

On the Curvature of a Curve in n Dimensional Non-Euclidean Space.

By

Hidetoshi Kashiwagi.

(Received Dec. 13, 1922).

1. The curvature of a curve in n dimensional Non-Euclidean space has already been discussed by many professors—G. Kowalewski,¹ E. Stransky² and T. Nishiuchi³ from different points of view. And also Prof. T. Kubota⁴ has treated the problem following the method given by E. Rath⁵ in Euclidean space. In this paper, I will give the generalization of Prof. Nishiuchi's discussion according to the idea of Meyer⁶ which he applied in the generalization of Serret-Frenet's formula in the Euclidean case.

In n Dimentional Space.

2. Let $x_0, x_1, x_2, \dots, x_n$ be the Weirstrass coordinates of point in n dimensional space whose measure of curvature is $\frac{1}{k^2}$ and

$$(xx) = x_0^2 + x_1^2 + x_2^2 + \dots + x_n^2 = 0$$

be the equation to the absolute.

Suppose

$$x_0 = \varphi_0(t), x_1 = \varphi_1(t), x_2 = \varphi_2(t), \dots, x_n = \varphi_n(t)$$

¹ Wiener Berichte, 120, (1911).

² Wiener Berichte, 121, (1912).

³ Mem. Coll. Sci., Kyoto, 5. No. 3. (1921).

⁴ Kubota, in Sendai, Tohoku Math. J., 21. No. 3, 4. (1922).

^{5,6} Jahresber. D. M. ver., 19, (1910).

represent the coordinates of a point on a curve Γ , where t is a parameter and

$$(\varphi_0(t))^2 + (\varphi_1(t))^2 + (\varphi_2(t))^2 + \dots + (\varphi_n(t))^2 = k^2.$$

Next, we consider any other curve Γ' defined by the equations

$$\alpha_i = \psi_i(t) = x_i \sin \frac{r}{k} + y_i \cos \frac{r}{k}$$

where r is a function of t and

$$(xy) = 0, (aa) = k^2$$

$$i=0, 1, 2, \dots, n.$$

Take a point $P_o[x(t)]$ on the curve Γ and take $r+1$ points $P'_o[a(t)], P'_1[a(t+4t)], P'_2[a(t+24t)], \dots, P'_r[a(t+r4t)]$ on the curve Γ' . Then the coordinates of a point $Q(r\eta)$ which is on the plane manifold passing through $r+1$ points $(P_o, P'_o, P'_1, \dots, P'_{r-1})$ and orthogonal to r points $(P_o, P'_o, P'_1, \dots, P'_{r-2})$ will be

$$(1) \quad r\eta_i = \frac{k \begin{vmatrix} (xx) & (xa) & \dots & (xa^{r-2}) & x_i \\ (ax) & (aa) & \dots & (aa^{r-2}) & a_i \\ \vdots & \vdots & & \vdots & \vdots \\ (a^{r-1}x) & (a^{r-1}a) & \dots & (a^{r-1}a^{r-2}) & a_i^{r-1} \end{vmatrix}}{\sqrt{\begin{vmatrix} (xx) & (xa) & \dots & (xa^{r-2}) \\ (ax) & (aa) & \dots & (aa^{r-2}) \\ \vdots & \vdots & & \vdots \\ (a^{r-2}x) & (a^{r-2}a) & \dots & (a^{r-2}a^{r-2}) \end{vmatrix} \cdot \begin{vmatrix} (xx) & (xa) & \dots & (xa^{r-1}) \\ (ax) & (aa) & \dots & (aa^{r-1}) \\ \vdots & \vdots & & \vdots \\ (a^{r-1}x) & (a^{r-1}a) & \dots & (a^{r-1}a^{r-1}) \end{vmatrix}}},$$

$$(i=0, 1, 2, \dots, n)$$

where

$$\alpha^i = \frac{d^i a}{dt^i}.$$

And it is evident that

$$(r\eta_p\eta) = 0, (r \neq p),$$

$$(r\eta_p\eta) = k^2, (r = p).$$

Next, let $Q(r\dot{\eta})$ be a point on the plane manifold passing through $r+1$ points $(P_o, P'_o, P'_1, \dots, P'_{r-2}, P_r)$ and orthogonal to r points $(P_o, P'_o, P'_1, \dots, P'_{r-2})$, then

$$\begin{aligned}
 {}_r\dot{\eta}_i &= \left[\begin{array}{cccc} (xx) & (xa) & \dots & (xa^{r-2}) \\ (ax) & (aa) & \dots & (aa^{r-2}) \\ \vdots & \vdots & \ddots & \vdots \\ (a^{r-1}x) & (a^{r-1}a) & \dots & (a^{r-1}a^{r-2}) \end{array} \right] {}_{a_i} + \left[\begin{array}{cccc} (xx) & (xa) & \dots & (xa^{r-2}) \\ \vdots & \vdots & \ddots & \vdots \\ (a^{r-2}x) & (a^{r-2}a) & \dots & (a^{r-2}a^{r-2}) \\ (a^rx) & (a^ra) & \dots & (a^ra^{r-2}) \end{array} \right] {}_{a_i^{r-1}} \Delta t \times \\
 (2) \quad &\times \left[\begin{array}{cccc} (xx) & \dots & (xa^{r-2}) \\ (ax) & \dots & (aa^{r-2}) \\ \vdots & \vdots & \ddots \\ (a^{r-2}x) & \dots & (a^{r-2}a^{r-2}) \end{array} \right] \frac{1}{2} \left[\begin{array}{cccc} (xx) & \dots & (xa^{r-1}) \\ (ax) & \dots & (aa^{r-1}) \\ \vdots & \vdots & \ddots \\ (a^{r-1}x) & \dots & (a^{r-1}a^{r-1}) \end{array} \right] \\
 &+ 2 \left[\begin{array}{ccc} (xx) & \dots & (xa^{r-2}) & (xa^r) \\ \vdots & \vdots & \ddots & \vdots \\ (a^{r-2}x) & \dots & (a^{r-2}a^{r-2}) & (a^{r-2}a^r) \\ (a^{r-1}x) & \dots & (a^{r-1}a^{r-2}) & (a^{r-1}a^r) \end{array} \right] \Delta t + \left[\begin{array}{ccc} (xx) & \dots & (xa^{r-2}) & (xa^r) \\ \vdots & \vdots & \ddots & \vdots \\ (a^{r-2}x) & \dots & (a^{r-2}a^{r-2}) & (a^{r-2}a^r) \\ (a^rx) & \dots & (a^ra^{r-2}) & (a^ra^r) \end{array} \right] \frac{1}{2\Delta t^2}.
 \end{aligned}$$

The limiting value of $\frac{\overline{rQ_rQ}}{\text{arc } P_0 P_1} \times \frac{1}{k}$ when $P_1[x(t + \Delta t)]$ approaches to P_0 shall be called the r th curvature of the curve Γ at the point P_0 with respect to the curve Γ' , in analogy to Prof. Nishiuchi's definition.¹

But

$$\begin{aligned}
 \sin^2 \frac{\overline{rQ_rQ}}{k} &= \frac{\left\| \begin{array}{c} {}_r\eta_0 \ {}_r\eta_1 \ \dots \ {}_r\eta_n \\ {}_r\dot{\eta}_0 \ {}_r\dot{\eta}_1 \ \dots \ {}_r\dot{\eta}_n \end{array} \right\|^2}{k^4} \\
 (3) \quad &= \frac{\left\| \begin{array}{cc} (xx) & \dots & (xa^{r-2}) & (xa^{r-1}) \\ \vdots & \vdots & \ddots & \vdots \\ (a^{r-2}x) & \dots & (a^{r-2}a^{r-2}) & (a^{r-2}a^{r-1}) \\ (a^{r-1}x) & \dots & (a^{r-1}a^{r-2}) & (a^{r-1}a^{r-1}) \end{array} \right\|^2}{\Delta t^2} \frac{\left\| \begin{array}{cc} (xx) & \dots & (xa^{r-2}) & (xa^r) \\ \vdots & \vdots & \ddots & \vdots \\ (a^{r-2}x) & \dots & (a^{r-2}a^{r-2}) & (a^{r-2}a^r) \\ (a^{r-1}x) & \dots & (a^{r-1}a^{r-2}) & (a^{r-1}a^r) \end{array} \right\|^2} \\
 &\quad - \frac{\left\| \begin{array}{cc} (xx) & \dots & (xa^{r-2}) & (xa^r) \\ \vdots & \vdots & \ddots & \vdots \\ (a^{r-2}x) & \dots & (a^{r-2}a^{r-2}) & (a^{r-2}a^r) \\ (a^{r-1}x) & \dots & (a^{r-1}a^{r-2}) & (a^{r-1}a^r) \end{array} \right\|^2}{\Delta t^2} + \theta \overline{\Delta t^2}
 \end{aligned}$$

¹ Loc. cit.

where

$$\lim_{\Delta t \rightarrow 0} \theta = 0.$$

Applying the Sylvester theorem, we have

$$(4) \quad \sin^2 \frac{\overline{rQ_rQ}}{k} = \frac{\Delta_{r-1} \Delta_{r+1}}{\Delta_r^2} \Delta t^3 + \theta \Delta t^2$$

where

$$(5) \quad \Delta_i = \begin{vmatrix} (xx) & (xa) & \dots & (xa^{i-1}) \\ \vdots & \vdots & & \vdots \\ (a^{i-1}x) & (a^{i-1}a) & \dots & (a^{i-1}a^{i-1}) \end{vmatrix} = \begin{vmatrix} x_0 & x_1 & \dots & x_n \\ a_0 & a_1 & \dots & a_n \\ a'_0 & a'_1 & \dots & a'_n \\ \dots & \dots & & \dots \\ a_n^{i-1} & a_1^{i-1} & \dots & a_n^{i-1} \end{vmatrix}^2$$

On the other hand

$$\begin{aligned} \sin \frac{\overline{P_oP_1}}{k} &= \sqrt{\frac{\begin{vmatrix} (xx) & (xx') \\ (x'x) & (x'x') \end{vmatrix}}{(xx)^2}} \Delta t + W \Delta t \\ &= \frac{\sqrt{\Delta}}{k^2} \Delta t + W \Delta t \end{aligned}$$

where

$$\lim_{\Delta t \rightarrow 0} W = 0.$$

So the r^{th} curvature $\frac{I}{R_r}$ of the curve I' at the point P_o with respect to the curve I' will be

$$\begin{aligned} \frac{I}{R_r} &= \lim_{\Delta t \rightarrow 0} \frac{\overline{Q_rQ}}{k \arcsin \frac{\overline{P_oP_1}}{k}} = \lim_{\Delta t \rightarrow 0} \frac{k \sin \frac{\overline{rQ_rQ}}{k}}{k \sin \frac{\overline{P_oP_1}}{k}} \times \frac{I}{k} \\ (6) \quad &= k \frac{\sqrt{\frac{\Delta_{r-1} \Delta_{r+1}}{\sqrt{\Delta} \Delta_r}}}{\sqrt{\Delta} \Delta_r} \\ &\quad (r = 1, 2, \dots, n) \end{aligned}$$

$$\frac{I}{R_o} = \frac{I}{k}.$$

Also, if θ be the angle between two plane manifolds whose absolute poles are Q and Q' respectively, then we have

$$\frac{I}{R_r} = \lim_{\Delta t \rightarrow 0} \frac{r\theta}{\text{arc } P_0 P_1}.$$

From this equation we can also define $\frac{I}{R_r}$, but I think the former definition is natural.

3. Differentiating η_i with respect to t , we have

$$\begin{aligned} \frac{d_r \eta_i}{dt} &= \frac{k}{\Delta_{r-1}^{\frac{3}{2}} \Delta_r^{\frac{3}{2}}} \left[\Delta_{r-1} \left\{ \begin{vmatrix} (xx) & \dots & (xa^{r-1}) & x_i \\ \vdots & \ddots & \vdots & \vdots \\ (a^{r-2}x) & \dots & (a^{r-2}a^{r-1}) & \\ \vdots & \ddots & \vdots & \vdots \\ (a^{r-1}x) & \dots & (a^{r-1}a^{r-1}) & \\ \end{vmatrix} \cdot \begin{vmatrix} (xx) & \dots & (xa^{r-2}) & x_i \\ \vdots & \ddots & \vdots & \vdots \\ (a^{r-2}x) & \dots & (a^{r-2}a^{r-2}) & a_i^{r-2} \\ \vdots & \ddots & \vdots & \vdots \\ (a^r x) & \dots & (a^r a^{r-2}) & a_i^r \\ \end{vmatrix} \right. \right. \\ &\quad - \begin{vmatrix} (xx) & \dots & (xa^{r-2}) & x_i \\ \vdots & \ddots & \vdots & \vdots \\ (a^{r-2}x) & \dots & (a^{r-2}a^{r-2}) & a_i^{r-2} \\ \vdots & \ddots & \vdots & \vdots \\ (a^{r-1}x) & \dots & (a^{r-1}a^{r-2}) & a_i^{r-1} \\ \end{vmatrix} \cdot \begin{vmatrix} (xx) & \dots & (xa^{r-2}) & (xa^r) \\ \vdots & \ddots & \vdots & \vdots \\ (a^{r-2}x) & \dots & (a^{r-2}a^{r-2}) & (a^{r-2}a^r) \\ \vdots & \ddots & \vdots & \vdots \\ (a^{r-1}x) & \dots & (a^{r-1}a^{r-2}) & (a^{r-1}a^r) \\ \end{vmatrix} \left. \right\} \\ &\quad - \Delta_r \left\{ \begin{vmatrix} (xx) & \dots & (xa^{r-2}) & x_i \\ \vdots & \ddots & \vdots & \vdots \\ (a^{r-2}x) & \dots & (a^{r-2}a^{r-2}) & a_i^{r-2} \\ \vdots & \ddots & \vdots & \vdots \\ (a^{r-1}x) & \dots & (a^{r-1}a^{r-2}) & a_i^{r-1} \\ \end{vmatrix} \cdot \begin{vmatrix} (xx) & \dots & (xa^{r-3}) & (xa^{r-1}) \\ \vdots & \ddots & \vdots & \vdots \\ (a^{r-3}x) & \dots & (a^{r-3}a^{r-3}) & (a^{r-3}a^{r-1}) \\ \vdots & \ddots & \vdots & \vdots \\ (a^{r-2}x) & \dots & (a^{r-2}a^{r-3}) & (a^{r-2}a^{r-1}) \\ \end{vmatrix} \right. \\ &\quad - \begin{vmatrix} (xx) & \dots & (xa^{r-2}) \\ \vdots & \ddots & \vdots \\ (a^{r-3}x) & \dots & (a^{r-3}a^{r-2}) \\ \vdots & \ddots & \vdots \\ (a^{r-2}x) & \dots & (a^{r-2}a^{r-2}) \\ \end{vmatrix} \cdot \begin{vmatrix} (xx) & \dots & (xa^{r-3}) & (xa^{r-1}) & x_i \\ \vdots & \ddots & \vdots & \vdots & \vdots \\ (a^{r-2}x) & \dots & (a^{r-2}a^{r-3}) & (a^{r-2}a^{r-1}) & a_i^{r-2} \\ \vdots & \ddots & \vdots & \vdots & \vdots \\ (a^{r-1}x) & \dots & (a^{r-1}a^{r-3}) & (a^{r-1}a^{r-1}) & a_i^{r-1} \\ \end{vmatrix} \left. \right\} \\ &\quad + \Delta_r \left\{ \begin{vmatrix} (x'x) & (x'a) & \dots & (x'a^{r-2}) & x'_i \\ (ax) & (aa) & \dots & (aa^{r-2}) & a_i \\ \vdots & \ddots & \ddots & \ddots & \vdots \\ (a^{r-1}x) & (a^{r-1}a) & \dots & (a^{r-1}a^{r-2}) & a_i^{r-1} \\ \end{vmatrix} \cdot \begin{vmatrix} (xx) & \dots & (xa^{r-2}) \\ \vdots & \ddots & \vdots \\ (a^{r-2}x) & \dots & (a^{r-2}a^{r-2}) \\ \end{vmatrix} \right. \\ &\quad - \begin{vmatrix} (xx) & \dots & (xa^{r-2}) & x_i \\ \vdots & \ddots & \vdots & \vdots \\ (a^{r-1}x) & \dots & (a^{r-1}a^{r-2}) & a_i^{r-1} \\ \end{vmatrix} \cdot \begin{vmatrix} (xx') & (xa) & \dots & (xa^{r-2}) \\ \vdots & \ddots & \ddots & \vdots \\ (a^{r-2}x') & (a^{r-2}a) & \dots & (a^{r-2}a^{r-2}) \\ \end{vmatrix} \left. \right\} \end{aligned}$$

$$\begin{aligned}
& -\Delta_{r-1} \left\{ \begin{vmatrix} (xx) & \dots & (xa^{r-2}) & x_i \\ \vdots & & \vdots & \vdots \\ (a^{r-1}x) \dots (a^{r-1}a^{r-2}) & a_i^{r-1} & & \end{vmatrix} \cdot \begin{vmatrix} (xx') & (xa) & \dots & (xa^{r-1}) \\ \vdots & \vdots & & \vdots \\ (a^{r-1}x') & (a^{r-1}a) \dots (a^{r-1}a^{r-2}) & a_i^{r-1} & \end{vmatrix} \right. \\
& \left. - \begin{vmatrix} (xx') & (xa) & \dots & (xa^{r-2}) & x_i \\ \vdots & \vdots & & \vdots & \vdots \\ (a^{r-1}x') & (a^{r-1}a) \dots (a^{r-1}a^{r-2}) & a_i^{r-1} & & \end{vmatrix} \cdot \begin{vmatrix} (xx) & \dots & (xa^{r-1}) \\ \vdots & & \vdots \\ (a^{r-1}x) \dots (a^{r-1}a^{r-1}) & & \end{vmatrix} \right\}.
\end{aligned}$$

By the Sylvester theorem, we have

$$\begin{aligned}
& \frac{d_r \eta_i}{dt} = \frac{k}{\Delta_{r-1}^{\frac{3}{2}} \Delta_r^{\frac{3}{2}}} [(\Delta_{r-1}^2 N_{r+1} - \Delta_r^2 N_{r-1})] \\
& + \Delta_r \begin{vmatrix} (ax) & (aa) & \dots & (aa^{r-2}) \\ (a'x) & (a'a) & \dots & (a'a^{r-2}) \\ \vdots & \vdots & & \vdots \\ (a^{r-1}x)(a^{r-1}a) \dots (a^{r-1}a^{r-2}) & & & \end{vmatrix} \cdot \begin{vmatrix} (x'x) & (x'a) & \dots & (x'a^{r-2}) & x'_i \\ (xx) & (xa) & \dots & (xa^{r-2}) & x_i \\ (ax) & (aa) & \dots & (aa^{r-2}) & a_i \\ \vdots & \vdots & & \vdots & \vdots \\ (a^{r-2}x) & (a^{r-2}a) \dots (a^{r-2}a^{r-2}) & a^{r-2} & & \end{vmatrix} \\
& - \Delta_{r-1} \begin{vmatrix} (xx') & (xx) & (xa) & \dots & (xa^{r-2}) \\ (ax') & (ax) & (aa) & \dots & (aa^{r-2}) \\ \vdots & \vdots & \vdots & & \vdots \\ (a^{r-1}x') & (a^{r-1}x) & (a^{r-1}a) \dots (a^{r-1}a^{r-2}) & & \end{vmatrix} \cdot \begin{vmatrix} (xa) & (xa') & \dots & (xa^{r-1}) & x_i \\ (aa) & (aa') & \dots & (aa^{r-1}) & a_i \\ \vdots & \vdots & & \vdots & \vdots \\ (a^{r-1}a)(a^{r-1}a') \dots (a^{r-1}a^{r-1}) & a_i^{r-1} & & & \end{vmatrix} \\
(7) \quad & - \Delta_{r-1} \begin{vmatrix} (xx') & (xx) & (xa) & \dots & (xa^{r-2}) \\ (ax') & (ax) & (aa) & \dots & (aa^{r-2}) \\ \vdots & \vdots & \vdots & & \vdots \\ (a^{r-1}x') & (a^{r-1}x) & (a^{r-1}a) \dots (a^{r-1}a^{r-2}) & & \end{vmatrix} \cdot \begin{vmatrix} (xa) & (xa') & \dots & (xa^{r-1}) & x_i \\ (aa) & (aa') & \dots & (aa^{r-1}) & a_i \\ \vdots & \vdots & & \vdots & \vdots \\ (a^{r-1}a)(a^{r-1}a') \dots (a^{r-1}a^{r-1}) & a_i^{r-1} & & & \end{vmatrix}
\end{aligned}$$

where

$$N_r = \begin{vmatrix} (xx) & (xa) & \dots & (xa^{r-2}) & x_i \\ (ax) & (aa) & \dots & (aa^{r-2}) & a_i \\ \vdots & \vdots & & \vdots & \vdots \\ (a^{r-1}x) & (a^{r-1}a) \dots (a^{r-1}a^{r-2}) & a_i^{r-1} & & \end{vmatrix}$$

and

$$i=0, 1, 2, \dots, n$$

$$r=2, 3, \dots, n.$$

Hence, we have

$$\frac{d_r \eta_i}{ds} = \frac{r+1 \eta_i}{R_r} - \frac{r-1 \eta_i}{R_{r-1}} + \frac{r \xi_i}{P_r} - \frac{r \zeta_i}{Q_r},$$

($r=2, 3, \dots, n$) ($i=0, 1, 2, \dots, n$).

$$(8) \quad \frac{d_o\eta_i}{ds} = \frac{o\xi_i}{P_o}, \quad \frac{d_1\eta_i}{ds} = \frac{1\eta_i}{R_1} + \frac{1\xi_i}{P_1} - \frac{\zeta_i}{Q_1},$$

$$\frac{d_{n+1}\eta_i}{ds} = -\frac{n\eta_i}{R_n} + \frac{n+1\xi_i}{P_{n+1}} - \frac{n+1\zeta_i}{Q_{n+1}}$$

($i=0, 1, 2, \dots, n$)

These are the generalized Serret-Frenet formula, where

$$r\xi_i = \frac{k \begin{vmatrix} (x'x) & (x'a) & \dots & (x'a^{r-2}) & x'_i \\ (xx) & (xa) & \dots & (xa^{r-2}) & x_i \\ (ax) & (aa) & \dots & (aa^{r-2}) & a_i \\ \vdots & \vdots & & \vdots & \vdots \\ (a^{r-2}x) & (a^{r-2}a) & \dots & (a^{r-2}a^{r-2}) & a_i^{r-2} \end{vmatrix}}{\sqrt{\begin{vmatrix} (xx) & (xa) & \dots & (xa^{r-2}) & (x'a') & (x'x) & (x'a) & \dots & (x'a^{r-2}) \\ (ax) & (aa) & \dots & (aa^{r-2}) & (xx') & (xx) & (xa) & \dots & (xa^{r-2}) \\ \vdots & \vdots & & \vdots & (ax') & (ax) & (aa) & \dots & (aa^{r-2}) \\ (a^{r-2}x) & (a^{r-2}a) & \dots & (a^{r-2}a^{r-2}) & (a^{r-2}x') & (a^{r-2}x) & (a^{r-2}a) & \dots & (a^{r-2}a^{r-2}) \end{vmatrix}}},$$

$$(9) \quad r\zeta_i = \frac{k \begin{vmatrix} (xa) & (xa') & \dots & (xa^{r-1}) & x_i \\ (aa) & (aa') & \dots & (aa^{r-1}) & a_i \\ \vdots & \vdots & & \vdots & \vdots \\ (a^{r-1}a) & (a^{r-1}a') & \dots & (a^{r-1}a^{r-1}) & a_i^{r-1} \end{vmatrix}}{\sqrt{\begin{vmatrix} (aa) & \dots & (aa^{r-1}) & (xx) & (xa) & \dots & (xa^{r-1}) \\ \vdots & & \vdots & (ax) & (aa) & \dots & (aa^{r-1}) \\ (a^{r-1}a) & \dots & (a^{r-1}a^{r-1}) & (a^{r-1}x) & (a^{r-1}a) & \dots & (a^{r-1}a^{r-1}) \end{vmatrix}}},$$

$$\frac{1}{P_r} = \frac{k}{\Delta} \frac{\sqrt{\begin{vmatrix} (x'x') & (x'x) & (x'a) & \dots & (x'a^{r-2}) & (ax) & (aa) & \dots & (aa^{r-2}) \\ (xx') & (xx) & (xa) & \dots & (xa^{r-2}) & (a'x) & (a'a) & \dots & (a'a^{r-2}) \\ (ax') & (ax) & (aa) & \dots & (aa^{r-2}) & \vdots & \vdots & & \vdots \\ (a^{r-2}x') & (a^{r-2}x) & (a^{r-2}a) & \dots & (a^{r-2}a^{r-2}) & (a^{r-1}x) & (a^{r-1}a) & \dots & (a^{r-1}a^{r-2}) \end{vmatrix}}}{\sqrt{\Delta_r} \Delta_{r-1}}$$

$$\frac{I}{Q_r} = \frac{k}{\Delta} \frac{\sqrt{\left| \begin{array}{ccc|cc} (aa) & \dots & (aa^{r-1}) & (xx') & (xx) \\ \vdots & & \vdots & (ax') & (xa) \\ (aa^{r-1}) & \dots & (a^{r-1}a^{r-1}) & (ax) & \dots \\ \vdots & & \vdots & (aa) & \dots \\ (a^{r-1}x') & (a^{r-1}x) & (a^{r-1}a) & \dots & (a^{r-1}a^{r-2}) \end{array} \right|}}{\sqrt{\Delta_{r-1}}} \frac{\Delta_r}{\Delta}.$$

It is easily seen that $(r\xi)$ will be the coordinates of a point rX which is on the plane manifold passing through $r+1$ points $(P_0, P_1, P'_0, P'_1, \dots, P'_{r-2})$ and orthogonal to r points $(P_0, P'_0, P'_1, \dots, P'_{r-2})$. And $(r\zeta)$ be that of a point rZ which is on the plane manifold passing through $r+1$ points $(P_0, P'_0, P'_1, \dots, P'_{r-1})$ and orthogonal to r points $(P'_0, P'_1, \dots, P'_{r-1})$.

Next, let Δr be the difference of the distance between the points $P_o[x(t)], rQ[r\eta(t+\Delta t)]$ and $P_o[x(t)], rQ[r\eta(t)]$, then

$$\frac{I}{Q_r} = \frac{\frac{I}{P_o, Z}}{\cos \frac{k}{k}} \left[\lim_{\Delta t \rightarrow 0} \frac{\Delta r}{\text{arc } P_o P_1} \right],$$

$$\frac{I}{P_r} = \frac{\cos \frac{rQ_r Z}{k}}{\cos \frac{rQ_r X}{k}} \frac{I}{Q_r}.$$

We shall call $\frac{I}{P_r} \left(\frac{I}{Q_r} \right)$ the r^{th} left (right) curvature of the curve Γ at the point $P_o(x)$ with respect to the curve Γ' .

4. Specially, if Γ' be a curve traced by a point on the tangent to the curve Γ at the point P_o , then we have

$$a_i = x_i \sin \frac{r}{k} + \rho k x_i' \cos \frac{r}{k},$$

where

$$\rho = \frac{dt}{ds},$$

$$(i=0, 1, 2, 3, \dots, n).$$

And we have

$$(10) \quad r\eta_i = \frac{k}{\sqrt{\left| \begin{array}{c} (xx) \dots (xx^{r-1}) \\ \vdots \\ (x^rx) \dots (x^rx^{r-1}) \end{array} \right| \left| \begin{array}{c} (xx) \dots (xx^r) \\ \vdots \\ (x^rx) \dots (x^rx^r) \end{array} \right|}},$$

$$(11) \quad \frac{I}{R_r^2} = k^2 \frac{\Delta_{r-1} \Delta_{r+1}}{\Delta_r^2 \Delta_1},$$

where

$$\Delta_i = \left| \begin{array}{c} (xx) \dots (xx^i) \\ \vdots \\ (x^ix) \dots (x^ix^i) \end{array} \right|.$$

And the Serret-Frenet formula will be

$$(12) \quad \begin{aligned} \frac{d_r \eta_i}{ds} &= \frac{r+1 \eta_i}{R_r} - \frac{r-1 \eta_i}{R_{r-1}}, \quad (r=1, 2, 3, \dots, n-1) \\ \frac{d_0 \eta_i}{ds} &= \frac{1 \eta_i}{k}, \quad \frac{d_n \eta_i}{ds} = -\frac{n-1 \eta_i}{R_{n-1}}, \\ (i &= 0, 1, 2, \dots, n). \end{aligned}$$

There are the formula given by Prof. Nishiuchi.¹

In Euclidean Space.

5. If we put

$$x_0 = k\dot{x}_0, \quad x_1 = \dot{x}_1, \quad x_2 = \dot{x}_2, \quad \dots, \quad x_n = \dot{x}_n,$$

$$y_0 = k\dot{y}_0, \quad y_1 = \dot{y}_1, \quad y_2 = \dot{y}_2, \quad \dots, \quad y_n = \dot{y}_n$$

and

$$\frac{\dot{x}_i}{\dot{x}_0} = \alpha_i,$$

$$\frac{\dot{y}_i}{\dot{y}_0} = \beta_i, \quad (i=1, 2, \dots, n)$$

¹ loc. cit.

and take the limiting value when $\frac{I}{k^2}$ tends to zero, we have

$$(13) \quad \frac{I}{R_r^2} = \frac{D_{r-1} D_{r+1}}{\Delta D_r^2},$$

where

$$D_i = \begin{vmatrix} y_1 - x_1 & y_2 - x_2 & \dots & y_n - x_n \\ \bar{a}_1' & \bar{a}_2' & \dots & \bar{a}_n' \\ \dots & \dots & \dots & \dots \\ \bar{a}_1^{i-1} & \bar{a}_2^{i-1} & \dots & \bar{a}_n^{i-1} \end{vmatrix}^2$$

$$a_i = x_i + r(y_i - x_i)$$

$$\Delta = (x' x').$$

6. If we consider the case when r tends to infinity in the formula above, then

$$(14) \quad \frac{I}{R_r^2} = \frac{D_{r-1} D_{r+1}}{\Delta D_r^2}$$

where

$$(14_1) \quad D_i = \begin{vmatrix} a_1 & a_2 & \dots & a_n \\ a_1' & a_2' & \dots & a_n' \\ \dots & \dots & \dots & \dots \\ a_1^{i-1} & a_2^{i-1} & \dots & a_n^{i-1} \end{vmatrix}^2$$

$$a_i = y_i - x_i.$$

And if we take

$$\lim_{k \rightarrow \infty} \frac{k_r \eta_i}{r \eta_0} = {}_r a_i,$$

$$({}_r a_r a) = I,$$

then we have

$$(15) \quad {}_r\alpha_i = \frac{\begin{vmatrix} (aa) & (aa') & \dots & (aa^{r-2}) & a_i \\ \vdots & \vdots & & \vdots & \vdots \\ (a^{r-1}a) & (a^{r-1}a') & \dots & (a^{r-1}a^{r-2}) & a_i^{r-1} \end{vmatrix}}{\sqrt{\begin{vmatrix} (aa) & \dots & (aa^{r-2}) \\ \vdots & & \vdots \\ (a^{r-2}a) & \dots & (a^{r-2}a^{r-2}) \end{vmatrix} \cdot \begin{vmatrix} (aa) & \dots & (aa^{r-1}) \\ \vdots & & \vdots \\ (a^{r-1}a) & \dots & (a^{r-1}a^{r-1}) \end{vmatrix}}} \quad (r=1, 2, \dots, n+1).$$

$${}_1a_i = a_i,$$

$$({}_r a_p a) = 0, (a \neq p)$$

$$({}_r a_p a) = 1 \quad (a = p).$$

Now, instead of the curve Γ' , we consider a straight line g through the point P_0 on the curve Γ whose direction cosines are $(_1a)$. If we take n consecutive lines g', g'', \dots, g^n through the points P_1, P_2, \dots, P_n respectively and let the lines p_1, p_2, \dots, p_n be parallel to the lines g', g'', \dots, g^n through the point P_0 , then the equation (15) gives the direction cosines of the line $({}_r a)$ which is in the plane manifold passing through the lines $g, p_1, p_2, \dots, p_{r-1}$ and orthogonal to the one passing through the lines $g, p_1, p_2, \dots, p_{r-2}$.

And $\frac{1}{R_r}$ which is given by the equation (14) shall be called the r^{th} curvature of the curve Γ at the point P_0 with respect to the line g .

Let θ be the angle between the line $({}_r a)$ and the line which is in the plane manifold passing $g, p_1, p_2, \dots, p_{r-2}, p_r$ and orthogonal to the one passing through $g, p_1, p_2, \dots, p_{r-2}$, then it is evident that

$$\lim_{\Delta t \rightarrow 0} \frac{{}_r\theta}{\text{arc } P_0 P_1} = \frac{1}{R_r}.$$

Differentiating ${}_r a_i$ with respect to t , we have.

$$(16) \quad \frac{d_r a_i}{dt} = \frac{1}{D_{r-1}^{\frac{3}{2}} D_{r+1}^{\frac{3}{2}}} \{ D_{r-1}^2 N_{r+1} - D_r^2 N_{r-1} \}$$

where

$$N_r = \begin{vmatrix} (aa) & \dots & (aa^{r-2}) & a_i \\ \vdots & & \vdots & \vdots \\ (a^{r-1}a) & \dots & (a^{r-1}a^{r-2}) & a_i^{r-1} \end{vmatrix}.$$

Hence, we have

$$\frac{d_r a_i}{ds} = \frac{r+1 a_i}{R_r} - \frac{r-1 a_i}{R_{r-1}}, \quad (r=2, 3, \dots, n).$$

$$(17) \quad \frac{d_1 a_i}{ds} = \frac{_2 a_i}{R_1},$$

$$\frac{d_{n+1}a_i}{ds} = -\frac{n a_i}{R_n}$$

$$(i=1, 2, \dots, n).$$

These are generalized Brunel¹ and Landsbergs¹ formula.

7. From the equations (17), we have

$$\left(\frac{d_r a}{ds}, \frac{d_r a}{ds} \right) = -\frac{I}{R_r^2} + \frac{I}{R_{r-1}^2} \equiv -\frac{I}{r_r^2} (\equiv K_r^2),$$

$$\left(\frac{d_1\alpha}{ds} - \frac{d_1\alpha}{ds} \right) = \frac{I}{R_1^2} \equiv \frac{I}{r^2} (\equiv K_1^2),$$

$$\left(\frac{d_{n+1}\alpha}{ds} \quad \frac{d_{n+1}\alpha}{ds} \right) = \frac{\mathbf{I}}{R_n^2} \equiv \frac{\mathbf{I}}{\gamma_{n+1}^2} (\equiv K_{n+1}^2).$$

So we get

$$\frac{I}{R_2^2} = \frac{I}{r_2^2} - \frac{I}{r_1^2},$$

$$\frac{I}{R_3^2} = \frac{I}{r_3^2} - \frac{I}{R_2^2} = \frac{I}{r_3^2} - \frac{I}{r_2^2} + \frac{I}{r_1^2}$$

(18)

$$\frac{I}{R^2} = \frac{I}{r_i^2} - \frac{I}{R_{i-1}^2} = \frac{I}{r_i^2} - \frac{I}{r_{i-1}^2} + \frac{I}{r_{i-2}^2} + \dots + (-1)^{i-1} \frac{I}{r_1^2},$$

$$I \rightarrow I_+ - I_- = I_+ + (-1)^{n-1} I_-$$

$$= \frac{\mathbf{I}}{2},$$

1 May 19

Math. Ann. 1
Call. I. 114

Putting

$$\frac{I}{\rho_i} = + \sqrt{\frac{I}{r_i^2} - \frac{I}{r_{i-1}^2} + \dots + (-1)^{i-1} \frac{I}{r_1^2}} = \frac{I}{R_i},$$

$(i=2, 3, \dots, n-1)$

$$\frac{I}{\rho_n} = \frac{I}{r_{n+1}} = - \sqrt{\frac{I}{r_n^2} - \frac{I}{r_{n-1}^2} + \dots + (-1)^{n-1} \frac{I}{r_1^2}}$$

We have

$$(19) \quad \begin{aligned} \frac{da_i}{ds} &= \frac{2a_i}{r_1}, \\ \frac{d_2a_i}{ds} &= \frac{3a_i}{\rho_2} - \frac{1a_i}{r_1} \\ \frac{d_3a_i}{ds} &= \frac{4a_i}{\rho_3} - \frac{2a_i}{\rho_2} \end{aligned}$$

.....

$$\frac{d_na_i}{ds} = \frac{n+1a_i}{\rho_n} - \frac{n-1a_i}{\rho_{n-1}}$$

$$\frac{d_{n+1}a_i}{ds} = - \frac{n a_i}{\rho_n}$$

The formulas (18) and (19) are those which were given by Meyer¹ who defines K_r as the r^{th} curvature of the curve I' with respect to the line g .

3 Dimensional Space.

8. Let (x) be a point orthogonal to (x) and on the tangent, (y) orthogonal to (x) on the principal normal, (z) orthogonal to (x) on the binormal, then

$$(x\mathcal{X}) = (x\mathcal{Y}) = (x\mathcal{Z}) = (\mathcal{X}\mathcal{Y}) = (\mathcal{X}\mathcal{Z}) = (\mathcal{Y}\mathcal{Z}) = 0.$$

If we, hereafter, take as our parameter on the given curves the length of arc, then

¹ loc. cit.

$$x'_i = \frac{dx_i}{ds}, \quad (x'x') = 1, \quad (i=0, 1, 2, 3)$$

and

$$\mathcal{X}_i = kx'_i,$$

$$\mathcal{Y}_i = -\frac{\rho}{k}(x_i + kx''_i),$$

$$\mathcal{Z}_i = \rho \frac{\partial}{\partial t_i} \left| \begin{array}{c} t \\ x \\ x' \\ x'' \end{array} \right|,$$

$$(\mathcal{X}\mathcal{X}) = k^2, \quad (\mathcal{Y}\mathcal{Y}) = k^2, \quad (\mathcal{Z}\mathcal{Z}) = k^2$$

and

$$\frac{d\mathcal{X}_i}{ds} = \frac{\mathcal{Y}_i}{\rho} - \frac{x_i}{k},$$

$$\frac{d\mathcal{Y}_i}{ds} = -\frac{\mathcal{X}_i}{\rho} - \frac{\mathcal{Z}_i}{\tau},$$

$$\frac{d\mathcal{Z}_i}{ds} = \frac{\mathcal{Y}_i}{\tau}, \quad (i=0, 1, 2, 3)$$

where ρ and τ are the curvature and torsion respectively.

9. If the curve Γ' be the evolute of the curve Γ or the curve traced by a point on the tangent of the curve P , then

$${}^0\eta_i = x_i,$$

$${}^1\eta_i = \mathcal{X}_i,$$

$${}^2\eta_i = \mathcal{Y}_i,$$

$${}^3\eta_i = -\mathcal{Z}_i,$$

$$R_0 = k, \quad R_1 = \rho, \quad R_2 = \tau, \quad \frac{I}{P_r} = 0, \quad \frac{I}{Q_r} = 0.$$

and we have

$$\frac{d_0\eta_i}{ds} = \frac{{}^1\eta_i}{R_0}, \quad \frac{d_1\eta_i}{ds} = \frac{{}^2\eta_i}{R_1} - \frac{{}^0\eta_i}{R_0}$$

$$\frac{d_2\eta_i}{ds} = \frac{{}^3\eta_i}{R_2} - \frac{{}^1\eta_i}{R_1}, \quad \frac{d_3\eta_i}{ds} = -\frac{{}^2\eta_i}{R_2} \quad (i=0, 1, 2, 3)$$

which are the formulas given by Bianchi.¹

10. Suppose Γ' be a curve traced by the point (2) which is orthogonal to (x) and on the principal normal. We get

$$a_i = \mathcal{Y}_i,$$

$$\eta_i = x_i,$$

$$\eta_i = \mathcal{Y}_i,$$

$$\eta_i = k \frac{\mathcal{Y}'_i}{\sqrt{(\mathcal{Y}'_i)^2}} = \frac{-\frac{x_i - \mathcal{X}_i}{\rho} - \frac{\mathcal{Y}_i}{\tau}}{\sqrt{\frac{1}{\rho^2} + \frac{1}{\tau^2}}},$$

$$\eta_i = \frac{\frac{x_i - \mathcal{X}_i}{\rho} - \frac{\mathcal{Y}_i}{\tau}}{\sqrt{\frac{1}{\rho^2} + \frac{1}{\tau^2}}},$$

$$(i=0, 1, 2, 3).$$

and

$$\begin{aligned} \frac{1}{R_1} &= \sqrt{\frac{1}{\rho^2} + \frac{1}{\tau^2}}, \\ \frac{1}{R_2} &= \frac{\tau \frac{d\rho}{ds} - \rho \frac{d\tau}{ds}}{\rho^2 + \tau^2} = \frac{\frac{1}{\rho} \frac{d}{ds} \left(\frac{1}{\tau} \right) - \frac{1}{\tau} \frac{d}{ds} \left(\frac{1}{\rho} \right)}{\frac{1}{\rho^2} + \frac{1}{\tau^2}}, \\ \frac{1}{P_0} &= \frac{1}{k}, \quad \frac{1}{P_1} = 0, \quad \frac{1}{P_2} = 0, \\ \frac{1}{P_3} &= \frac{1}{k^2 \tau \rho} \frac{1}{\left(\frac{1}{\rho} \frac{d}{ds} \left(\frac{1}{\tau} \right) - \frac{1}{\tau} \frac{d}{ds} \left(\frac{1}{\rho} \right) \right)}, \\ \frac{1}{Q_0} &= 0, \quad \frac{1}{Q_1} = 0, \quad \frac{1}{Q_2} = -\frac{1}{k \rho \sqrt{\frac{1}{\rho^2} + \frac{1}{\tau^2}}} \end{aligned}$$

¹ Lezioni di Geometria Differenziale, p. 457. A. Razzaboni, Le formale del Frenet in geometria iperbolica e loro applicazioni. (Bologna, Gamberini 1897). Also see Nischiali, loc. cit.

$$\frac{1}{Q_3} = - \frac{\sqrt{\frac{1}{\rho^2 k^2} \left(\frac{1}{\rho^2} + \frac{1}{\tau^2} \right) + E^2}}{k \tau E \sqrt{\frac{1}{\rho^2} + \frac{1}{\tau^2}}},$$

$${}^0\xi_i = \mathcal{X}_i, \quad {}^3\xi_i = - \frac{\frac{\mathcal{X}_i - \mathcal{Y}_i}{\tau} - \frac{\rho}{\sqrt{\frac{1}{\rho^2} + \frac{1}{\tau^2}}}}{\sqrt{\frac{1}{\rho^2} + \frac{1}{\tau^2}}} = - {}^3\eta_i,$$

$${}^2\zeta_i = x_i, \quad {}^3\zeta_i = \frac{1}{k} \frac{k E x_i + \frac{1}{\rho} \left(\frac{\mathcal{Y}_i - \mathcal{X}_i}{\tau} \right)}{\sqrt{\frac{1}{k^2 \rho^2} \left(\frac{1}{\rho^2} + \frac{1}{\tau^2} \right) + E^2}}$$

$$(i=0, 1, 2, 3)$$

where

$$E = \frac{1}{\rho} \frac{d}{ds} \left(\frac{1}{\tau} \right) - \frac{1}{\tau} \frac{d}{ds} \left(\frac{1}{\rho} \right).$$

Hence, we have

$$\frac{1}{R_1^2} \left(\frac{1}{Q_3^2} - \frac{1}{k^2 P_3^2} \right) = \frac{1}{k^2 \tau^2},$$

$$\frac{1}{P_3 R_2} = \frac{1}{\rho \tau} \cdot \frac{1}{R_1^2},$$

$$\frac{1}{R_1 Q_2} + \frac{1}{k \rho} = 0.$$

and

$$\frac{d {}^0\eta_i}{ds} = \frac{{}^0\xi_i}{P_0}, \quad \frac{d {}^1\eta_i}{ds} = \frac{{}^2\eta_i}{R_1},$$

$$\frac{d {}^2\eta_i}{ds} = \frac{{}^3\eta_i}{R_2} - \frac{{}^1\eta_i}{R_1} - \frac{{}^2\zeta_i}{Q_2},$$

$$\frac{d {}^3\eta_i}{ds} = - \frac{{}^2\eta_i}{R_2} + \frac{{}^3\xi_2}{P_3} - \frac{{}^3\zeta_i}{Q_3}.$$

$$(i=0, 1, 2, 3)$$

11. If Γ and Γ' have the same principal normal, then the equations of the curve Γ' will be

$$a_i = x_i \sin \frac{r}{k} + y_i \cos \frac{r}{k},$$

$$(i=0, 1, 2, 3),$$

and the coordinates of a points on the principal normal to Γ' and orthogonal to (a) will be

$$\bar{y}_i = x_i \cos \frac{r}{k} - y_i \sin \frac{r}{k},$$

$$(i=0, 1, 2, 3).$$

And we have

$$(\bar{y} da) = 0$$

or

$$k^2 dr = 0$$

i. e.

$$r = \text{const.},$$

and we can find such quantities λ, μ, ν that

$$\bar{y}_i = \lambda a_i + \mu a'_i + \nu a''_i.$$

Multiplying through a'_i, \bar{y}_i and adding, we get

$$\mu(a' a') + \nu(a'' a') = 0,$$

$$\mu(a' \bar{y}) + \nu(a'' \bar{y}) = 0.$$

Eliminating μ, ν ,

$$\begin{vmatrix} (a' a') (a'' a') \\ (a' \bar{y}) (a'' \bar{y}) \end{vmatrix} = 0$$

or

$$k \left\{ \frac{1}{\rho} \frac{d}{ds} \left(\frac{1}{\tau} \right) - \frac{1}{\tau} \frac{d}{ds} \left(\frac{1}{\rho} \right) \right\} = \tan \frac{r}{k} \frac{d}{ds} \left(\frac{1}{\tau} \right).$$

Hence, we have

$$\frac{k}{\tau} + \frac{Ck}{\rho} = C \tan \frac{r}{k} \quad (C: \text{integration const.})$$

This is the corresponding relation given by Bertrand in the Euclidean case.

And

$$\begin{aligned} \frac{I}{R_1} &= \frac{\sqrt{(a' a')}}{k \cos \frac{r}{k}} = \frac{1}{\tau} \sqrt{\frac{1}{C^2} + 1}, \quad \frac{I}{R_2} = 0 \\ \frac{I}{P_0} &= \frac{I}{k}, \quad \frac{I}{P_1} = \frac{I}{k} \tan \frac{r}{k}, \quad \frac{I}{P_2} = 0 \\ \frac{I}{Q_0} &= 0, \quad \frac{I}{Q_1} = 0, \\ \frac{I}{Q_2} &= \frac{\sin \frac{r}{k} - \frac{k}{\rho} \cos \frac{r}{k}}{k \cos \frac{r}{k} \sqrt{(a' a')}} = \frac{I}{k \cos \frac{r}{k} \sqrt{1 + C^2}}, \\ \eta_i &= x_i, \quad i\eta_i = y_i, \quad i\eta_i = \frac{k a'}{\sqrt{(a' a')}}, \\ {}_0\xi_i &= x_i, \quad {}_1\xi_i = -x_i, \quad {}_2\xi_i = x_i, \\ {}_2\xi_i &= \cos \frac{r}{k} x_i - \sin \frac{r}{k} y_i = \bar{y}_i. \end{aligned}$$

Hence, we have

$$\begin{aligned} \frac{I}{R_1} \cdot \frac{I}{Q_2} &= \frac{I}{C k \cos \frac{r}{k}} - \frac{I}{\tau} \\ &= \frac{I}{k \cos \frac{r}{k}} \left[\frac{I}{P_1} - \frac{I}{\rho} \right] \end{aligned}$$

or

$$\frac{I}{R_1} \cdot \frac{I}{Q_2} = \frac{I}{k \cos \frac{r}{k}} \left[\frac{I}{P_1} - \frac{I}{\rho} \right],$$

and the generalized Serret-Frenet formula will be

$$\frac{d \eta_i}{ds} = \frac{\xi_i}{P_0},$$

$$\frac{d \eta_i}{ds} = \frac{\eta_i}{R_1} + \frac{\xi_i}{P_1},$$

$$\frac{d \eta_i}{ds} = -\frac{\eta_i}{R_1} - \frac{\xi_i}{Q_2}, \quad (i=0, 1, 2, 3)$$

And (η) will be on the absolute.

12. If the principal normal of the curve I' be the binormal of the curve I'' , we have

$$a_i = x_i \sin \frac{r}{k} + y_i \cos \frac{r}{k}$$

$$(i=0, 1, 2, 3)$$

and let (\bar{g}) be the coordinates of the points on the binormal of I'' and orthogonal to (a) , then

$$\bar{g}_i = x_i \cos \frac{r}{k} - y_i \sin \frac{r}{k},$$

and we have

$$(a' \bar{g}_i) = 0,$$

$$(a'' \bar{g}_i) = 0.$$

Hence we get

$$r = \text{const.},$$

$$\left(\frac{k^2}{\rho^2} + \frac{k^2}{\tau^2} - 1 \right) \sin \frac{r}{k} \cos \frac{r}{k} = \frac{k}{\rho} \left(\sin^2 \frac{r}{k} - \cos^2 \frac{r}{k} \right).$$

And

$$\frac{1}{R_1} = \frac{\sqrt{(a' a')}}{k \cos \frac{r}{k}},$$

$$\frac{1}{R_2} = \frac{k \cos \frac{r}{k} \sin \frac{r}{k} \left[\left(\sin \frac{r}{k} - \frac{r}{\rho} \cos \frac{r}{k} \right) \frac{d}{ds} \left(\frac{1}{\tau} \right) + \frac{k}{\tau} \frac{d}{ds} \left(\frac{1}{\tau} \right) \cos \frac{r}{k} \right]}{\sin \frac{r}{k} - \frac{k}{\rho} \cos \frac{r}{k}}$$

$$\frac{\mathbf{I}}{P_0} = \frac{\mathbf{I}}{k}, \quad \frac{\mathbf{I}}{P_1} = \frac{\mathbf{I}}{k} \tan \frac{r}{k}, \quad \frac{\mathbf{I}}{P_2} = 0, \quad \frac{\mathbf{I}}{P_3} = 0.$$

$$\frac{\mathbf{I}}{Q_0} = 0, \quad \frac{\mathbf{I}}{Q_1} = 0, \quad \frac{\mathbf{I}}{Q_2} = \frac{\mathbf{I}}{k} \tan \frac{r}{k} \sqrt{(a' a')}$$

$$\frac{\mathbf{I}}{Q_3} = -\frac{\mathbf{I}}{\tau \sqrt{(a' a')}}$$

Hence, we have

$$\frac{\mathbf{I}}{Q_2} \frac{\mathbf{I}}{Q_3} = -\frac{\tan \frac{r}{k}}{k \tau},$$

$$k^2 \cos^2 \frac{r}{k} \frac{d}{ds} \left(\frac{R_1}{Q_3} \right) + \frac{Q_2^2}{R_2} = 0$$

and the generalized Serret-Frenet formula will be

$$\frac{d \eta_i}{ds} = \frac{\xi_i}{P_0},$$

$$\frac{d \eta_i}{ds} = \frac{\eta_i}{R_1} + \frac{\xi_i}{P_1},$$

$$\frac{d \eta_i}{ds} = \frac{\eta_i}{R_2} - \frac{\eta_i}{R_1} - \frac{\xi_i}{Q_2}.$$

$$\frac{d \eta_i}{ds} = -\frac{\eta_i}{R_2} - \frac{\xi_i}{Q_3}.$$

$$(i=0, 1, 2, 3)$$

13. Suppose I'' be a curve traced by the points (γ) which is orthogonal to (x) and on the binormal, then

$$a_i = \gamma_i$$

$$\frac{\mathbf{I}}{R_1} = \frac{\mathbf{I}}{\tau}, \quad \frac{\mathbf{I}}{R_2} = \frac{\mathbf{I}}{\rho},$$

$$\frac{\mathbf{I}}{P_0} = \frac{\mathbf{I}}{k}, \quad \frac{\mathbf{I}}{P_1} = 0, \quad \frac{\mathbf{I}}{P_2} = 0, \quad \frac{\mathbf{I}}{P_3} = 0.$$

$$\frac{\mathbf{I}}{Q_1} = 0, \quad \frac{\mathbf{I}}{Q_2} = 0, \quad \frac{\mathbf{I}}{Q_3} = \frac{\mathbf{I}}{k}.$$

$$\begin{aligned} {}_0\eta_i &= x_i, & {}_1\eta_i &= \mathcal{J}_i, & {}_2\eta_i &= \mathcal{Y}_i \\ {}_3\eta_i &= -\mathcal{X}_i, & {}_3\zeta_i &= -x_i & (i=0, 1, 2, 3) \end{aligned}$$

And the generalized Serret-Frenet formula will be

$$\begin{aligned} \frac{d {}_0\eta_i}{ds} &= \frac{{}_0\xi_i}{P_0} \\ \frac{d {}_1\eta_i}{ds} &= \frac{{}_2\eta_i}{R_1}, \quad \frac{d {}_2\eta_i}{ds} = \frac{{}_3\eta_i}{R_2} - \frac{{}_1\eta_i}{R_1} \\ \frac{d {}_3\eta_i}{ds} &= -\frac{{}_2\eta_i}{R_2} - \frac{{}_3\zeta_i}{Q_3} \\ (i &= 0, 1, 2, 3). \end{aligned}$$

14. If the binormal of the curve Γ be the principal normal to the curve Γ' and let $(\bar{\mathcal{Y}})$ be the coordinates of the point on the binormal of the curve Γ' and orthogonal to (a) , then

$$\begin{aligned} a_i &= x_i \sin \frac{r}{k} + \mathcal{J}_i \cos \frac{r}{k}, \\ \bar{\mathcal{Y}}_i &= x_i \cos \frac{r}{k} - \mathcal{J}_i \sin \frac{r}{k} \\ (i &= 0, 1, 2, 3) \end{aligned}$$

and

$$(\bar{\mathcal{Y}} d a) = 0$$

we get

$$r = \text{const.}$$

More over we can find such quantities λ, μ, ν that

$$\bar{\mathcal{Y}}_i = \lambda a_i + \mu a'_i + \nu a''_i$$

Multiplying through $a'_i, \bar{\mathcal{Y}}_i$ and adding, we have

$$\begin{aligned} \mu(a' a') + \nu(a'' a') &= 0, \\ \mu(a' \bar{\mathcal{Y}}) + \nu(a'' \bar{\mathcal{Y}}) &= 0 \end{aligned}$$

or

$$\begin{vmatrix} (\alpha' \alpha) & (\alpha' \alpha'') \\ (\alpha' \beta) & (\alpha'' \beta) \end{vmatrix} = 0$$

i. e.

$$\frac{I}{\rho} \tan^2 \frac{r}{k} + k \frac{d}{ds} \left(\frac{I}{\tau} \right) \tan \frac{r}{k} + \frac{k^2}{\rho \tau^2} = 0.$$

and

$$\frac{I}{R_1} = \frac{\sqrt{(\alpha' \alpha')}}{k \cos \frac{r}{k}} = \sqrt{\frac{I}{k^2} \tan^2 \frac{r}{k} + \frac{I}{\tau^2}}, \quad \frac{I}{R_2} = 0$$

$$\frac{I}{P_0} = \frac{I}{k}, \quad \frac{I}{P_1} = \frac{I}{k} \tan \frac{r}{k}, \quad \frac{I}{P_2} = 0$$

$$\frac{I}{Q_0} = 0, \quad \frac{I}{Q_1} = 0, \quad \frac{I}{Q_2} = \frac{\tan \frac{r}{k}}{k \sqrt{(\alpha' \alpha')}}.$$

So we have

$$\frac{I}{R_1} \frac{I}{Q_2} = \text{const.}, \quad \frac{I}{P_1} = \text{const.}$$

and

$$\frac{d \eta_i}{ds} = \frac{\xi_i}{P_0},$$

$$\frac{d \eta_i}{ds} = \frac{\eta_i}{R_1} + \frac{\xi_i}{P_1},$$

$$\frac{d \eta_i}{ds} = - \frac{\eta_i}{R_1} - \frac{\xi_i}{Q_2}$$

where

$$\eta_i = x_i, \quad \eta_i = y_i, \quad \eta_i = \frac{k \alpha'_i}{\sqrt{(\alpha' \alpha')}}.$$

$$\xi_i = \mathcal{X}_i, \quad \xi_i = -\mathcal{Y}_i$$

$$\xi_i = \bar{\mathcal{Y}}_i, \quad (i=0, 1, 2, 3).$$

And $(s\eta)$ will be on the absolute.

15. If the binormal of the curve Γ' be that of the curve Γ , and let $(\bar{\gamma})$ be the coordinates of a points on the binormal to Γ' and orthogonal to (α) , then

$$\alpha_i = x_i \sin \frac{r}{k} + y_i \cos \frac{r}{k},$$

$$y_i = x_i \cos \frac{r}{k} - y_i \sin \frac{r}{k}$$

$$= -\frac{\partial}{\partial t_i} \left| t \alpha \alpha' \alpha'' \right|$$

$$(i=0, 1, 2, 3),$$

and

$$(\alpha' \bar{\gamma}) = (\alpha'' \bar{\gamma}) = 0.$$

Hence, we have

$$r = \text{const.}$$

$$\frac{I}{\tau^2} = \frac{I}{k^2}.$$

In this case, it is evident that the binormals will generate a ruled surface with vanishing Gaussian curvature.¹

And

$$\frac{I}{R_1} = \frac{I}{k \cos \frac{r}{k}}, \quad \frac{I}{R_2} = \frac{I}{\rho}.$$

$$\frac{I}{P_0} = \frac{I}{k}, \quad \frac{I}{P_1} = \frac{I}{k} \tan \frac{r}{k}, \quad \frac{I}{P_2} = 0, \quad \frac{I}{P_3} = 0.$$

$$\frac{I}{Q_0} = 0, \quad \frac{I}{Q_1} = 0, \quad \frac{I}{Q_2} = \frac{I}{k} \tan \frac{r}{k}, \quad \frac{I}{Q} = \frac{I}{k}$$

$$s\eta_i = y_i \sin \frac{r}{k} - x_i \cos \frac{r}{k},$$

$$z\eta_i = x_i \sin \frac{r}{k} + y_i \cos \frac{r}{k},$$

¹ Coolidge. Non-Euclidean Geometry.

$$_1\eta_i = \mathcal{J}_i,$$

$$_1\xi_i = -\mathcal{X}_i,$$

$$_3\xi_i = \mathcal{J}_i \sin \frac{r}{k} - x_i \cos \frac{r}{k}$$

$$_2\xi_i = x_i \cos \frac{r}{k} - \mathcal{J}_i \sin \frac{r}{k}$$

$$(i=0, 1, 2, 3)$$

So the generalized formula will be

$$\frac{d_0\eta_i}{ds} = \frac{0\xi_i}{P_0},$$

$$\frac{d_1\eta_i}{ds} = \frac{1\eta_i}{R_1} + \frac{1\xi_i}{P_1}$$

$$\frac{d_2\eta_i}{ds} = \frac{2\xi_i}{R_2} - \frac{1\eta_i}{R_1} - \frac{2\xi_i}{Q_2}$$

$$\frac{d_3\eta_i}{ds} = -\frac{2\eta_i}{R_2} - \frac{3\xi_i}{Q_3}$$

$$(i=0, 1, 2, 3)$$

In conclusion, the author wishes to express his sincere thanks to Prof. Nischiuchi for his kind guidance and valuable remarks and also to Asst. Prof. T. Matsumoto for his kind remarks.