3.675 6.248 5.558 -9.752 -20.00 5.282 0.610 0.710 0.620 0.600 0.500 0.400 0.400 0.580 0.550 0.510 0.810 0.810 0.730 0.620 0.590 0.550 0.650 0.740 270 407 866 1325 1402 1551 1816 2078 41 50 48 23 30 134 181 217 200 219 9.714 6.466 -6.794 -17.877 -23.708 -12.552 7.579 7.866 8.745 6.236 2.625 2.388 3.272 4.802 5.606 13.979 5.651 6.531 -30.00 0.530 0.570 0.640 0.490 0.530 0.510 0.500 0.750 0.650 0.610 0.570 0.560 0.520 0.580 0.530 0.830 0.790 0.770 29 84 113 162 176 161 157 287 469 735 763 875 1019 915 29 23 17 18 8.665 8.682 4.677 0.557 8.198 7.981 7.212 6.567 8.734 12.248 11.628 10.276 -1.763 -40.00 8.797 7.086 7.564 8.128 7.958 0.580 0.790 0.810 0.830 0.840 0.760 0.680 0.690 0.620 0.570 0.570 0.590 0.570 0.610 0.680 0.620 0.480 0.610 451 39 54 78 121 192 270 343 376 587 572 29 14 12 22 28 40 44 15.001 8.803 12.511 11.756 6.784 10.133 14.446 12.882 9.220 9.696 8.228 6.896 6.980 7.536 8.141 9.638 11.485 14.584 -50.00 0.580 0.590 0.610 0.610 0.580 0.570 0.780 0.760 0.730 0.710 0.690 0.720 0.750 0.710 0.640 0.570 0.550 0.750 242 295 361 292 237 217 302 21 22 33 37 146 197 238 10 8 12 18 6.723 7.427 8.475 9.889 12.003 14.102 13.661 11.348 9.996 12.246 15.680 16.365 16.363 9.302 7.987 6.650 6.238 -60.00 10.285 0.600 0.710 0.700 0.680 0.680 0.700 0.690 0.640 0.590 0.560 0.550 0.560 0.600 0.590 0.690 0.720 0.730 0.660 693 551 18 21 43 56 68 67 179 205 290 365 443 654 617 403 18 14 8.195 6.634 11.138 12.050 11.496 12.791 16.144 18.104 16.967 -70.00 11.480 10.525 9.397 7.058 6.416 7.315 8,277 9.562 12.359 0.680 0.620 0.600 0.590 0.570 0.570 0.530 0.480 0.450 0.450 0.480 0.530 0.520 0.550 0.610 0.680 0.720 0.720 71 79 69 65 92 161 267 384 561 645 765 624 434 40 59 60 72 39 11.955 13.072 13.358 9.064 2.601 16.147 47.254 40.428 19.796 7.377 6.372 7.122 8.046 8.819 10.025 10.714 -80.00 9.334 9.749 0.480 0.350 0.090 0.220 0.840 1.050 1.010 1.000 0.430 0.330 0.480 0.590 0.590 1.620 0.930 1.040 0.100 0.340 351 416 97 38 52 74 80 77 79 68 56 35 62 84 200 601 620 35

Depth = 2104 km

		1 2 0 0 0	1 6 0 0 0	150 00	140 00	130 00	-120 00	-110.00	-100.00	-90.00	-80.00	-70.00	-60.00	-50.00	-40.00	-30.00	-20.00	-10.00
	-180.00	-1/0.00	-160.00	-100.00	-140.00	-130.00		-4.072	-4.631	-3.227	-3.238	-4.272	-5.470	-4.109	-0.841	0.767	0.644	-0.212
80.00	5.647	3.132	-6.89/	-13.569	-13.12/	-0.014	0 360	0 120	0 330	0.120	0.080	0.080	0.080	0.080	0.170	0.140	0.160	0.240
	0.340	0.250	0.200	0.410	0./30	0.530	0.500	2427	2362	2273	2246	2142	2054	1934	1583	1099	440	178
	956	1475	2067	2659	2665	2619	2014	242/ E 06/	1 700	_4 340	-3.492	-3,110	-3.437	-4.197	-3.949	-2.326	-0.819	-0.160
70.00	10.374	8.376	6.040	-0.195	-6.485	-9.1/3	-8.296	-5.904	-4.700	-4.340	0 250	0.160	0.130	0.130	0.130	0.120	0.130	0.150
	0.500	0.410	0.330	0.270	0.140	0.370	0.420	0.380	1041	0.500	1026	1060	1067	1192	1100	740	329	161
	3875	3160	3057	3141	2900	2388	1913	1336	1041	2 274	2 644	2 040	_1 775	_1 879	-2.187	-2.229	-1.684	-0.972
60.00	12.694	11.909	10.110	6.922	2.606	-1.601	-4.080	-4.52/	-3.9/2	-3.270	-2.044	-2.040	0 180	0 140	0.110	0.090	0.060	0.060
	0.200	0.270	0.280	0.270	0.240	0.120	0.110	0.200	0.250	0.270	0.200 E10	410	286	134	44	34	44	75
	4578	3867	3265	2278	1230	686	580	558	529		0 110	0 295	0 117	-0.033	-0.135	-0.304	-0.478	-0.496
50.00	10.427	11.396	9.252	5.204	1.984	0.909	0.123	-0.645	-0.982	-0.545	0.110	0.235	0.170	0 160	0 140	0.120	0.100	0.070
	0.300	0.160	0.100	0.150	0.180	0.190	0.160	0.080	0.060	0.100	0.140	211	189	54	12	16	16	18
	2695	1809	1371	907	509	333	293	379	429	403	1 200	1 212	0 967	0 685	0.501	0.413	0.327	0.183
40.00	5.048	5.474	3.339	-1.001	-3.009	-1.867	-0.460	0.378	0.393	0.516	1.300	1.212	0.907	0.005	0.110	0.110	0.100	0.080
	0.340	0.250	0.180	0.110	0.120	0.140	0.160	0.160	0.110	0.070	0.040	401	209	28	16	16	18	18
	1806	1265	786	419	156	99	41	83	144	263	420	401	0 909	0 538	0.201	-0.004	-0.007	0.070
30.00	5.549	3.092	-0.024	-2.274	-4.510	-4.618	-2.272	-0.465	0.365	0.5//	0.690	0.004	0.000	0.050	0.070	0.070	0.080	0.070
	0.220	0.180	0.130	0.130	0.130	0.140	0.150	0.150	0.130	0.100	0.070	0.040	275	359	129	19	15	17
	1615	1117	519	242	138	100	57	61	103	216	313	207	0 575	0 504	0 074	-0.524	-0.860	-0.718
20.00	8.394	7.187	-0.301	-3.457	-5.301	-5.097	-2.771	-1.028	-0.084	0.414	0.533	0.431	0.570	0.060	0.060	0.060	0.070	0.070
	0.260	0.170	0.110	0.130	0.170	0.170	0.160	0.130	0.110	0.050	0.070	0.000	0.000	366	122	22	29	43
	1313	1159	714	295	197	134	80	39	39	44	3/	108	0 179	0 246	_0 261	-0.796	-1.415	-1.155
10.00	9.486	7.210	-0.344	-5.892	-8.486	-4.763	-1.879	-0.851	-0.520	-0.045	0.345	0.342	0.170	0.240	0.070	0 070	0.070	0.070
	0.210	0.200	0.130	0.150	0.190	0.200	0.170	0.140	0.100	0.080	0.070	0.070	0.070	157	37	37	43	50
	1279	1257	838	366	220	210	199	119	68	70	36	45	249	0 261	0 756	_1 673	-1.217	-0.586
0.00	3.578	4.825	-1.026	-7.338	-7.306	-2.065	1.318	0.507	-0.333	-0.563	-0.194	0.155	0.003	-0.201	0.000	0.080	0.070	0.070
	0.120	0.160	0.160	0.170	0.190	0.200	0.180	0.160	0.120	0.100	0.090	0.090	0.090	0.090	0.090	45	43	34
	1135	1193	705	367	352	363	287	186	80	63	54	23	20	41	1 201	.1 284	_0 748	-0.214
-10.00	6.164	7.535	1.300	-3.541	-3.810	-0.642	1.194	1.223	0.502	-0.209	-0.655	-0.350	-0.185	-0.090	-1.391	0 100	0 0 0 0	0.080
	0.110	0.100	0.140	0.150	0.170	0.170	0.170	0.160	0.130	0.110	0.100	0.090	0.100	0.100	38	35	21	18
	1166	1137	852	111	. 309	308	270	145	31	44	45	31	20	0 522	-0 640	-0 679	-0.230	0.160
-20.00	2.992	5.806	2.665	-0.718	3 -1.317	-0.299	0.684	0.792	0.573	0.081	-0.570	-0.854	-0.349	0.000	0.090	0 100	0.100	0.090
	0.110	0.080	0.090	0.110	0.150	0.180	0.170	0.160	0.130	0.100	0.100	0.090	0.090	0.000	35	23	17	16
	884	782	678	38	3 40	115	97	99	87	36	29	30	3/	0 217	0 126	0 049	0.225	0.460
-30.00	1.831	1.717	1.235	-0.220	0 -0.551	0.189	0.781	0.952	0.746	0.100	-0.416	-0./53	-0.539	-0.217	0.070	0.070	0.070	0.080
	0.100	0.070	0.080	0.090	0.120	0.150	0.170	0.140	0.100	0.090	0.100	0.110	0.100	0.000	15	16	14	15
	493	338	3 46	5 41	1 56	131	. 118	106	92	32	48	42	0 4 2 2	0 101	0 070	0 268	0.442	0.594
-40.00	2.885	1.933	0.623	0.044	-0.135	0.206	0.544	0.922	0.910	0.491	-0.1/8	-0.55/	-0.432	-0.101	0.070	0.200	0 050	0.040
	0.100	0.090	0.080	0.050	0.060	0.070	0.080	0.090	0.070	0.080	0.090	0.100	0.100	0.000	10	0.000	0.0000	10
	638	408	3 37	38	3 65	67	7 82	71	L 47	23	/4	92	51	40	0 144	0 313	0 494	0.653
-50.00	2.117	2.158	1.506	0.913	3 0.699	0.737	0.876	1.235	5 1.515	1.456	1.036	0.5/1	0.106	-0.122	0.144	0.010	0 050	0 030
	0.070	0.070	0.070	0.080	0.070	0.070	0.070	0.070	0.070	0.080	0.090	0.090	0.080	0.070	0.000	19	10	12
	540	335	5 16	5 19	9 29	44	1 70) 77	7 60	50	166	201	1 1 6 5	42	0 430	0 478	0 507	0.577
-60.00	2.091	1.912	2 1.788	3 1.530	1.282	1.165	5 1.160	1.231	1.528	1.879	1.987	1./83	1.165	0.025	0.439	0.470	0.050	0 040
	0.070	0.060	0.060	0.070	0.070	0.080	0.080	0.080	0.080	0.090	0.100	0.100	0.100	0.090	0.070	0.000	10	18
	273	100) 10) 2	1 18	2	1 41	49	9 53	73	215	223	/ 6	42	0 004	0 720	0 635	0 598
-70.00	1.710	1.755	5 1.696	5 1.62	3 1.494	1.348	3 1.212	1.132	2 1.230	1.671	2.097	2.121	1.831	1.403	0.994	0.730	0.055	0.040
	0.060	0.070	0.070	0.06	0.070	0.070	0.070	0.080	0.080	0.090	0.100	0.100	0.100	0.090	0.080	0.070	10	21
	153	2	7 24	4 3	4 36	4	2 38	3 30	6 94	151	174	177	59	20	20	0 946	0 752	0 730
-80.00	1.639	0.709	9 0.720	0.78	2 0.742	0.85	9 0.973	0.359	9 0.582	2.219	5.256	2.580	1.059	0.787	0.010	0.040	0.100	0.120
	0.070	0.070	0.050	0.04	0 0.050	0.02	0.030	0.060	0.070	0.190	0.270	0.150	0.050	0.030	0.070	0.110	0.100	15
	50) 31	8 34	4 4	3 40) 5	0 110) 150	0 218	223	172	142	61	51	36	24	15	10

1

	0.00	10.00	20.00	30.00	40.00	50.00	60.00	70.00	80.00	90.00	100.00	110.00	120.00	130.00	140.00	150.00	160.00	170.00
80.00	-0.697	-1,905	-2.999	-2.497	-0.299	-0.187	1.281	-1.291	-5.117	-7.494	-5.853	-0.940	5.203	7.404	10.512	16.035	13.879	6.936
00.00	0.240	0.090	0.080	0.090	0.140	0.280	0.290	0.700	1.630	1.790	1.240	1.020	0.930	0.510	0.160	1.470	0.920	0.460
	131	130	163	521	1164	1715	2303	2887	3280	3677	4066	4345	4673	4688	4150	3434	2688	1645
70 00	0 241	-0 538	_1 321	_2 291	-2 584	-1.701	-1.103	0.056	-0.375	-2.364	-4.500	-4.833	-2.661	1.302	4.161	7.153	11.366	13.314
10.00	0.241	-0.550	0 170	0 120	0 110	0 120	0 190	0.230	0.290	0.870	1.240	1,190	1.070	0.980	0.750	0.390	0.490	0.600
	122	122	142	415	1010	1703	2530	3532	4778	5648	6101	6170	5236	4031	3951	3934	3235	3664
<pre></pre>	100	123	143	1 5 5 7	2 216	2 762	2 7 7 6	2 5 3 0	_0 0/1	0 673	0 674	-0 747	-2 294	_1 478	0.876	2.970	5.848	9.652
60.00	-0.536	-0.539	-0.001	-1.557	-2.510	-2.703	-2.720	0 120	0 150	0.075	0.350	0.660	0 790	0 820	0.810	0.720	0.540	0.140
	0.060	0.100	0.140	0.130	140	0.000	1265	2011	5255	6302	6807	6650	6160	5443	3110	2337	3078	4189
F0 00	0 450	0 512	0 602	0 0 0 0 0 0	1 222	1 0 1 2	2 9/3	5 201	-8 456	-6 155	_0 520	4 137	4 095	-0.321	-2.078	0.229	2.556	7,940
50.00	-0.458	-0.512	-0.092	-0.908	-1.223	-1.015	-2.045	- 1201	0.150	0 170	0.160	0 120	0 250	0.380	0 440	0 500	0.530	0.500
	0.060	0.050	0.000	0.090	0.110	0.110	125	0.120	2644	3801	1901	6220	6666	5953	3633	1304	1668	2172
10 00	23	0 244	4/	42	41	0 005	1 557	2 504	0 6/1	10 000	-12 205	-1 658	4 630	2 743	-2 921	-1.278	0.245	2.519
40.00	0.026	-0.244	-0.501	-0.000	-0.000	-0.895	-1.557	-3.304	- 7.041	-10.000	-12,205	-1.050	0 140	0 110	0 140	0 190	0 280	0.360
	0.070	0.050	0.040	0.040	0.070	0.100	0.120	120	1200	2154	2752	2490	3705	3540	2242	840	1265	1857
20.00	20	23	31	34	33	0 271	194	420	1 2 7 9	0 5 1 1	14 520	0 001	0 7 9 0	1 2 2 1	1 666	0 497	0 517	2 861
30.00	-0.091	-0.401	-0.792	-0.869	-0.6/9	-0.371	-0.370	-1.100	-4.2/0	-9.511	-14.550	-0.004	-0.700	0 170	0 150	0.120	0 190	0 250
	0.070	0.060	0.060	0.050	0.050	0.070	0.100	0.120	0.100	0.100	1600	2042	1109	0.170	1056	0.120	1279	1581
	19	25	37	39	30	/ 1	232	2/0	1 770	0.1Z	1030	2043	2 250	0 806	1 923	2 698	2 689	6 128
20.00	-0.548	-0.994	-1.263	-1.348	-0.770	-0.049	0.370	0.035	-1.//0	-2.919	-0.233	-0.070	-3.250	-0.090	0 190	0 160	0 170	0.280
	0.070	0.070	0.070	0.070	0.080	0.080	0.100	0.120	0.100	0.200	0.240	0.200	0.250	517	1194	1323	1273	1545
	34	30	42	43	24	32	123	1/2	204	2 214	520	6 750	240	0 250	2 220	1 0 0 5	1 069	2 354
10.00	-0.613	-0.56/	-0./39	-0.650	-0.370	0.154	0.531	0.549	-0.392	~3.214	- 3 . 4 4 4	-6.750	-3.235	0.200	2.220	0 160	-1.009	0 170
	0.070	0.080	0.090	0.080	0.070	0.080	0.090	0.120	0.150	0.190	0.240	0.200	0.270	0.230	1212	1216	0.170	1050
	41	29	21	27	23	19	24	41	12	1 220	300	40/	399	0 1 6 7	2 001	1 202	2 702	1 442
0.00	-0.234	-0.072	0.081	0.087	0.211	0.304	0.4/3	0.503	0.112	-1.229	-2.613	-5.500	-4./40	0.10/	3.901	1.202	-2.702	1.442
	0.090	0.090	0.100	0.100	0.090	0.070	0.080	0.120	0.150	0.180	0.220	0.230	0.230	0.210	1200	0.150	0.150	0.100
	35	25	16	18	19	25	28	36	0 1 2 0	144	1 1 5 0	340	241	2 472	1 241	0 664	1 062	0 072
-10.00	0.141	0.265	0.429	0.506	0.50/	0.49/	0.329	0.229	-0.138	-0.5/3	~1.160	-2.542	-3.564	- 3 . 4 / 2	-1.241	-0.004	-1.902	0.072
	0.090	0.110	0.120	0.120	0.110	0.090	0.080	0.090	0.130	0.160	0.190	0.200	0.200	0.180	0.150	0.120	0.110	1084
	29	30	15	11	13	23	22	28	64	83	118	262	490	1041	1190	2 202	2 801	1004
-20.00	0.302	0.343	0.455	0.563	0.514	0.371	0.299	-0.022	-0.383	-0.2/5	-0.3/5	-0.633	-1.535	-3.094	-3.644	-3.302	-2.891	-0.848
	0.090	0.090	0.110	0.110	0.110	0.110	0.100	0.100	0.110	0.130	0.160	0.180	0.170	0.150	0.130	0.100	0.120	0.110
	20	19	8	11	11	9	20	51	66	/4	107	218	34/	1 204	025	1 011	2 0 2 4	900
-30.00	0.479	0.489	0.452	0.497	0.511	0.411	0.244	0.193	0.019	0.118	0.223	1.065	0.43/	-1.394	-2.946	-1.911	-2.034	-0.254
	0.080	0.080	0.090	0.090	0.100	0.100	0.100	0.100	0.090	0.100	0.110	0.130	0.150	0.140	0.110	0.090	0.070	0.120
	17	17	9	14	10	10	15	49	/4	63	110	195	321	455	4/1	0 456	0 246	0 256
-40.00	0.594	0.554	0.603	0.600	0.580	0.398	0.402	0.448	0.612	0.843	0.963	0.830	0.754	0.868	0.568	0.450	0.340	0.350
	0.040	0.060	0.080	0.090	0.090	0.100	0.110	0.110	0.090	0.080	0.080	0.080	0.090	0.110	0.110	0.090	0.070	0.110
	10	6	11	14	13	12	8	22	37	90	139	214	318	390	394	424	015	534
-50.00	0.679	0.644	0.612	0.614	0.608	0.559	0.479	0.515	0.597	0.921	1.189	1.203	0.244	-0.03/	0.8/1	1.321	1.565	1.749
	0.030	0.030	0.040	0.060	0.080	0.070	0.090	0.100	0.110	0.110	0.100	0.080	0.070	0.070	0.070	0.070	0.070	0.070
	7	6	10	14	19	17	21	30	64	100	193	208	241	372	521	492	485	483
-60.00	0.686	0.682	0.659	0.627	0.598	0.558	0.505	0.455	0.508	0.683	0.948	0.975	0.856	0.558	0.342	0./68	1.423	2.01/
	0.000	0.020	0.030	0.040	0.050	0.050	0.060	0.070	0.080	0.100	0.100	0.090	0.090	0.080	0.070	0.060	0.070	0.070
	4	5	10	13	17	21	45	56	76	168	181	250	388	593	751	/03	705	482
-70.00	0.606	0.653	0.663	0.639	0.606	0.572	0.519	0.483	0.484	0.534	0.641	0.756	0.699	0.617	0.640	0.789	1.426	1.511
	0.040	0.030	0.030	0.030	0.040	0.040	0.050	0.060	0.070	0.070	0.080	0.090	0.100	0.090	0.080	0.070	0.060	0.060
	14	15	12	14	27	50	64	65	63	58	67	136	305	453	544	690	623	466
-80.00	0.756	0.655	0.719	0.511	0.357	0.396	0.404	0.269	0.425	0.646	0.794	0.788	0.381	-0.884	0.692	1.711	4.439	6.521
	0.120	0.100	0.050	0.010	0.020	0.010	0.040	0.080	0.100	0.100	0.060	0.060	0.100	0.390	0.080	0.060	0.080	0.720
	18	2.2	25	36	46	63	59	60	52	54	75	74	110	110	82	195	215	141

-180.00 -170.00 -160.00 -150.00 -140.00 -130.00 -120.00 -110.00 -100.00 -90.00 -80.00 -70.00 -60.00 -50.00 -40.00 -30.00 -20.00 -10.00 80.00 -54.012 -46.049 -39.921 5.017 45.996 29.098 10.525 2.252 8.562 17.337 18.659 17.219 11.340 4.957 0.560 -5.996 -9.179 -8.302 0.740 0.890 0.870 0.930 0.970 0.880 0.910 0.760 0.590 1.200 0.880 1.500 1.050 0.760 2.370 1.860 1.910 1.890 408 155 78 56 48 49 50 1697 1668 1589 1470 1310 1053 779 1391 1578 1666 1418 7.735 12.302 15.076 15.784 13.387 9.176 5.215 0.496 -3.060 70.00 -52.370 -53.053 -49.919 -45.450 -32.873 1.131 13.156 11.155 6.766 1.160 1.270 1.330 1.330 1,460 1.370 1.370 1.310 1.180 1,980 1.710 1.660 1.610 1.530 1.400 1.480 1.450 1,440 281 191 132 63 58 57 57 59 60 918 575 346 2000 1949 1819 1386 2890 2285 12.666 10.524 8.202 14.384 15.357 14.651 1.493 7.460 8.362 9.651 12.235 60.00 -29.407 -43.180 -46.979 -45.771 -41.556 -32.862 -13.096 0.540 0.700 0.700 0.660 0.710 0.700 0.590 0.540 0.620 0.580 0.610 0.810 0.800 0.830 0.780 0.930 1.020 1.050 21 64 42 21 19 20 20 23 59 78 83 842 326 143 49 2973 2240 1689 6.636 11.168 13.240 14.302 15.354 15.783 15.401 14.271 13.114 12.861 50.00 -35.468 -36.676 -41.524 -39.316 -32.375 -22.363 -10.915 -1.110 0.400 0.380 0.430 0.390 0.380 0.430 0.470 0.460 0.420 0.860 0.780 0.620 0.550 0.530 0.900 0.850 0.870 0.890 17 15 14 18 18 21 58 45 18 609 458 267 158 99 45 28 39 69 3.736 11.063 15.089 16.119 15.812 15.559 14.139 12.530 11.834 11.713 11.788 40.00 -40.957 -44.093 -48.527 -44.607 -29.978 -7.296 7.629 0.410 0.420 0.410 0.360 0.420 0.380 0.410 0.850 0.570 0.450 0.380 0.420 1.350 0.930 1.240 1.010 1.030 1.040 23 21 18 27 21 42 51 26 17 16 21 22 20 249 191 96 69 261 7.860 10.395 11.862 9.656 16.646 19.254 18.572 15.682 13.407 9.774 7.407 30.00 -43.634 -46.257 -46.387 -43.025 -38.480 -21.526 0.616 0.320 0.290 0.420 0.410 0.440 0.410 0.900 1.100 1.020 0.940 0.860 0.820 0.650 0.430 0.350 0.400 1.720 0.940 16 25 29 24 20 13 13 21 23 15 113 72 54 40 26 231 188 193 6.582 8.038 15.400 21.845 21.323 18.032 11.632 8.492 6.182 6.512 8.416 20.00 -45.585 -35.142 -33.766 -37.356 -32.934 -22.510 -4.948 0.750 0.750 0.000 0.330 0.340 0.360 0.380 0.390 0.420 0.340 0.290 1.060 0.840 0.620 1,940 1.430 0.790 0.920 34 24 18 18 23 13 25 81 62 45 26 11 2 5 199 289 212 91 3.292 0.384 -0.206 1.548 5.695 7.802 12.314 18.094 21.845 20.315 14.875 9.715 6.597 10.00 -46.908 -38.689 -30.612 -28.521 -13.469 0.330 0.350 0.340 0.260 0.710 0.590 0.000 0.290 0.340 0.360 0.980 0.760 0.670 1.200 1.110 1.070 0.920 0.900 17 28 31 29 20 .11 2 9 19 18 294 313 227 95 84 51 46 34 -5,644 16.150 22.402 18.284 14.943 14.167 18.344 21.845 18.655 13.024 6.344 -2.438 -4.576 1.504 0.00 -53.209 -43.667 -35.327 -30.890 0.300 0.420 0.280 0.770 0.590 0.000 0.300 0.330 0.300 0.620 0.490 0.640 1.280 0.970 0.800 0.850 0.800 0.680 31 33 30 197 175 103 26 14 6 Z 8 16 26 312 282 170 83 117 8.305 4.055 -10.00 -43.857 -29.566 -15.152 -9.966 -2.334 10.430 18.329 21.939 20.113 16.051 13.927 17.027 19.114 15.729 3.526 4.995 0.940 0.560 0.320 0.260 0.270 0.210 0.270 0.310 1.040 0.990 0.880 0.870 0.740 0.580 0.530 0.520 0.910 0.960 18 14 5 11 24 30 25 20 172 81 8 10 327 44 99 190 617 523 9.754 10.350 10.698 13.075 17.989 20.321 19.600 18.071 14.672 14.245 17.010 18.637 16.953 13.381 11.989 13.513 -20.00 -5.938 4.142 0.290 0.740 0.690 0.620 0.480 0.500 0.930 0.740 0.480 0.340 0.290 0.370 0.230 1.150 0.980 1.040 1.000 1.010 5 11 21 21 14 14 25 17 19 21 16 255 17 13 27 26 531 406 13.672 16.303 19.390 20.336 19.742 18.073 17.194 12.454 11.118 11.965 14.163 16.109 14.289 13.749 14.764 -30.00 29.940 22.436 15.490 0.310 0.370 0.380 0.700 0.560 0.520 0.720 0.650 0.840 0.730 0.510 0.360 0.900 1.000 0.810 0.910 0.960 1.050 10 13 20 25 21 6 6 9 12 207 31 31 37 42 40 31 19 341 12.368 16.251 21.845 20.929 21.218 20.208 6.776 8.383 10.907 10.378 10.061 8.744 9.159 11.603 -40.00 57.192 37.735 22.199 10.626 0.580 0.710 0.850 0.820 0.000 0.290 0.270 0.330 0.630 0.500 1.000 1.010 1.030 1.010 0.990 0.990 0.820 0.860 24 41 34 8 5 4 6 9 8 34 38 47 41 48 41 20 582 367 6.179 10.391 15.497 18.389 21.664 -50.00 53.657 46.697 33.459 23.215 15.275 12.021 10.829 12.479 11.206 10.256 8.707 8.179 7.770 0.200 0.290 0.210 1.120 1.070 0.990 0.840 0.750 0.700 0.570 0.500 0.460 0.530 0.550 0.940 1.020 1.040 1.110 8 11 45 57 58 44 37 86 78 8 8 10 6 20 20 21 583 383 2.300 5.883 11.351 16.191 -60.00 26.140 35.524 34.865 30.741 26.057 21.069 17.844 16.575 16.584 14.795 12.760 11.513 9.573 6.128 0.750 0.670 0.660 0.570 0.400 0.320 0.240 0.260 0.990 0.960 0.930 0.840 0.820 0.810 0.880 0.910 0.970 0.980 95 194 185 30 10 11 7 8 8 35 52 42 485 297 16 23 24 47 27.923 25.893 23.113 20.401 18.260 17.396 16.604 15.919 14.557 12.527 9.624 6.948 7.897 10.923 -70.00 15.276 20.758 26.299 28.463 0.540 0.480 0.430 0.360 0.320 0.900 0.920 0.810 0.680 0.600 0.620 0.580 0.610 0.620 0.680 0.720 0.810 0.610 6 5 5 6 9 39 40 47 41 44 47 70 121 198 210 178 31 408 22.984 20.771 17.240 16.040 21.845 20.132 -80.00 41.303 25.270 16.149 14.896 16.926 16.444 17.506 20.197 14.191 11.088 15.647 25.008 0.310 0.000 0.720 1.090 0.480 1.010 2.030 1.580 1.010 0.210 0.210 0.530 0.460 0.480 1.290 1.820 1.730 1.990 223 226 140 17 12 10 5 4 8 89 99 153 188 58 50 71 84 91

10.00 20.00 30.00 40.00 50.00 60.00 70.00 80.00 90.00 100.00 110.00 120.00 130.00 140.00 150.00 160.00 170.00 0.00 80.00 -6.878 -8.106 -13.998 -25.868 -35.001 -39.684 -33.215 21.127 62.105 36.417 -10.844 -33.513 -38.501 -43.822 -46.528 -10.666 0.822 -61.319 1.480 1.200 1.450 1.760 1.520 1.490 1.590 2.060 2.050 1.750 1.910 2.360 1.030 1.920 0.850 0.780 0.970 1.450 1799 2149 2456 2676 2755 2766 2623 2479 74 82 92 102 124 170 363 617 960 1402 -9.259 -17.969 -30.257 -36.561 -36.766 -20.802 14.148 20.374 1.201 -22.675 -33.843 -39.991 -43.711 -34.959 -20.546 70.00 -4.332 -4.407 -5.352 1.610 1.390 1.420 1.420 1.440 1.690 1.810 1.810 1,670 1.740 1.260 1.560 1.430 1.160 1.460 1.640 1.780 1.940 2752 2999 94 95 101 103 116 272 555 1230 2206 2920 3115 2863 2181 2445 2863 85 -4.504 -15.800 -30.276 -38.910 -44.312 -43.736 -33.871 -17.289 -25.060 -36.973 -40.339 -42.482 -42.064 -35.852 4.941 3.825 1.369 60.00 6.214 0.730 0.670 0.710 0.760 0.900 0.990 0.960 0.860 0.720 0.960 1.080 1.130 1.100 1.010 1.010 0.960 0.760 0.680 2354 3454 3832 3753 2717 1015 925 1852 2811 54 101 270 899 30 32 24 26 53 6.629 -2.321 -12.843 -25.238 -36.873 -47.120 -54.208 -50.497 -40.497 -44.011 -55.246 -52.101 -45.995 -39.847 50.00 12.898 12.952 12.637 11.078 1.940 1.500 1.280 1.040 0.810 0.870 0.910 0.960 1.020 1.150 1.090 1.020 1.310 0.550 0.670 0.670 0.750 0.780 540 37 120 742 1758 3279 3700 3045 1096 446 614 20 18 19 25 23 42 48 5.365 -1.025 -5.119 -18.868 -35.069 -48.444 -56.969 -53.445 -48.071 -52.270 -51.507 -46.805 -43.009 40.00 12.656 13.979 14.819 13.891 10.846 1.090 1.300 1.300 1.320 1.120 0.830 0.990 1.230 1.860 1.350 0.620 0.650 0.720 0.840 0.950 1.010 1.040 0.550 15 15 16 16 21 24 33 32 74 246 411 859 1571 1655 857 373 274 276 4.978 -4.513 -29.974 -35.324 -46.438 -52.325 -50.784 -48.896 -44.135 -44.602 -43.046 6.445 4.013 5.225 30.00 12.843 13.369 12.640 10.324 1.140 1.220 1.370 1.570 1.390 1.410 1.230 1.140 1.200 1.790 2.230 0.410 0.490 0.450 0.520 0.640 0.820 0.960 20 34 56 75 98 137 175 361 458 370 266 193 16 17 17 27 37 17 4.201 -19.862 -27.976 -35.507 -41.292 -47.351 -47.008 -34.270 -44.173 -49.517 1.191 -2.593 4.020 10.368 20.00 9.414 11.381 11.379 8.444 0.460 0.630 0.800 0.870 0.880 0.960 1.050 1.170 1.440 1.490 1.110 0.760 0.910 1.060 1.270 2.050 0.350 0.420 148 300 732 785 456 238 19 16 16 18 17 35 79 156 177 17 19 17 8.851 11.392 15.336 10.825 -12.115 -29.459 -26.825 -32.083 -26.856 -23.435 -24.057 -45.019 -54.741 10.00 6.340 12.097 12.668 8.289 8.167 1.000 0.950 0.920 0.990 0.990 1.230 1.240 1.030 1.190 1.160 1.230 1.630 0.590 0.670 0.840 0.950 0.420 0.500 184 250 556 915 908 544 14 14 20 33 119 240 332 20 13 11 15 18 7.031 13.689 16.368 15.624 14.722 15.195 16.954 16.237 14.046 -4.214 -32.943 -31.225 -28.249 -27.656 21.534 -2.605 -48.104 -52.101 0.00 0.940 0.640 0.760 0.830 0.880 0.830 0.840 0.840 1.030 1.060 1.020 0.950 1.360 1.600 0.370 0.480 0.600 0.620 11 10 15 17 13 18 22 44 106 183 259 319 614 864 753 403 354 16 9.378 6.851 -13.519 -25.733 -28.938 -36.968 -30.220 -10.272 -34.147 -50.548 -10.00 10.670 15.591 18.451 18.697 18.837 19.183 17.142 13.340 0.700 0.600 0.520 0.580 0.750 0.930 0.830 0.920 0.630 0.890 1.630 0.340 0.450 0.550 0.630 0.420 0.520 0.760 19 35 -50 109 197 285 397 482 303 261 521 13 11 14 10 17 14 7 2.943 -5.054 -20.573 -30.879 -30.939 -29.366 -18.927 -3.116 -20.00 13.863 15.011 17.511 18.755 19.407 21.845 16.874 10.741 6.400 3.072 0.740 0.700 0.720 0.830 0.930 0.850 0.650 0.570 0.760 0.650 0.820 0.380 0.480 0.630 0.740 0.450 0.000 0.680 9 17 32 63 94 140 152 239 239 150 444 13 8 8 7 3 6 14 8.179 -9.762 -34.147 -32.451 -10.181 0.735 20.157 -30.00 17.241 17.123 17.262 17.866 18.416 18.345 15.831 11.449 9.974 3.170 -4.388 0.690 0.830 0.660 0.460 C.500 0.620 0.620 0.650 0.730 0.830 0.870 0.820 0.760 0.590 0.610 0.700 0.370 0.540 5 7 5 7 33 43 104 136 219 273 303 375 418 318 12 9 7 7 -40.00 19.208 18.794 19.165 19.349 18.769 18.178 16.394 15.393 15.116 14.062 15.466 14.943 -2.340 -33.245 -27.660 -8.458 4.198 25.551 0.750 0.640 0.650 0.650 0.670 0.710 0.670 0.750 0.740 0.770 0.780 0.730 0.710 0.880 0.660 0.750 0.390 0.490 11 12 16 33 96 137 201 261 273 356 412 616 504 8 5 8 10 9 -7.799 -50.00 20.721 20.195 20.097 20.614 20.295 19.147 17.956 17.070 16.951 15.905 18.507 19.331 1.543 -19.951 -12.272 -4.005 19.457 0.330 0.420 0.530 0.610 0.650 0.660 0.660 0.690 0.680 0.730 0.800 0.780 0.830 0.800 0.660 0.750 0.770 0.870 11 12 18 13 15 30 109 168 203 250 356 574 666 662 749 9 7 10 -60.00 21.845 20.871 20.715 20.998 21.446 21.100 20.171 18.735 16.975 16.785 16.405 16.064 13.415 4.133 -4.311 -3.733 0.163 14.441 0.480 0.550 0.600 0.590 0.610 0.600 0.580 0.640 0.650 0.610 0.610 0.630 0.700 0.820 0.000 0.260 0.330 0.430 9 7 12 13 18 29 92 141 143 289 428 641 739 855 769 4 7 7 -70.00 14.604 18.726 20.067 20.641 21.091 21.410 21.082 20.291 19.261 17.903 16.958 16.087 15.055 13.564 10.373 7.372 8.186 9.163 0.500 0.490 0.450 0.530 0.600 0.530 0.490 0.510 0.520 0.240 0.300 0.330 0.360 0.430 0.470 0.470 0.370 0.310 48 71 84 172 323 427 508 632 485 13 14 9 8 8 8 18 34 44 -80.00 21.024 21.698 21.617 21.606 21.834 22.034 20.423 17.987 16.565 16.763 12.956 12.524 14.182 12.112 18.229 27.148 41.641 43.323 2.720 3.100 2.490 1.720 1.410 0.990 0.210 0.500 0.310 0.110 0.260 0.420 0.520 0.520 1.620 2.540 1.050 0.660 14 15 22 23 26 33 43 48 66 71 86 90 93 89 84 80 135 133