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1 **Morphological transitions for pore water and pore air during drying and wetting processes**
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8 **in partially saturated sand**

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15 **Abstract**

16 Water retention characteristics are important for modeling the mechanical and hydraulic behavior of partially
17 saturated sand. It is well known that the soil water characteristic curve shows hysteresis during drying and wetting
18 processes. For a better understanding of the water retention characteristics of partially saturated soil, a microscopic
19 investigation of the morphological transitions for the pore water phase and the pore air phase, such as volume
20 distribution, spatial distribution and continuity during drying and wetting processes, is crucial. In the present study,
21 different water retention states of a partially saturated sand were visualized during water retention tests using
22 microfocus x-ray computed tomography (CT). The CT images obtained from the tests were segmented into the soil
23 particle phase, the pore water phase and the pore air phase. Then, a series of image processing, erosion, dilation and
24 cluster labeling, was applied to the images in this order to quantify the cluster volume distributions, the number of
25 clusters and the continuity of both the pore water phase and the pore air phase. The morphological transitions for the
26 pore air phase and the pore water phase, subjected to decreasing and increasing degrees of saturation, were revealed
27 using the results of the image processing, and then the water retention states were characterized based on the
28 morphologies for the two phases. The influence of the morphologies on the hysteresis was discussed.

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30 Keywords: Partially saturated sand, Water retention test, Microfocus x-ray CT, Image processing, Morphology, Water
31 retention state

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34 **1. Introduction**

35 The relationship between suction and the degree of saturation for partially saturated soil is interpreted as the soil
36 water retention curve (SWRC). The SWRC is an important characteristic for the hydraulic and mechanical behavior of
37 partially saturated soil. Thus, a modeling of the SWRC that incorporates the effect of the hydraulic hysteresis of the
38 water retention characteristics into the shear strength, permeability and volume change of partially saturated soil was
39 developed (e.g., [5, 9, 11, 33, 44]). The hysteresis shown during the drying and wetting processes by the SWRC was
40 observed through water retention tests (e.g., [8, 13, 20, 43]), and the water retention capability was found to significantly
41 depend on the bulk density of the soil and the particle size distribution (e.g., [10, 39]). The main causes of the hysteresis
42 have been interpreted as follows: 1) the ink-bottle effect due to irregularities in the size and connectivity of the pores
43 (e.g., [34]) and 2) the contact angle hysteresis at the interface between a liquid and a solid during the drying and wetting
44 processes (e.g., [3, 6]). Up to now, these mechanisms at the pore scale have generally been expressed by schematic
45 illustrations (e.g., [2, 30]). For a better understanding of these mechanisms, a microscopic investigation of the water
46 retention behavior in particulate soils is important.

47 The purpose of the present study is to reveal the microscopic water retention behavior of partially saturated sand
48 using microfocus x-ray computed tomography (CT). Microfocus x-ray CT is an effective tool for nondestructively and
49 three-dimensionally visualizing the microstructures of geomaterials or porous media; it has been widely used for
50 investigating the failure mechanism of particulate soils with strain localization (e.g., [1, 7, 17, 37]) and particle
51 morphological features of granular geomaterials [31]. Spatial resolution and image processing techniques for

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52 microfocus x-ray CT have been developed, resulting in the ability to segment the phases in an object at the microscopic
53 scale and to investigate the microstructural changes in soils [e.g., [36]]. For partially saturated sands, microfocus x-ray
54 CT has been applied to investigations of water retention states and the evolution of pore-scale quantities. The
55 investigations have been done through triaxial compression tests (e.g., [17, 18, 21, 26]) and water retention tests (e.g.,
56 [4, 16, 19, 20, 22, 24, 28, 29, 35]).

57 Changes in the degree of saturation in partially saturated soil involve morphological transitions for both water and
58 air in void spaces, which cause variations in the water retention states. Microscopic investigations of the morphologies
59 for the pore water phase and the pore air phase, and their transitions during the drying and wetting processes, provide
60 important data for classifying the water retention states and contribute to elucidating the mechanism of the hysteresis.
61 The morphologies of pore water for partially saturated soils, such as the shape of the liquid bridges and the distribution
62 of pore water, have been extensively studied. Observations of the morphologies have been done using a scanning
63 electron microscope (SEM) and an environmental scanning electron microscope (ESEM) (e.g., [12, 40]). Mercury
64 intrusion porosimetry (MIP) is the other approach for studying pore water morphologies based on pore space
65 morphologies (e.g., [38, 40]). Although SEM and ESEM provide high resolution images sufficient for visualizing the
66 liquid bridges, the images are limited to those that capture small portions of the sample surfaces. Recently, microfocus
67 x-ray CT with image analyses has been applied to investigate the pore water morphologies in three-dimensional
68 conditions (e.g., [23, 27, 32, 41, 46]). The morphologies of both pore water and pore air, and their transitions during
69 triaxial compression tests and water retention tests, need further study. In addition, the morphological transitions for

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70 pore fluids with a variation in the degree of saturation are essential for interpreting the relationship between the water
71 retention characteristics and the mechanical behavior during shearing as well as the permeability of partially saturated
72 soil (e.g., [14, 18, 26, 42]).

73 In the present study, a water retention test was performed on sand, and the various water retention states subjected
74 to drying and wetting were visualized using microfocus x-ray CT. The CT images obtained in the tests were segmented
75 into the soil particle phase, the pore water phase and the pore air phase (trinarization). A series of image processing,
76 erosion, dilation and cluster labeling, was applied to the trinarized images to quantify the volume distributions, the
77 number of clusters and the continuity for the pore water phase and the pore air phase. The morphologies for the pore
78 water phase and the pore air phase at given degrees of saturation and their transitions during the drying and wetting
79 processes were clearly specified using the results of the image processing. Then, the water retention states which have
80 been schematically explained were interpreted based on the morphologies for the two phases. Through comparisons
81 of the analysis results using the images obtained at almost the same degrees of saturation during drying and wetting,
82 the influence of the morphologies for the two phases on the hysteresis was examined.

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83 **2. Material and Experimental Setup**

84 The sample used in the present study is Toyoura sand. Figure 1 shows the grain size distribution curve of Toyoura
85 sand, while the physical properties of this sand are listed in Table 1. The diameter D_{50} of Toyoura sand is 190 μm .
86 Figure 2 shows a schematic illustration of the test apparatus consisting of an acrylic hollow cylinder (18.0 mm in inner
87 diameter and 18.0 mm in height), an acrylic pedestal (35.0 mm in diameter), a saturated ceramic disc, a double-tube
88 burette and a water tank. The air-entry pressure of the ceramic disc was 50 kPa, which is sufficiently larger than the
89 water retention capability of Toyoura sand; thus, the suction imposed on the Toyoura sand could be controlled by the
90 ceramic disc. A loose (low bulk density) sand specimen was prepared by the water pluviation technique; namely, the
91 Toyoura sand was poured from a certain height into the hollow cylinder that was initially filled with water. The specimen
92 conditions are listed in Table 2. It is seen in the x-ray tomographic images that tiny air bubbles were trapped at the
93 initial condition. In the present study, it was assumed that the volume of trapped air bubbles was sufficiently small and
94 that the degree of saturation at the initial state was 100%.

95 The water retention test in the present study was started by conducting the drying process using a negative water
96 column [45]. Suction was applied making sure the water level in the burette was lower than the top of the specimen
97 (Fig. 2); the water level in the burette was varied until equilibrium was reached (about 1 day for the studied specimen).
98 The applied suction was then seen to correspond to the water head difference between the water level in the burette and
99 the top of the specimen. A level of suction that corresponded to the air-entry pressure of Toyoura sand (2 kPa) was
100 firstly applied and then a step-by-step increase in suction was applied up to 10 kPa during the drying process. The

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8 102 gauge installed on the burette. After the drying process, the wetting process was started by decreasing the suction from
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14 104 water absorption at each equilibrium were measured by the differential pressure gauge. It should be noted that the
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18 105 experiment was carried out in a temperature-controlled room at 20 degrees C, and the top of the specimen was exposed
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21 106 to an atmospheric pressure with almost 100% humidity through the water tank to minimize water evaporation.
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25 107 At each equilibrium during the drying and wetting processes, the three-phase microstructures in the specimen were
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28 108 visualized using a microfocus x-ray CT apparatus “KYOTO-GEO μ XCT (TOSCANER-32250 μ hdk)” (e.g. [17]). Its
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31 109 specifications are listed in Table 3. The scan area and the scan conditions are shown in Fig. 3. The entire specimen was
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34 110 observed by global tomography, while the local region of interest focusing on the middle height of the specimen was
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37 111 observed by local tomography. The materials comprising the sand specimen are distinguished from each other based
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41 112 on the level of attenuation of the x-ray, that is, the distribution of the CT values had a 16-bit signed integer. It is
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44 113 empirically known that the relation between the levels of attenuation of x-ray and the CT values is linear (e.g. [7, 17]).
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47 114 As indicated by Fig. 3, each phase can be identified by different grayscale colors in a CT image as follows: the brighter
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50 115 gray portion corresponds to soil particles, the black portion corresponds to air, the darker gray portion corresponds to
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53 116 water and the white portion corresponds to metal inclusions.
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118 3. Image Analysis Methods

119 3.1. Trinarization

120 In the present study, the soil particle phase, the pore water phase and the pore air phase in the three-dimensional
121 tomographic volume were segmented using the region growing method (e.g. [19]). The region growing method is a
122 segmentation method for digital images that postulates that the adjacent voxels with gray values similar to a chosen
123 voxel are assimilated into the same phase. A certain voxel representing the gray value of a phase is firstly chosen as the
124 “initial seed”. Subsequently, the voxels adjacent to the initial seed are extracted as the same phase when their gray
125 values are smaller than the tolerance limit. To distinguish between the three phases using the region growing method,
126 a suitable tolerance for each phase is needed. In the CT images scanning partially saturated sand, a voxel often shares
127 more than two phases. Specifically, voxels sharing the soil particle phase and the pore air phase are often misidentified
128 as the pore water phase owing to the partial volume effect (e.g., [19, 20, 25]). In the present study, the levels of tolerance
129 for the region growing of the soil particle phase and the pore air phase were determined by taking the partial volume
130 effect into account in the following steps. Firstly, the gray value distributions for the soil particle phase, the pore water
131 phase and the pore air phase were assumed as normal distributions, while those for the three types of phases due to the
132 partial volume effect, namely, the voxels sharing the soil particle phase and the pore water phase, the voxels sharing
133 the pore water phase and the pore air phase and the voxels sharing the pore air phase and the soil particle phase, were
134 assumed as uniform distributions, as shown in Fig. 4. Subsequently, the superposition of the weighted gray value
135 distributions for the six phases was determined using the maximum likelihood estimation method so that it was close

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5 136 to the gray value distribution of the original CT image. Once the superposition was estimated, the level of tolerance for
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11 138 pore air phase and the intersection of the normal distributions for the pore air phase and the pore water phase, as shown
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14 139 in Fig. 5. Similarly, the level of tolerance for extracting the soil particle phase was determined as the interval between
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18 140 the mean value of the normal distribution for the soil particle phase and the intersection of the soil particle phase and
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21 141 the pore water phase. The remaining voxels after the extraction of the pore air phase and the soil particle phase were
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24 142 considered as the pore water phase. Prior to the trinarization, a median filter with 5^3 voxels was applied to the CT
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27 143 images obtained in the present study to reduce noise. The median filter was applied and region growing was performed
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31 144 using the 3D image analysis software VGStudioMax3.1 (Volume Graphics GmbH). Examples of the original CT image
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34 145 and the trinarized image are shown in Fig. 6 in which the gray, blue and black colors denote the soil particle phase, the
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37 146 pore water phase and the pore air phase, respectively.

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41 147 To investigate the accuracy of the measuring volumes of the pore water phase and the pore air phase using the
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44 148 trinarization technique, validation work was conducted. A specimen with a height of 12 mm, a diameter of 6 mm, a
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47 149 void ratio of 0.846 and a degree of saturation of 0.662 was prepared, as shown in Fig. 7. Toyoura sand was packed in
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50 150 an acrylic cylinder by the moist tamping method. Two kinds of X-ray CT scans were performed with spatial resolutions
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53 151 of $6.72 \mu\text{m}$ (Case A) and $12.25 \mu\text{m}$ (Case B). Then, the void ratio and the degree of saturation, calculated using
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56 152 trinarization, were compared with those of the specimen. The specimen was small enough to be observed in its entirety
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60 153 even with the high spatial resolution of $6.72 \mu\text{m}$. The results are listed in Table 4. The void ratio and the degree of

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8 155 values than Case B, which indicates that the higher the resolution of the CT image is, the more accurate the trinarization
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11 156 will be. The gray value histograms for Cases A and B are shown in Figs. 8a and 8b, respectively. It is found from these
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18 158 method is similar to that of the original distribution for both cases. As shown in Fig. 8b, for Case B, the proposed
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21 159 technique describes the influence of the partial volume effect which leads to a relatively larger amount of frequency
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24 160 between the pore water phase and the soil phase. These results confirm that the proposed trinarization technique is a
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28 161 reasonable segmentation technique for partially saturated sand.
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32 33 34 35 163 **3.2. Morphology analysis** 36

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45 166 phase extracted from the trinarized volumes were divided into some assemblies with individual continuity. Hereafter,
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48 167 they are referred to as “clusters” using the 3D image analysis software Avizo9.4.0 (FEI). The procedure for the
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51 168 morphology analysis of the pore water phase is as follows. Firstly, the pore water phase is extracted from the trinarized
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55 169 volume to provide the binary volume in which the blue portion is the pore water phase and the black portion is the
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58 170 background phase, as shown in Fig. 9b. The binary volume contains pore water voxels due to the partial volume effect
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5 171 between the soil particle phase and the pore air phase as well as the absorbed water that surrounds the soil particles.
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8 172 Erosion and dilation are performed in this order to remove those voxels. Erosion is the morphological operator which
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15 174 while dilation is the morphological operator which combines the two sets using the vector addition of set elements to
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18 175 fill in the voids in the digital image (e.g., [15]). A structuring element that is composed of a center voxel and the
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21 176 neighboring six voxels is defined for the erosion and the dilation. For the erosion, the target pore water voxel centered
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24 177 at the structuring element is replaced with a background voxel when one of the neighboring six voxels corresponds to
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27 178 the background voxel. In contrast, for the dilation, the target background voxel centered at the structuring element is
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31 179 replaced with a pore water voxel when one of the neighboring six voxels corresponds to the pore water voxel. It is
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34 180 assumed that the one-voxel erosion-dilation image processing sufficiently removes the voxels due to the partial volume
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37 181 effect as well as the voxels due to the absorbed water. Once this processing has been done, the pore water phase is
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40 182 clusterized, as shown in Fig. 9c. The separated pore water is labeled by assigning a unique number to all adjacent voxels
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43 183 that constitute a cluster. Each cluster exhibits a different consecutive number starting with the value 1. In Fig. 9d, each
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47 184 color describes a unique number for each cluster. The cluster volumes and the number of clusters are quantified by
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50 185 counting the number of voxels that constitute each cluster in the labeled images.
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188 **4. Results**

189 **4.1. Water retention curve**

190 Figure 10 describes the water retention curve. The wetting curve is located below the drying path at a given degree
191 of saturation; i.e., hysteresis is clearly observed.

192 The degree of saturation begins to decrease at a suction of 1.9 kPa (point “b”) to that of 9.8 kPa (point “g”) in the
193 drying process, while it begins to increase at a suction of 1.9 kPa (point “h”) in the wetting process. The degree of
194 saturation at a suction of 0.0 kPa at the end of the wetting process is less than 100%, which indicates that air bubbles
195 have been trapped due to drying and wetting in this order.

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197 **4.2. Local void ratio and degree of saturation**

198 In Fig. 10, the symbols from “a” to “l”, except for “h” and “l”, indicate the points at which the specimen is in
199 equilibrium, and x-ray CT scanning and trinarization were performed. Points “h” and “l” are omitted because the
200 obtained images were of low quality due to mechanical problems. Figure 11 shows examples of the horizontal and
201 vertical cross sections of the local tomography images and the trinarized images during the drying and wetting processes.
202 It is clearly observed that the black portion, indicating the pore air phase, increases in the drying process, whereas the
203 blue portion, indicating the pore water phase, increases in the wetting process. The local void ratio and the degree of

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5 204 saturation were quantified by counting the number of voxels for the three phases (the soil particle phase, the pore air
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8 205 phase and the pore water phase) in the trinarized volumes. Figure 12 shows the local void ratios at each degree of
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11 206 saturation. It is seen that the local void ratios are comparable with the global void ratios. Figure 13 shows a comparison
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18 208 with the trinarized volumes and the suction imposed on the specimen. Figure 13 indicates that the water retention curve
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21 209 is qualitatively described by trinarization, although the local degrees of saturation tend to be relatively larger than the
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24 210 global degrees of saturation of the specimen. One of the causes is that the initial global degree of saturation, assumed
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27 211 to be 100%, is larger than the real one due to the trapped air bubbles. Another possible reason is that the trinarized
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34 213 heterogeneity of the degree of saturation. In addition, the degrees of saturation shown in this figure are calculated using
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37 214 the trinarized volumes including the voxels for the pore water phase due to the partial volume effect.
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47 216 **4.3. Morphological transitions for pore water and pore air**

50 217 ***4.3.1 Distributions of cluster volume for pore air and pore water***

54 218 Figures 14a and 14b show the cluster volume distribution curves (CVDCs) of the pore air and the pore water,
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57 219 respectively. The cluster volume used as a horizontal axis in these figures is the number of voxels that constitute each
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60 220 cluster, while the vertical axis is the cumulative ratio of each cluster volume to the total cluster volume, i.e., the
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5 221 proportion of clusters within a certain volume. In Fig. 14a, the pore air clusters with a volume of 10^3 to 10^5 voxels exist
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15 224 than 10^6 voxels is observed at the cumulative volume of 100%. This suggests that the pore air clusters with smaller
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18 225 volumes connect to each other, forming a large pore air cluster with a decreasing degree of saturation. Further
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21 226 desaturation up to point “g” provides a larger pore air cluster. On the contrary, a larger pore air cluster loses its volume
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24 227 and is divided into smaller clusters during the wetting process from points “g” to “k”.

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29 228 In Fig. 14b, the CVDC of the pore water exhibits an opposite trend to that of the pore air during the drying and
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32 229 wetting processes. A large pore water cluster exists at higher degrees of saturation and gradually loses its volume during
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35 230 the drying process, which is finally divided into smaller pore water clusters at lower degrees of saturation. The smaller
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39 231 pore water clusters tend to merge together into a large pore water cluster during the wetting process. As indicated by
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42 232 Fig. 14b, the cumulative volume of a pore water cluster with a volume of 10^4 voxels is less than 10% at degrees of
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45 233 saturation higher than 28% (points without “f” and “g”) and a pore water cluster with a volume larger than 10^8 voxels
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48 234 shows 100% cumulative volume. On the other hand, a pore water cluster with a volume of 10^4 voxels shows 100%
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51 235 cumulative volume at degrees of saturation lower than 28% (points “f” and “g”). This indicates that the volume of 10^4
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54 236 voxels for the pore water cluster seems to be the threshold between smaller volume clusters and a large volume cluster
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58 237 for Toyoura sand. The large volume cluster of the pore water phase is larger than 10^8 voxels.

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4.3.2 Continuity and number of clusters for pore air and pore water

The maximum number of voxels that constitute a cluster, that is, the maximum volume (V_{max}) of a cluster out of all the clusters, was evaluated. Figures 15a and 15b show the V_{max} of the pore air and pore water clusters at each degree of saturation, respectively. The symbols in these figures correspond to the x-ray scanning points shown in Fig. 10. In Fig. 15a, the V_{max} of the pore air cluster increases from points “c” to “g” in the drying process and then gradually decreases from points “g” to “k” in the wetting process. On the contrary, the V_{max} of the pore water cluster decreases in the drying process and increases in the wetting process, as shown in Fig. 15b. Figures 16a and 16b show the total volumes (V_{total}) of the pore air and pore water clusters at each degree of saturation, respectively. For pore air, the V_{total} is larger than the V_{max} at points “a”, “b”, “c” and “k” where the degrees of saturation are higher than 60%. The same trend is observed for the pore water at points “f” and “g” where the degrees of saturation are lower than 20%. For the other points, the V_{total} for both the pore air and pore water clusters is almost identical to the V_{max} .

In the present study, continuity is defined as the ratio of V_{max} to V_{total} . It should be noted that continuity is defined as an indicator for discussing the water retention states; it does not directly describe whether or not the pore water is continuous in real soil. Figures 17a, 17b and 17c show the labeled images of the pore water cluster with continuity of 100.00% (point “a”), 97.26% (point “e”) and 0.10% (point “f”), respectively. Continuity of almost 100% means that one cluster occupies the total volume of clusters, whereas continuity of 0.10% means that the individual clusters exist

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5 255 independently and spatially. A large cluster and some smaller clusters coexist when the continuity is about 97.26%, as
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8 256 demonstrated in Fig. 17b. Figure 18 shows examples of pore water clusters with different volumes at point “e” where
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11 257 the continuity of the pore water phase is almost 97.26%. The erosion-dilation image processing, aimed at removing the
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14 258 pore water voxels from the grain surface, possibly removes the voxels of the capillary bridges created between grains.
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18 259 Nevertheless, it is apparent from this figure that the pore water clusters with volumes smaller than 10^3 voxels (2.1×10^5
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21 260 μm^3) form capillary bridges between the grains and that the clusters with a larger volume exhibit the same shape as
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24 261 some of the connected small clusters. If the volume of a pore water cluster is larger than 10^4 voxels ($2.1 \times 10^6 \mu\text{m}^3$), as
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27 262 shown in Fig. 18, the pore water phase becomes continuous with a volume of 10^8 voxels ($2.1 \times 10^{10} \mu\text{m}^3$). Figures 19a,
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31 263 19b and 19c show the labeled images of pore air clusters with different levels of continuity. The figures indicate that
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34 264 the pore air clusters exist as bubbles when the continuity is near 0% and they connect to each other to form a large pore
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37 265 air cluster with an increase in continuity. Figure 20 shows examples of pore air clusters with different volumes. It can
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40 266 be seen from this figure that the pore air cluster with a volume smaller than 10^5 voxels exists as a bubble, while that
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43 267 with a volume of 10^6 voxels seems to be a continuous cluster comprising some air bubbles. In other words, a volume
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46 268 of 10^6 voxels seems to be the threshold of a morphological transition for the pore air between small volume clusters
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53 270 Figures 21a and 21b show the relations of the global degrees of saturation with continuity for pore air and with
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56 271 continuity for pore water, respectively. The continuity for pore air at degrees of saturation higher than 80% is smaller
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60 272 than 10% and it is nearly 100% at degrees of saturation lower than 80% without point “c”. On the other hand, the

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273 continuity for pore water at degrees of saturation lower than 30% is almost 0% and it is almost 100% at degrees of
274 saturation higher than 30%. In other words, pore air becomes continuous while losing the continuity of pore water in
275 the drying process, and pore water becomes continuous while losing the continuity of pore air in the wetting process.
276 It is also clearly seen in Fig. 21 that the continuity for both pore air and pore water is relatively large at degrees of
277 saturation between 30% and 80%. This indicates that the pore air phase and the pore water phase are mostly continuous
278 during a certain range of degrees of saturation in the middle of the drying and wetting processes.

279 Figures 22a and 22b show the number of clusters of pore air and pore water, respectively. At higher degrees of
280 saturation, a lot of pore air clusters and a smaller number of pore water clusters exist. Along with lower degrees of
281 saturation, comes the tendency for a larger number of pore water clusters to exist with a decreasing number of pore air
282 clusters.

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5. Discussions

The results of the morphology analysis for Toyoura sand, including the continuity, the cluster volume and the number of clusters for pore air and pore water, are summarized in Fig. 23. Firstly, pore air is discontinuous; therefore, smaller pore air clusters exist at almost fully saturated conditions (points “a” and “b”). In this case, a continuous pore water cluster with a large volume occupies the void spaces in the sand, as shown in Fig. 17a; smaller air bubbles are spatially trapped in the void spaces, as shown in Fig. 19a.

As desaturation proceeds until degrees of saturation lower than the AEV (points “c”, “d” and “e”), morphologies for both the pore air phase and the pore water phase start to change. Specifically, discontinuous pore air clusters with smaller volumes connect to each other forming a continuous pore air cluster with a large volume, as shown in Fig. 19b, whereas continuous pore water begins to be separated into smaller pore water clusters, for example, as shown in Fig. 17b. In other words, a continuous phase with a large volume and a discontinuous phase with a smaller volume exist together in the void spaces. In the water retention state, along with lower degrees of saturation, comes a larger number of pore water clusters.

With a further decrease in the degrees of saturation (points “f” and “g”), a continuous pore air cluster becomes larger and then only discontinuous pore water clusters with smaller volumes exist. This suggests that capillary bridges exist spatially at the grain contacts, as shown in Figs. 17c and 18. In the wetting process, pore air and pore water become

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300 continuous with increasing degrees of saturation, after which the pore air becomes discontinuous and the pore water
301 becomes continuous.

302 The results of the morphology analysis confirmed that the morphologies for pore air and pore water in partially
303 saturated sand can be identified as follows: i) a continuous and large volume and ii) discontinuous and smaller volumes.
304 Then, the water retention states of partially saturated sand can be classified using the two kinds of morphologies for the
305 two phases as the following three states: 1) a state at which discontinuous pore air (trapped air) and continuous pore
306 water coexist, 2) a state at which continuous pore air and continuous pore water coexist and 3) a state at which
307 continuous pore air and discontinuous pore water (capillary bridges) coexist.

308 Figure 14b suggests that there is a threshold where the morphology of pore water starts to transit, i.e., discontinuous
309 pore water clusters with smaller volumes become a continuous pore water cluster with a large volume and vice versa.
310 In the present study, the threshold was, for example, about 0.6 times as large as a soil particle of Toyoura sand (2.1×10^6
311 μm^3). Similarly, Fig. 14a suggests that there is a threshold where the morphology of pore air starts to transit, and its
312 value was about 60 times as large as a soil particle of Toyoura sand ($2.1 \times 10^8 \mu\text{m}^3$). These trends can probably be
313 attributed to the uniformity of the pore volumes in the Toyoura sand which is a poorly graded sand. On the other hand,
314 the threshold of pore air is not as clear as that of pore water. In other words, pore air clusters with a larger variety of
315 volumes spatially distribute more in partially saturated sand than pore water clusters. A morphology analysis for sand
316 with various grain size distributions or bulk densities will contribute to clarifying the mechanism of the morphological
317 transitions for both pore air and pore water.

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318 In cases where partially saturated sand is subjected to drying and wetting in this order, pore air and pore water
319 experience continuous or discontinuous morphology. Then, the water retention states transit as follows: states 1), 2) and
320 3) in this order during the drying process and states 3), 2) and 1) in this order during the wetting process. These histories
321 correspond to the states demonstrated in Figs. 17a, 17b and 17c during the drying process and the states demonstrated
322 in Figs. 17c, 17b and 17a during the wetting process. Assuming that the above water retention states correspond to
323 those suggested by Bear [2], insular air saturation, funicular saturation and pendular saturation correspond to states 1),
324 2) and 3), respectively.

325 A comparison of the results at similar degrees of saturation during the drying and wetting processes, given in Fig. 10,
326 examines the relationship between the morphological transitions of pore fluid (pore air and pore water) and hysteresis.
327 Comparisons of the results at such points, e.g., “d” and “j”, and “e” and “i” in Fig. 23, confirm that both pore water and
328 pore air are continuous at any point. Thus, there is no significant difference in microscopic morphologies for pore air
329 and pore water at similar degrees of saturation during the drying and wetting processes evaluated by the morphology
330 analysis even though the water retention curve apparently exhibits hysteresis. It is possible that the difference in the
331 principal curvatures of the capillary bridges, which leads to different levels of suction even when the degrees of
332 saturation are similar, probably causes the hysteresis.

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334 **Conclusions**

335 X-ray CT images, scanning different water retention states with high spatial resolution, were analyzed using a
336 morphology analysis to investigate the volume distributions, continuity and number of clusters for pore air and
337 pore water with a variation in the degree of saturation. Then, the morphologies for the two phases were clearly
338 specified based on the results.

339 The analysis confirmed that pore air and pore water in partially saturated sand exhibit two kinds of
340 morphologies: a continuous and large volume and discontinuous and smaller volumes. In the drying process,
341 continuous pore water was divided into discontinuous pore water clusters, i.e., capillary bridges. In contrast,
342 discontinuous pore air bubbles connected to each other and formed a continuous pore air cluster with a large
343 volume. In the wetting process, the opposite behavior was observed. Based on the morphologies, the water
344 retention states were classified into three states at certain degrees of saturation: 1) the state at which discontinuous
345 pore air (trapped air) and continuous pore water coexist, 2) the state at which both pore air and pore water are
346 continuous and 3) the state at which continuous pore air and discontinuous pore water (capillary bridges) coexist.
347 In addition, there are probably thresholds between the discontinuous clusters with smaller volumes and the
348 continuous cluster with a large volume for both pore air and pore water. The water retention curve exhibited
349 apparent hysteresis; however, the morphology analysis revealed that there was no significant difference in the
350 morphologies for pore air and pore water at similar degrees of saturation during the drying and wetting processes.

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351 The discussions in the present study were made based on the local tomographic volume that is a small portion
352 of the entire specimen. Microscopic investigations of the entire specimen, such as the spatial distribution and the
353 homogeneity of the morphologies, should be conducted in the future.

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References

361
362 1. Andò E, Hall SA, Viggiani G, Desrues J, Bé-suelle P (2012) Grain-scale experimental investigation of localised
363 deformation in sand: a discrete particle tracking approach. *Acta Geotechnica* 7(1):1–13
364 2. Bear J (1979) *Hydraulics of groundwater*. New York, McGraw-Hill:190–224
365 3. Blake TD, Haynes IM (1973) Contact-angle hysteresis. *Progress in surface and membrane science* 6:125–138
366 4. Bruchon JF, Pereira JM, Vandamme M, Lenoir N, Delage P, Bornert M. (2013) Full 3D investigation and
367 characterization of capillary collapse of a loose partially saturated sand using X-ray CT. *Granular Matter*
368 15(6):783–800
369 5. Chiu, DF, Ni XW, Zhang LS (2014) Effect of hydraulic hysteresis on shear strength of partially saturated clay and
370 its prediction using a water retention surface. *Engineering Geology* 173:66–73
371 6. De Souza EJ, Gap L, McCarthy TJ, Arzt E, Crosby AJ (2008) Effect of contact angle hysteresis on the
372 measurement of capillary forces. *Langmuir* 24(4):1391–1396
373 7. Desrues J, Chambon R, Mokni M, Mazerolle F (1996) Void ratio evolution inside shear bands in triaxial sand
374 specimens studied by computed tomography. *Géotechnique* 46(3):539–546
375 8. Feia S, Ghabezloo S, Bruchon JF, Sulem J, Canou J, Dupla JC (2014) Experimental evaluation of the pore-access
376 size distribution of sands. *Geotechnical Testing Journal* 37(4):613–620
377 9. Fredlund DG, Xing A, Fredlund MD, Barbour SL (1995) The relationship of the partially saturated soil shear
378 strength to the soil-water characteristic curve. *Canadian Geotechnical Journal* 33(3):440–448
379 10. Gallage CPK, Uchimura T (2010) Effects of dry density and grain size distribution on soil-water characteristic
380 curves of sandy soils. *Soils and Foundations* 50(1):161–172
381 11. Gallipoli D, Wheeler S, Karstunen M (2003) Modelling the variation of degree of saturation in a deformable
382 partially saturated soil. *Géotechnique* 53(1):105–112
383 12. Gvirtzman H, Magaritz M, Klein E, Nadler A (1983) A scanning electron microscopy study of water in soil.
384 *Transport in Porous Media* 2:83–93
385 13. Haines WB (1930) Studies in the physical properties of soil – V: The hysteresis effect in capillary properties and
386 the modes of water distribution associated therewith. *Journal of Agricultural Science* 20(1):97–116
387 14. Hamamoto S, Moldrup P, Kawamoto K, Sakaki T, Nishimura T, Komatsu T (2016) Pore network structure linked
388 by X-ray CT to particle characteristics and transport parameters. *Soils and Foundations* 56(4):676–690
389 15. Haralick, RM, Sternberg, SR, Zhuang, X (1987) Image analysis using mathematical morphology. *IEEE*
390 *transactions on pattern analysis and machine intelligence* 9(4):532–550
391 16. Hashemi MA, Khaddour G, François B, Massart TJ, Salager S (2014) A tomographic imagery segmentation
392 methodology for three phase geomaterials based on simultaneous region growing. *Acta Geotechnica* 9(5):831–
393 846
394 17. Higo Y, Oka F, Kimoto S, Sanagawa T, Matsushima Y (2011) Study of strain localization and microstructural
395 changes in partially saturated sand during triaxial tests using microfocus X-ray CT. *Soils and Foundations*

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396 51(1):95–111

397 18. Higo Y, Oka F, Sato T, Matsushima Y, Kimoto S (2013) Investigation of localized deformation in partially
398 saturated sand under triaxial compression by microfocus X-ray CT with digital image correlation. *Soils and*
399 *Foundations* 53(2):181–198

400 19. Higo Y, Oka F, Morishita R, Matsushima Y, Yoshida T (2014) Trinarization of μ X-ray CT images of partially
401 saturated sand at different water retention states using a region growing method. *Nuclear Instruments and Methods*
402 *in Physics Research B* 324:63–69

403 20. Higo Y, Morishita R, Kido R, Khaddour G, Salager S (2015a) Local water retention behavior of sand during drying
404 and wetting process observed by micro x-ray tomography with trinarization. *The 15th Asian Regional Conference*
405 *on Soil Mechanics and Geotechnical Engineering, Japanese Geotechnical Society Special publication* 2(16):635–
406 638

407 21. Higo Y, Oka F, Morishita R, Matsushima Y (2015b) Quantitative observation of strain localisation in a partially
408 saturated triaxial specimen using microfocus X-ray CT with image analysis. In: *proceedings of the 10th*
409 *International Workshop on Bifurcation and Degradation in Geomaterials*:325–330

410 22. Higo Y, Kido R, Takamura F, Fukushima Y (2018) Pore-scale investigations of partially water-saturated granular
411 soil. *Mechanics Research Communications* 94:1–7

412 23. Khaddour G, Salager S, Higo Y, Andò E, Desrues J (2015) Discrete analysis of water phase evolution within
413 unsaturated soil. In: *proceedings of the 2nd International Conference on Tomography of Materials and Structures,*
414 *30th June-3rd July 2015, Quebec, Canada*

415 24. Khaddour G, Riedel I, Ando E, Charrier P, Besuelle P, Desrues J, Viggiani G, Salager S (2018) Grain-scale
416 characterization of water retention behaviour of sand using X-ray CT. *Acta Geotechnica* 13:497–512

417 25. Kido R, Higo Y (2017a) Evaluation of distribution of void ratio and degree of saturation in partially saturated
418 triaxial sand specimen using micro x-ray tomography. *Japanese Geotechnical Society Special Publication* 5(2):22–
419 27

420 26. Kido R, Higo Y, Salager S (2017b) Microscopic investigation of progressive changes of pore water distribution in
421 shear band of unsaturated sand under triaxial compression. In: *proceedings of the 19th International Conference*
422 *on Soil Mechanics and Geotechnical Engineering*:1171–1174

423 27. Kido R, Higo Y (2019) Distribution changes of grain contacts and menisci in shear band during triaxial
424 compression test for unsaturated sand. *Japanese Geotechnical Society Special Publication* 7(2):627–635

425 28. Kim FH, Penumadu D, Hussey DS (2012) Water distribution variation in partially saturated granular materials
426 using neutron imaging. *Journal of Geotechnical and Geoenvironmental engineering* 138(2):147–154

427 29. Kim FH, Penumadu D, Gregor J, Kardjilov N, Manke L (2013) High-resolution neutron and X-ray imaging of
428 granular materials. *Journal of Geotechnical and Geoenvironmental engineering* 139(5):715–723

429 30. Kohgo Y, Nakano M, Miyazaki T (1993) Theoretical aspects of constitutive modelling for partially saturated soils.
430 *Soils and Foundations* 33(4):49–63

431 31. Lai Z, Chen Q (2019) Reconstructing granular particles from X-ray computed tomography using the TWS

- 1
2
3
4 432 machine learning tool and the level set method. *Acta Geotechnica* 14:1–18
5
6 433 32. Manahiloh KN, Meehan CL (2017) Determining the soil water characteristic curve and interfacial contact angle
7
8 434 from microstructural analysis of X-ray CT images. *Journal of Geotechnical and Geoenvironmental Engineering*
9 435 143(8):1–11
10
11 436 33. Mašin D (2010) Predicting the dependency of a degree of saturation on void ratio and suction using effective stress
12 437 principle for partially saturated soils. *International Journal for Numerical and Analytical Methods in*
13 438 *Geomechanics* 34(1):73–90
14
15 439 34. Moro F, Böhni H (2002) Ink-bottle effect in mercury intrusion porosimetry of cement-base materials. *Journal of*
16 440 *Colloid and Interface Science* 246:135–149
17
18 441 35. Mukunoki T, Miyata Y, Mikami K, Shiota E (2016) X-ray CT analysis of pore structure in sand. *Solid Earth*
19 442 7(3):929–942
20
21 443 36. Nguyen CD, Benahmed N, Andò E, Sibille L, Philippe P (2019) Experimental investigation of microstructural
22 444 changes in soils eroded by suffusion using X-ray tomography. *Acta Geotechnica* 14: 749–765
23
24 445 37. Oda M, Takemura T, Takahashi M (2004) Microstructure in shear band observed by microfocus X-ray computed
25 446 tomography. *Géotechnique* 54(8):539–542
26
27 447 38. Prapaharan S, Altschaeffl AG, Dempsey BJ (1985) Moisture curve of a compacted clay: mercury intrusion method.
28 448 *Journal of Geotechnical Engineering* 111(9):1139–1143
29
30 449 39. Romero E, Gens A, Lloret A (1999) Water permeability, water retention and microstructure of unsaturated
31 450 compacted Boom clay. *Engineering Geology* 54(1-2):117–127
32
33 451 40. Romero E, Simms PH (2008) Microstructure investigation in unsaturated soils: a review with special attention to
34 452 contribution of mercury intrusion porosimetry and environmental scanning electron microscopy. *Geotechnical and*
35 453 *Geological Engineering* 26(6):705–727
36
37 454 41. Scheel M, Seemann R, Brinkmann M, Di Michiel M, Sheppard A, Breidenbach B, Herminghaus S (2008)
38 455 Morphological clues to wet granular pile stability. *Nature Materials* 7:189–193
39
40 456 42. Sun D, Sun W, Xiang L (2010) Effect of degree of saturation on mechanical behaviour of unsaturated soils and its
41 457 elastoplastic simulation. *Computers and Geotechnics* 37:678–688
42
43 458 43. Vachaud G, Thony JL (1971) Hysteresis during infiltration and redistribution in a soil column at different initial
44 459 water contents. *Water Resources Research* 7(1):111–127
45
46 460 44. Van Genuchten MT (1980) A closed-form equation for predicting the hydraulic conductivity of partially saturated
47 461 soil. *Soil Science Society of America Journal* 44(5):892–898
48
49 462 45. Vanapalli SK, Nicotera MV, Sharma RS (2008) Axis translation and negative water column techniques for suction
50 463 control. *Geotechnical and Geological Engineering* 26:645–660
51
52 464 46. Wang JP, Lambert P, De Kock T, Cnudde V, François B (2019) Investigation of the effect of specific interfacial
53 465 area on strength of unsaturated granular materials by X-ray tomography. *Acta Geotechnica* 14:1545–1559
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474 Table 1. Physical properties of Toyoura sand

| | |
|---------------------------------------|-------|
| Particle density (g/cm ³) | 2.64 |
| Maximum void ratio | 0.975 |
| Minimum void ratio | 0.614 |
| Average diameter (mm) | 0.185 |
| Uniformity coefficient | 1.6 |
| Fines content (%) | 0.1 |

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476 Table 2. Specimen conditions

| | |
|----------------------------------|---------------------|
| Diameter (mm) | 18.00 |
| Height (mm) | 17.74 |
| Initial void ratio | 0.822 |
| Initial porosity (%) | 45.12 |
| Relative density D_r (%) | 42.38 |
| Initial degree of saturation (%) | 100.00 (Assumption) |

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9 479 Table 3. Specifications of microfocus x-ray CT apparatus

| | | |
|---------------------------|---|-------------------|
| X-ray source | Max. voltage (kV) | 225 |
| | Max. current (mA) | 0.888 |
| | Max. consumption power (W) | 200 |
| | Min. focus size (μm) | 4 |
| Flat panel detector (FPD) | Image matrices | 1024 ² |
| | Resolution performance (μm) | 5 |
| | Integration time (ms) | 66-999 |
| | Projection views | 600-4800 |
| | Number of images averaged at each projection view | 1-50 |

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32 481 Table 4 Validation results for CT images with different resolutions

| Case | Measured value Specimen | Trinarization | |
|----------------------|----------------------------|---------------|-------|
| | | A | B |
| Void ratio | 0.846 | 0.831 | 0.820 |
| Degree of saturation | 0.662 | 0.656 | 0.725 |
| Water content | 0.212 | 0.206 | 0.225 |

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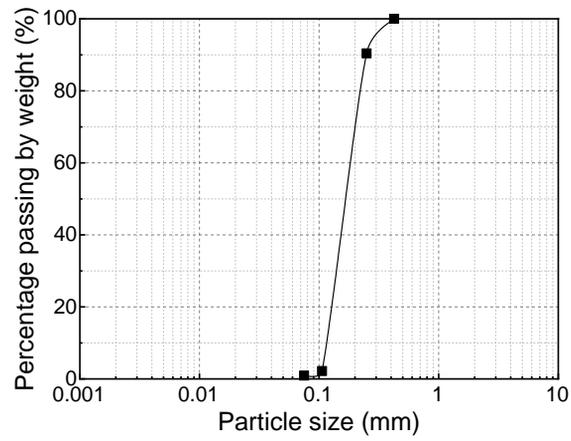


Fig. 1 Grain size distribution curve of Toyoura sand

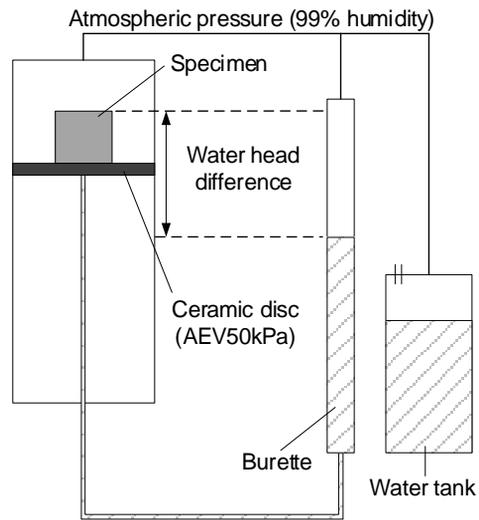


Fig. 2 Schematic illustration of test apparatus and negative water column

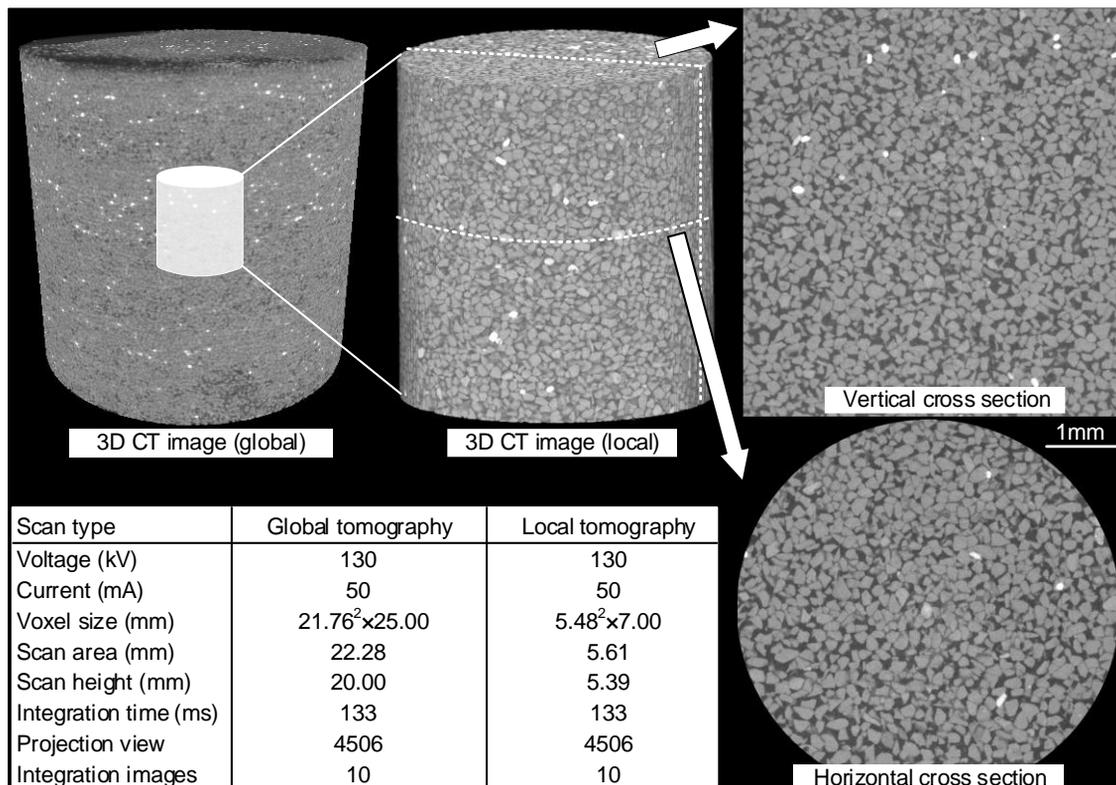


Fig. 3 Scan area and conditions

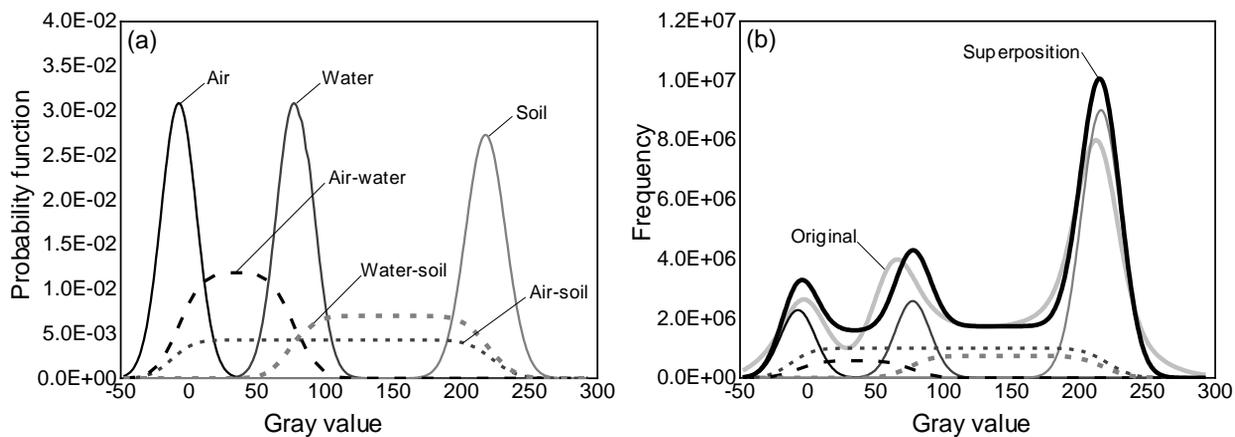


Fig. 4 Gray value distributions obtained by maximum likelihood evaluation: (a) assumption of gray value distributions as normal and uniform distributions and (b) superposition of gray value distributions

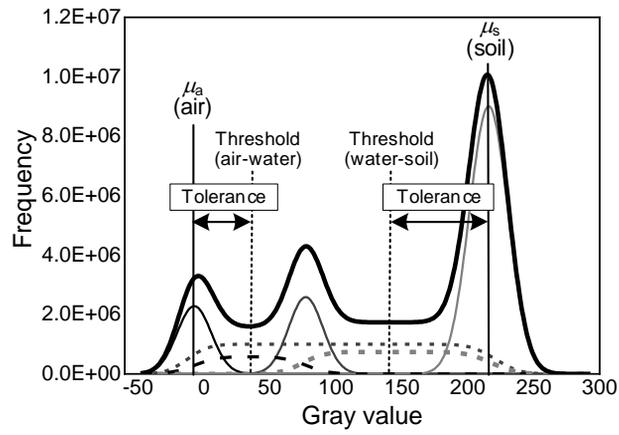
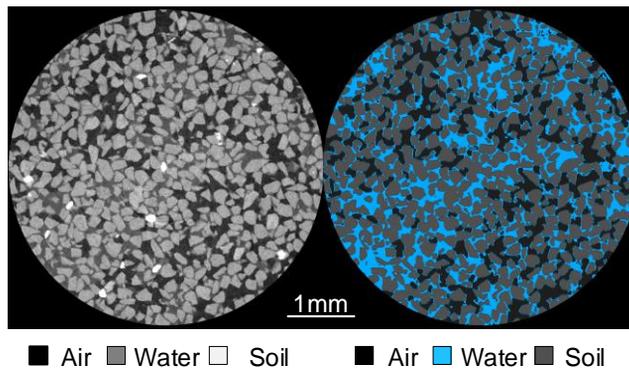


Fig. 5 Conceptual diagram of determination of tolerances for region growing



■ Air ■ Water □ Soil ■ Air ■ Water ■ Soil

Fig. 6 Horizontal cross section of trinarized image

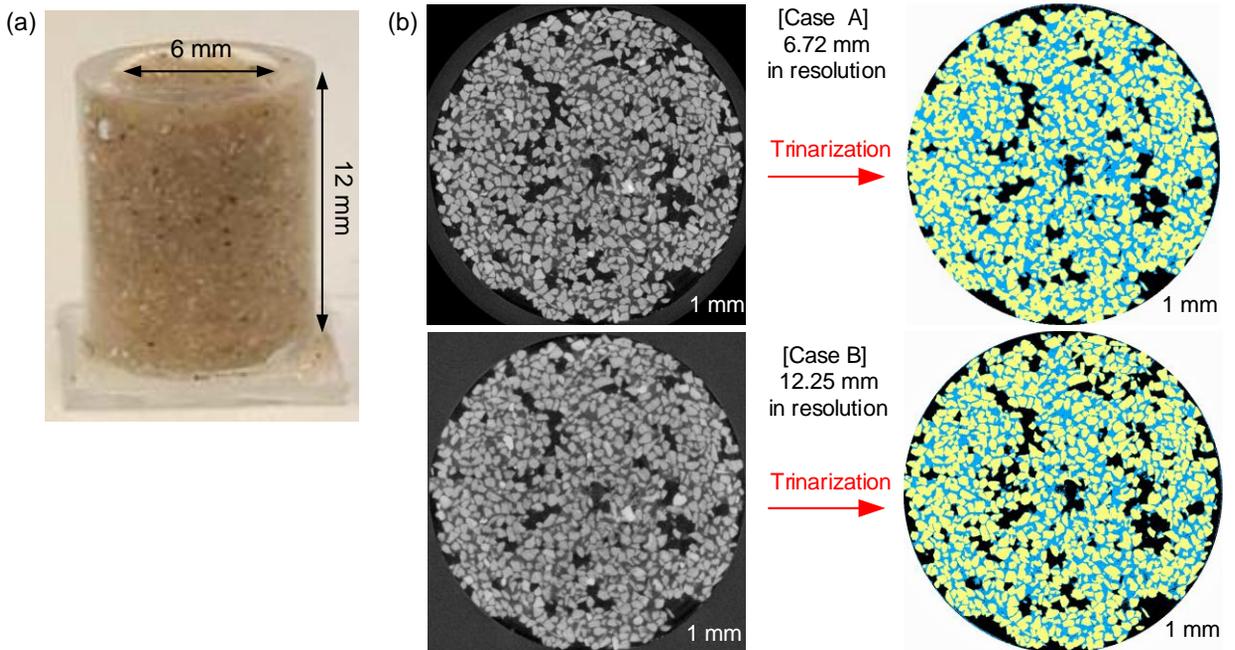


Fig. 7 Validation of trinarization technique: (a) specimen and (b) application of trinarization to CT images

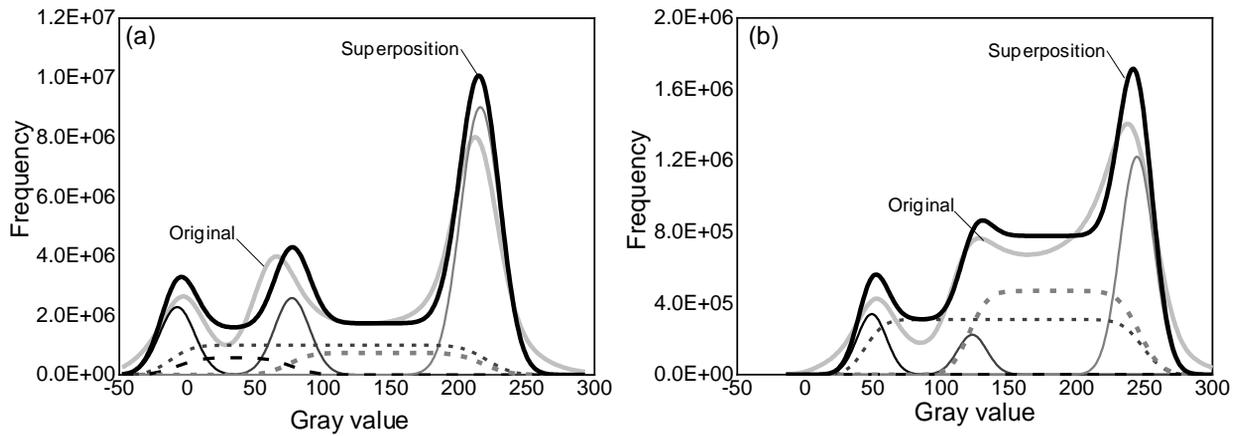


Fig. 8 Gray value histograms for CT images: (a) Case A (6.72 μm in resolution) and (b) Case B (12.25 μm in resolution)

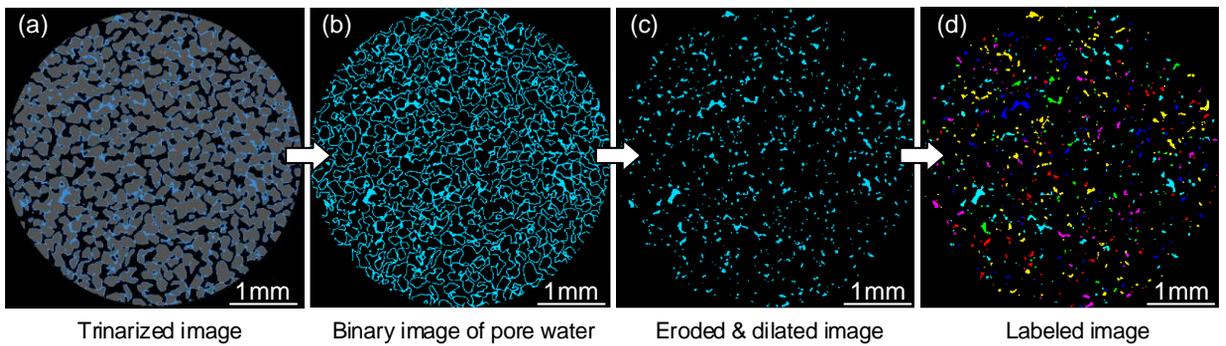


Fig. 9 Procedure for morphology analysis of pore water phase

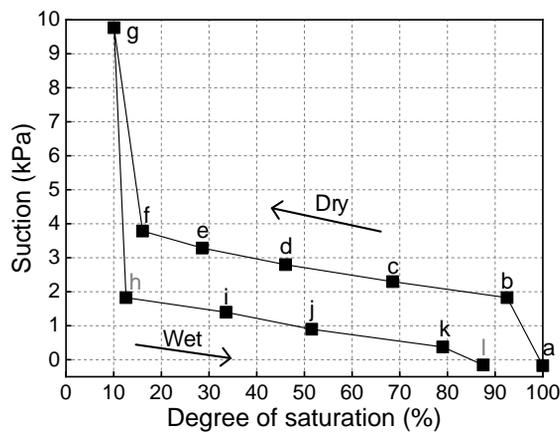


Fig. 10 Water retention curve

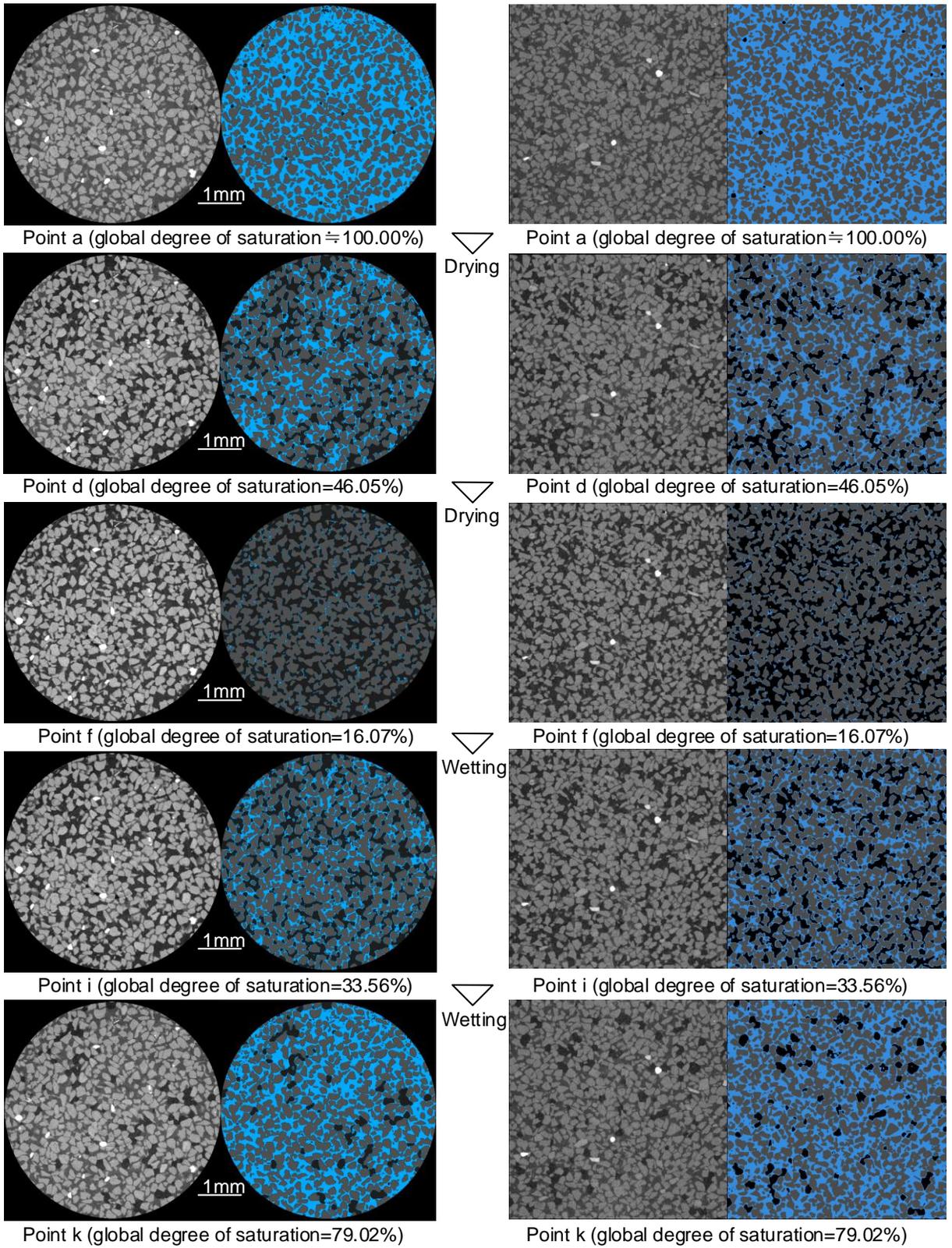


Fig. 11 Horizontal and vertical cross sections of original CT images and trinarized images

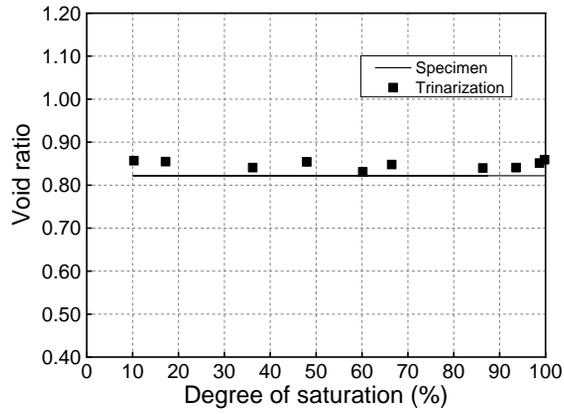


Fig. 12 Local void ratios at different degrees of saturation

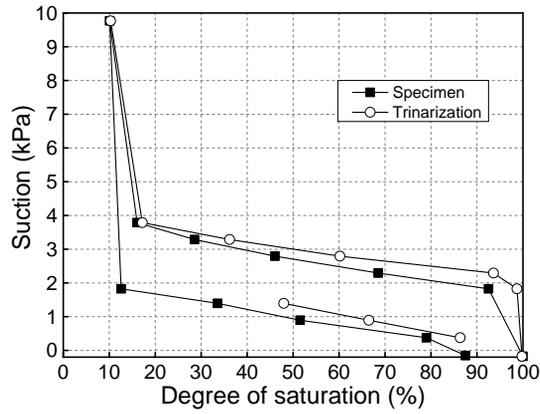


Fig. 13 Comparison of water retention curve with those calculated using trinarization

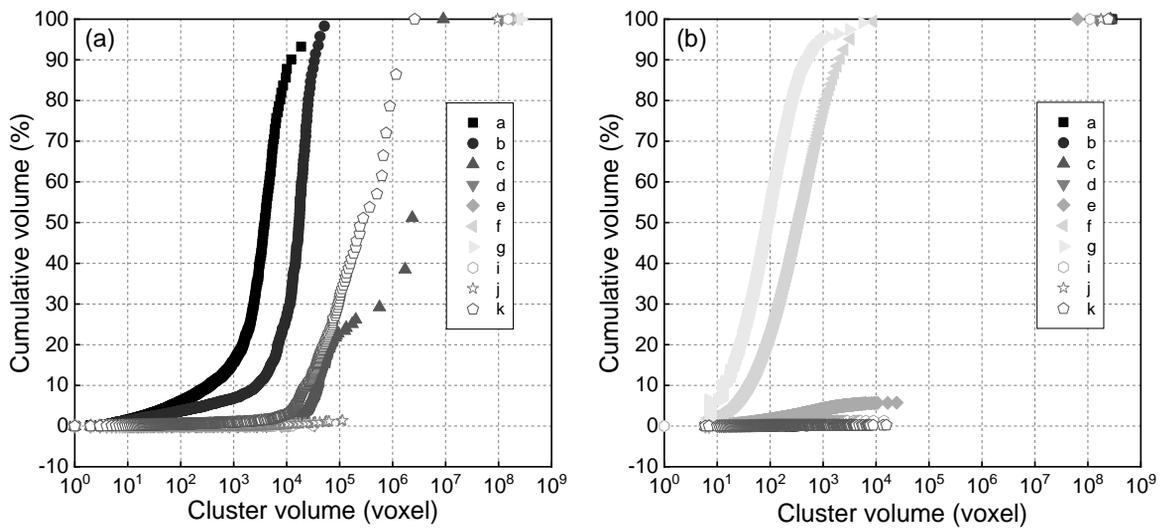


Fig. 14 Cluster volume distribution curves: (a) pore air and (b) pore water

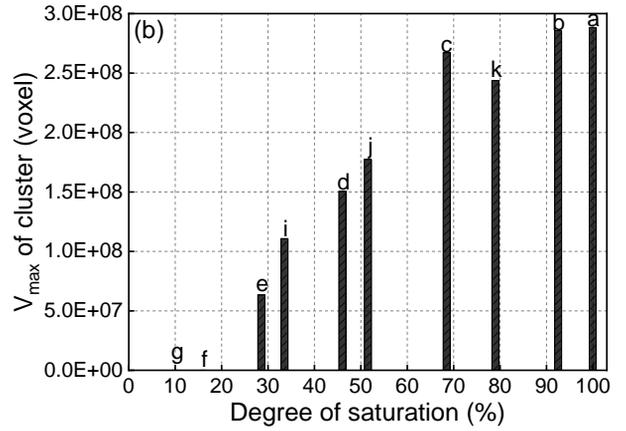
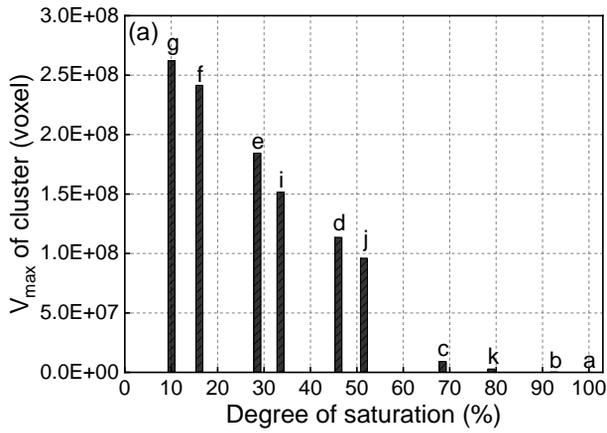


Fig. 15 Maximum volume of clusters at different degrees of saturation: (a) pore air and (b) pore water

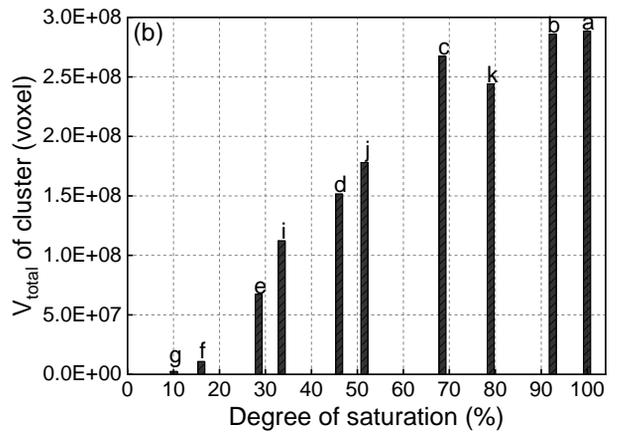
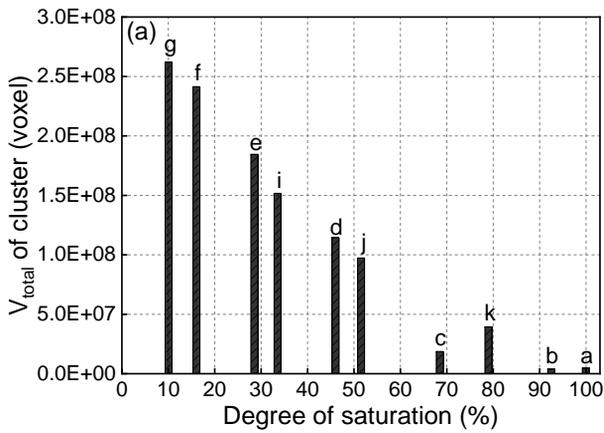


Fig. 16 Total volume of clusters at different degrees of saturation: (a) pore air and (b) pore water

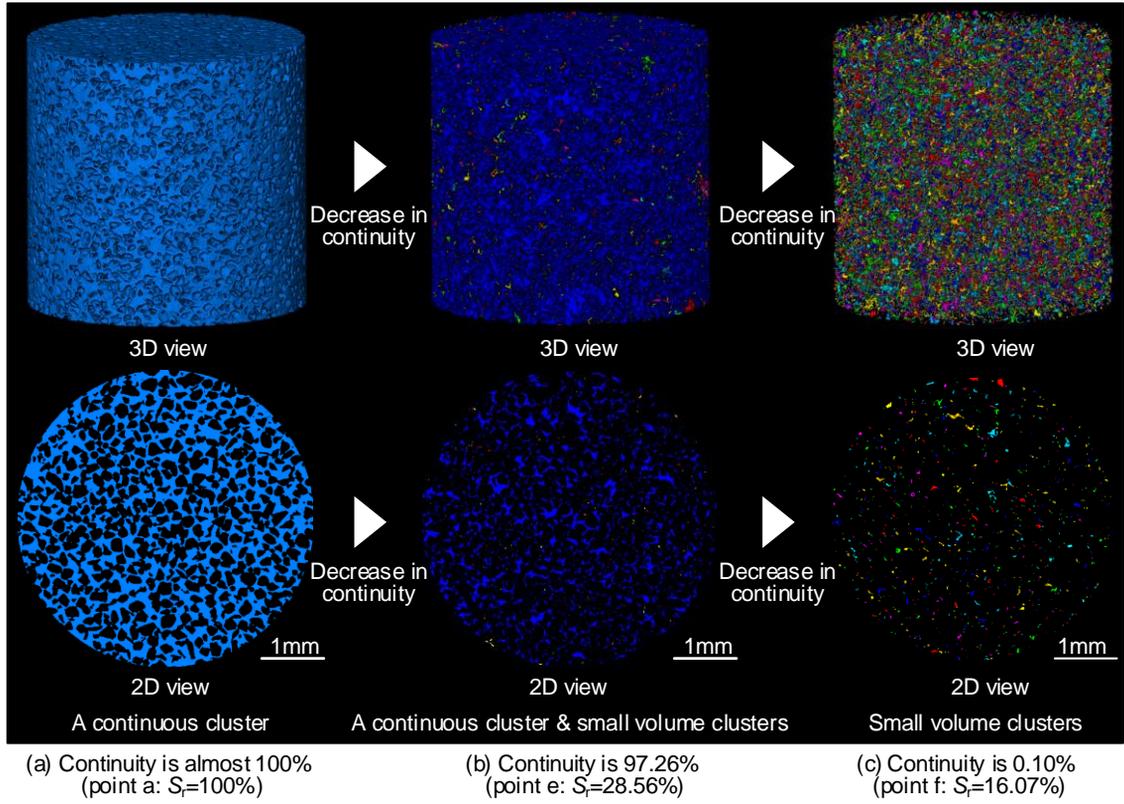


Fig. 17 3D and 2D views of pore water clusters for different levels of continuity

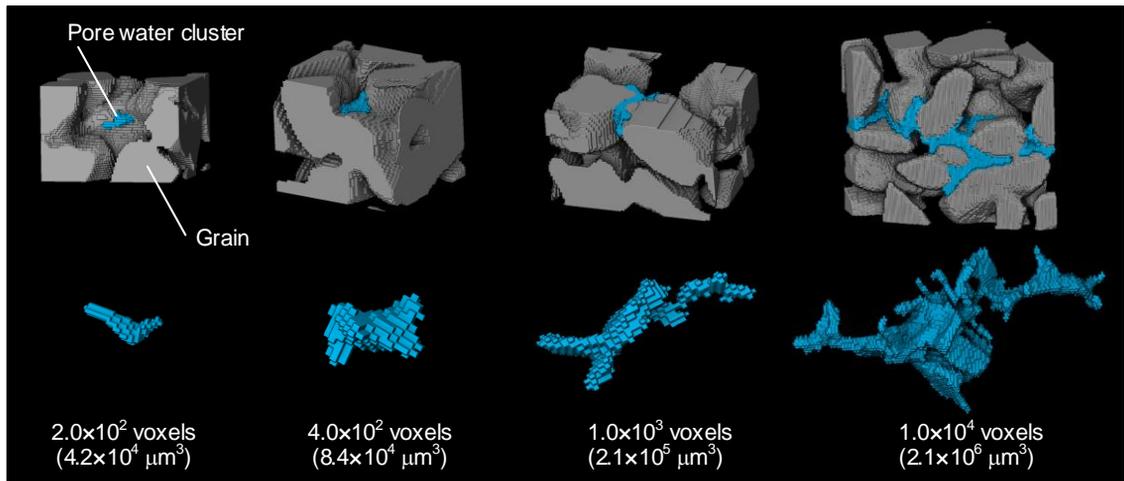


Fig. 18 Pore water clusters with different volumes at grain contacts (point “e”)

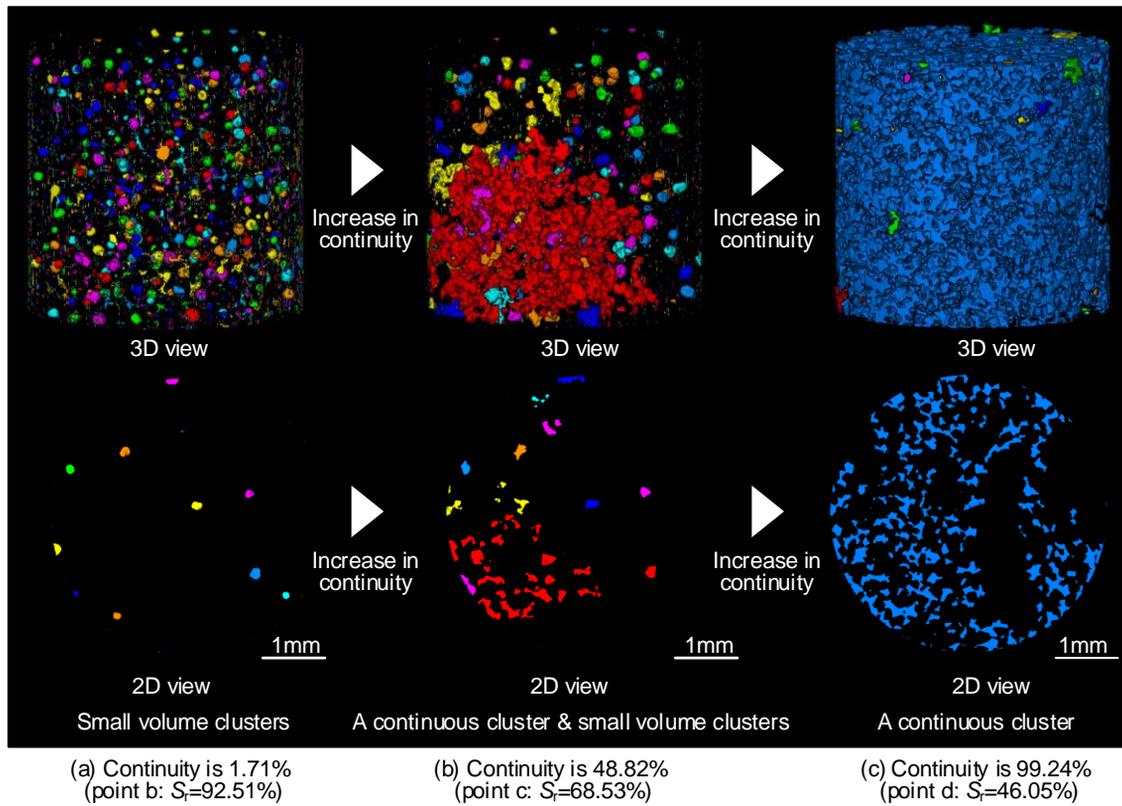


Fig. 19 3D and 2D views of pore air clusters for different levels of continuity

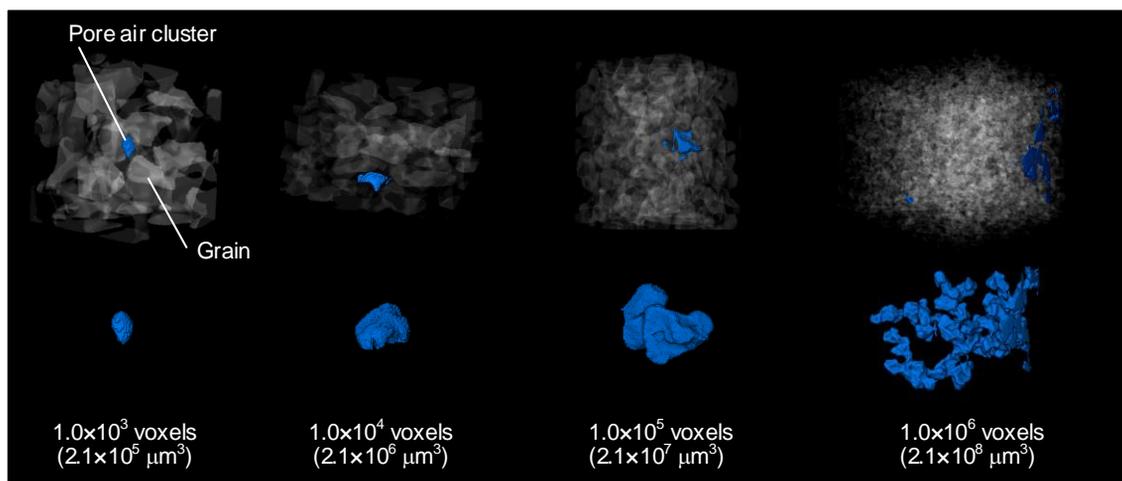


Fig. 20 Pore air clusters with different volumes (point "c")

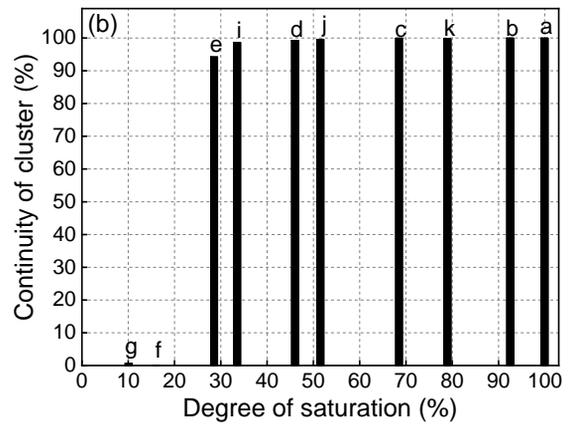
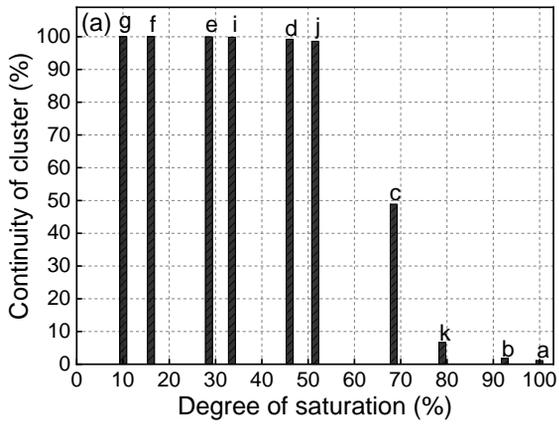


Fig. 21 Continuity of clusters at different degrees of saturation: (a) pore air and (b) pore water

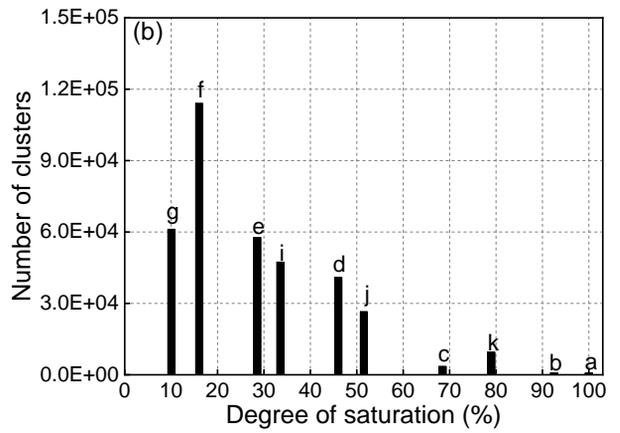
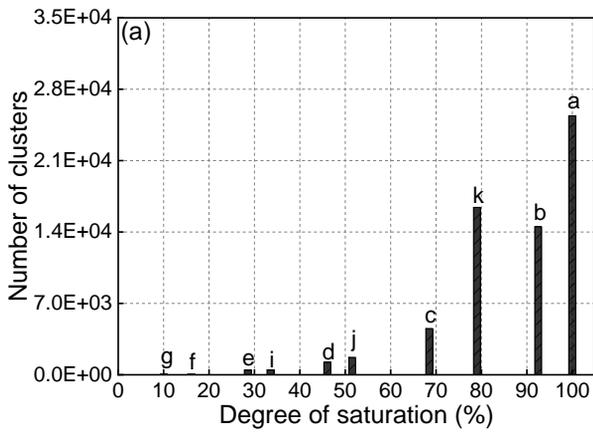


Fig. 22 Number of clusters at different degrees of saturation: (a) pore air and (b) pore water

| Process | Drying | | | | | | | Wetting | | | | | |
|----------------------------|---------------|-------|------------|-------|-------|---------------|-------|---------|------------|-------|---------------|---|---|
| Points | a | b | c | d | e | f | g | h | i | j | k | l | m |
| Global S_r (%) | 100 | 92.51 | 68.53 | 46.05 | 28.56 | 16.07 | 10.08 | | 33.56 | 51.54 | 79.02 | | |
| Continuity (air) | Discontinuous | | Continuous | | | Continuous | | | Continuous | | Discontinuous | | |
| Continuity (water) | Continuous | | Continuous | | | Discontinuous | | | Continuous | | Continuous | | |
| Cluster volume (air) | Small | | Large | | | | | | Large | | | | |
| Cluster volume (water) | Large | | | | Small | | | | Large | | | | |
| Number of clusters (air) | Large | | Small | | | | | | Small | | Large | | |
| Number of clusters (water) | Small | | | Large | | | | | Large | | Small | | |

Note 1: "continuous" means a continuity of nearly 100%, while "discontinuous" means a continuity of nearly 0%.

Note 2: 1.0×10^6 voxels and 1.0×10^4 voxels are thresholds for the air phase and the water phase, respectively, where their morphologies transit from "large cluster volume" to "small cluster volume" and vice versa.

Note 3: Thresholds between "large number of clusters" and "small number of clusters" are 7.0×10^3 (air) and 1.5×10^4 (water), respectively.

Fig. 23 Summary of morphology analysis