

# A Theoretical Note on the Diurnal Variation of Wind-Vector due to the Variation of Eddy Viscosity<sup>1</sup>

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## I. Introduction

The diurnal variation of wind-vector in the lower atmosphere is a familiar phenomenon in meteorology and it is generally accepted that this phenomenon is a consequence of the daily convection. As for the variation in the atmospheric layer above the flat open land-area where no local orographic influence appears, the classical Espy-Köppen's theory is well known. Prof. G. I. Taylor<sup>2</sup> modified this theory and concluded that this phenomenon is to be explained as a result of the diurnal variation of the coefficient of eddy viscosity. Assuming a quasi-steady state, he got an excellent simple theory which gives a clear explanation of the chief characteristic nature of the diurnal variation of wind-speed; but which fails to give a satisfactory explanation of the diurnal characteristics of wind-direction. The diurnal variation of wind-direction is also a remarkable phenomenon, but there is no comprehensive dynamical theory which explains the diurnal characteristics of wind-direction as well as of wind-speed. Iswekov's report of his study,<sup>3</sup> dealing with cases where the eddy viscosity changes periodically, is full of instructive hints for the author's present study. It must be borne in mind, however, that he does not attempt to inquire into the question of why the diurnal variation of wind occurs as a result of the variation of the eddy viscosity; i. e., as he gives a periodic function for the wind at the earth's surface, his study must be considered to have been directed only to the propagative nature of diurnal wind-vector in an atmospheric layer which is subject to a periodic change of eddy viscosity. H. Futi<sup>4</sup> has also treated the propagating nature of the diurnal wind-vector in a case where the eddy viscosity varies with altitude. What the writers intend now is an attempt to construct a

1. The outline of this paper was read at the Annual Meeting of Physico-Mathematical Society of Japan in Apr. 1935. 2. Proc. Roy. Soc. London. Ser. A. XCIV, 137.

3. Met. Zs. 46, 1 (1929). 4. Jap. J. Met. 10, 6, 345.

dynamical theory concerning the origin of the diurnal wind-vector, under Prof. G. I. Taylor's ingenious suggestion, and not a general discussion of the diurnal variation of the wind.

## II. The Problem and its Approximate Solution

Let us suppose a simplified case containing all the essential points of our problem, and by solving this idealized case, come to our final conclusion.

### (i) Dynamical equation

With the usual notations, we have

$$\begin{aligned} \frac{\partial \bar{u}}{\partial t} &= 2\omega \bar{v} \sin \varphi + \frac{1}{\rho} \frac{\partial}{\partial z} \left( K \frac{\partial \bar{u}}{\partial z} \right) \\ \frac{\partial \bar{v}}{\partial t} &= -2\omega \bar{u} \sin \varphi + \frac{1}{\rho} \frac{\partial}{\partial z} \left( K \frac{\partial \bar{v}}{\partial z} \right) - \frac{1}{\rho} \frac{\partial \rho}{\partial y}. \end{aligned}$$

Putting  $\lambda = 2\omega \sin \varphi$ ,  $k = \frac{K}{\rho}$ ,  $G = -\frac{1}{\rho \lambda} \frac{\partial \rho}{\partial y}$ ,  $u = \bar{u} + G$ ,

$$v = \bar{v}, \quad V = u + iv, \quad \text{and} \quad i = \sqrt{-1},$$

we get  $\frac{\partial V}{\partial t} + i\lambda V = k \frac{\partial^2 V}{\partial z^2}$  .....(1)

for the working dynamical equation.

### (ii) Coefficient of eddy viscosity (k).

In order to simplify the mathematical treatment, we consider a most simple case which barely serves our purpose, i. e.,

$$k = k_0 - k_1 \cos \sigma t \quad \dots\dots\dots(2)$$

( $t=0$  at midnight;  $\sigma = 2\pi/T$ ,  $T=24$  hours) where  $k_0$  and  $k_1$  are given constants independent of height ( $z$ ) and time ( $t$ ).

### (iii) Upper boundary condition.

We assume that a given constant gradient wind velocity ( $G$ ) prevails at a certain height ( $H$ ), i. e.,  $\bar{u} = G$  or  $u = 0$  at  $z = H$ , .....(3)

where  $H$  is assumed independent of time.

### (iv) Bottom-surface condition.

At first, we consider a reasonable condition, viz.,

$$k \frac{\partial V}{\partial z} \Big|_{z=0} = 0.002 (V_0 + G) |V_0 + G|,$$

where suffix 0 indicates the surface-value of the wind-vector. But this condition is non-linear and causes some serious mathematical difficulties, therefore it is advantageous to make some simplification. Thus, in spite of unavoidable depreciation in the validity of the solution, we must perform the linearization of the above condition. In this way, we

suppose a fundamental state and introduce a wind-vector,  $\bar{V}$ , which satisfies the equation of  $i\lambda\bar{V} = k_0 \frac{\partial^2 \bar{V}}{\partial z^2}$ ; then we get  $\bar{V} = C \sinh \beta_0(H-z)$  as a solution of the above equation which satisfies the boundary condition of  $\bar{V} = 0$  at  $z = H$ , where  $\beta_0 = \sqrt{\lambda/k_0} e^{i\pi/4}$  and the arbitrary constant  $C$  can be found by the aid of the method of numerical trials from the condition,

$$k_0 \frac{\partial \bar{V}}{\partial z} \Big|_{z=0} = 0.002(V_0 + G) |V_0 + G|$$

which is introduced also for the fundamental state.

Having simplified the non-linear surface condition by the elimination of the fundamental part above mentioned, we have for a deviating part  $V' (= V - \bar{V})$ ,

$$\frac{\partial V'}{\partial z} \Big|_{z=0} - c \cos \sigma t \frac{\partial \bar{V}}{\partial z} \Big|_{z=0} = q V_0', \dots\dots\dots (4)$$

where  $q = \frac{0.002}{k_0} |\bar{V}_0 + G|$  and  $c = k_1/k_0$ .

This adapted method of approximation which involves an assumption of  $|\bar{V}_0 + G + V_0'| \approx |\bar{V}_0 + G|$ , may invite serious objection. Indeed, this is the most difficult point in the authors' present study; yet they believe that the essential character of the problem remains unaltered. It must be admitted, however, that the solution thus obtained is not exact and in fact this study degenerates into the framing of a semi-quantitative theory.

(v) *Stationary condition.*

Instead of an initial condition, we take  $V(t) = V(t + T) \dots (5)$  from the nature of the problem.

(vi) *The required solution.*

Now we consider a particular solution of eq. (1), which satisfies the condition (3),

$$V = A_n e^{(k_0 \beta_n^2 - i\lambda)t - \frac{k_1 \beta_n^2}{\sigma} \sin \sigma t} \sinh \beta_n(H-z)$$

and  $\beta_n$  is determined by the condition (5), i. e.,

$$\beta_n^2 = i(n\sigma + \lambda)/k_0 \quad (n = 0 \pm 1 \pm 2 \dots\dots\dots)$$

or  $\beta_n = B_n e^{i\pi/4} \quad B_n = \sqrt{\frac{\varepsilon(n\sigma + \lambda)}{k_0}} \quad \left. \begin{array}{l} \varepsilon = 1 \quad \text{for } n\sigma + \lambda \geq 0 \\ \varepsilon = -1 \quad \text{for } n\sigma + \lambda < 0 \end{array} \right\} \dots (6)$

Thus we have an appropriate solution,

$$V = \sum_{-\infty}^{+\infty} A_n e^{in\pi/4} \sinh \beta_n(H-z) \dots\dots\dots (7)$$

$$(x = \sigma t - c \sin \sigma t, \quad \gamma = \lambda k_1 / \sigma k_0)$$

where constant-vectors  $A_n$  are determined by the remaining condition (4). Using the following two auxiliary expressions of Fourier's expansion,

$$e^{i\gamma \sin \sigma t} = \sum_{n=-\infty}^{n=+\infty} b_n e^{inx}, \quad \text{and} \quad \cos \sigma t e^{i\gamma \sin \sigma t} = \sum_{n=-\infty}^{n=+\infty} c_n e^{inx}$$

where 
$$b_n = \frac{1}{2\pi} \int_0^{2\pi} e^{i\gamma \sin \sigma t} e^{-inx} dx = \frac{\gamma}{nc + \gamma} J_n(nc + \gamma)$$

and

$$c_n = \frac{1}{2\pi} \int_0^{2\pi} \cos \sigma t e^{i\gamma \sin \sigma t} e^{-inx} dx = \frac{n J_n(nc + \gamma)}{nc + \gamma} - \frac{c}{2} \left\{ \frac{(n-1)}{nc + \gamma} J_{n-1}(nc + \gamma) + \frac{n+1}{nc + \gamma} J_{n+1}(nc + \gamma) \right\} \dots\dots (8)$$

and noticing

$$V' = V - \bar{V} = \sum_{n=-\infty}^{+\infty} \left\{ A_n \sinh \beta_n(H-z) - b_n C \sinh \beta_0(H-z) \right\} e^{-i\gamma \sin \sigma t + inx}$$

we get from the condition (4)

$$A_n = \frac{\beta_0 \cosh \beta_0 H (b_n + c C_n) + q b_n \sinh \beta_0 H}{\beta_n \cosh \beta_n H + q \sinh \beta_n H} C \dots\dots (9)$$

The required solution devised for the numerical computations is arranged as follows :—

$$V = \bar{V} + V' \quad \bar{V} = C \sinh \beta_0(H-z)$$

$$V' = \bar{V} \sum_{n=-\infty}^{n=+\infty} \tau v_n e^{-i\gamma \sin \sigma t + inx}$$

where

$$\tau v_n = \left\{ \frac{\beta_0(b_n + c C_n) \coth \beta_0 H + q b_n}{\beta_n \coth \beta_n H + q} \frac{\sinh \beta_n(H-z)}{\sinh \beta_n H} \frac{\sinh \beta_0 H}{\sinh \beta_0(H-z)} - b_n \right\} \dots\dots\dots (10)$$

and the resultant wind vector is  $V + G$  where  $G$  is the given gradient velocity.

### III. Numerical Examples

By giving two specified examples, we now try to make clear some main characters contained in the formal solution of (10).

*Ex. 1.* Assume  $k_0 = k_1 = 2 \times 10^4$ ,  $H = 10^5$ ,  $G = 5 \times 10^2$  and  $\varphi = 45^\circ$ , where all the units adopted are C. G. S. system. Then we have  $q = 3.3 \times 10^{-5}$ ,  $\gamma = 1.4$  and  $c = 1$ . The values of  $\beta_n$ ,  $b_n$  and  $c_n$  are calculated in Table 1. Table 2 gives the values of  $\bar{V}$  and  $V'$ (at  $t=0$ ), and the final results which represent the diurnal characters of wind-vector are shown in Figs. 1 and 2.

Table 1.

$\beta_0 = 7.21 \times 10^{-5} e^{i\pi/4}$	$b_0 = +0.567$	$c_0 = -0.388$
$\beta_1 = 9.33 \quad " \quad "$	$b_1 = +0.304$	$c_1 = +0.037$
$\beta_2 = 11.17 \quad " \quad "$	$b_2 = +0.193$	$c_2 = +0.085$
$\beta_3 = 12.73 \quad " \quad "$	$b_3 = +0.137$	$c_3 = +0.084$
$\beta_4 = 14.00 \quad " \quad "$	$b_4 = +0.098$	$c_4 = +0.067$
$\beta_5 = 15.26 \quad " \quad "$	$b_5 = +0.078$	$c_5 = +0.060$
$\beta_6 = 16.40 \quad " \quad "$	$b_6 = +0.064$	$c_6 = +0.052$
$\beta_{-1} = 3.82 \quad " \quad "$	$b_{-1} = -0.686$	$c_{-1} = +0.539$
$\beta_{-2} = 4.67 \times 10^{-5} e^{-i\pi/4}$	$b_{-2} = -0.102$	$c_{-2} = -0.104$
$\beta_{-3} = 7.64 \quad " \quad "$	$b_{-3} = -0.064$	$c_{-3} = -0.043$
$\beta_{-4} = 9.76 \quad " \quad "$	$c_{-4} = -0.045$	$c_{-4} = -0.029$
$\beta_{-5} = 11.45 \quad " \quad "$	$b_{-5} = -0.035$	$c_{-5} = -0.026$
$\beta_{-6} = 12.87 \quad " \quad "$	$b_{-6} = -0.030$	$c_{-6} = -0.014$

Table 2.  $V'$  (cm./sec., angle degree).

	$z=0$	$z=50^m$	$z=100^m$	$z=200^m$	$z=300^m$
$\bar{V}$	210 $\angle 152^{\circ}00'$	164 $\angle 138^{\circ}00'$	127 $\angle 123^{\circ}20'$	78 $\angle 95^{\circ}20'$	48 $\angle 67^{\circ}00'$
$n=0$	59.6 $\angle 345^{\circ}50'$	46.6 $\angle 331^{\circ}50'$	36.1 $\angle 317^{\circ}10'$	22.2 $\angle 289^{\circ}10'$	13.6 $\angle 260^{\circ}50'$
+1	6.6 $\angle 343^{\circ}30'$	11.0 $\angle 345^{\circ}40'$	11.7 $\angle 332^{\circ}40'$	11.2 $\angle 304^{\circ}20'$	8.6 $\angle 274^{\circ}20'$
+2	2.3 $\angle 340^{\circ}30'$	7.2 $\angle 351^{\circ}00'$	9.4 $\angle 336^{\circ}10'$	9.4 $\angle 303^{\circ}20'$	7.5 $\angle 269^{\circ}00'$
+3	2.1 $\angle 340^{\circ}40'$	7.2 $\angle 349^{\circ}50'$	9.0 $\angle 332^{\circ}50'$	8.3 $\angle 298^{\circ}30'$	6.2 $\angle 262^{\circ}40'$
+4	2.3 $\angle 340^{\circ}10'$	6.1 $\angle 347^{\circ}20'$	7.4 $\angle 329^{\circ}50'$	6.7 $\angle 293^{\circ}45'$	4.8 $\angle 258^{\circ}40'$
+5	2.5 $\angle 339^{\circ}10'$	5.6 $\angle 344^{\circ}30'$	6.7 $\angle 326^{\circ}30'$	5.7 $\angle 290^{\circ}30'$	3.9 $\angle 255^{\circ}30'$
+6	2.3 $\angle 340^{\circ}50'$	4.9 $\angle 343^{\circ}40'$	6.0 $\angle 324^{\circ}30'$	4.9 $\angle 288^{\circ}20'$	3.2 $\angle 252^{\circ}10'$
-1	50.0 $\angle 172^{\circ}00'$	27.9 $\angle 150^{\circ}10'$	13.6 $\angle 112^{\circ}30'$	19.3 $\angle 352^{\circ}30'$	24.5 $\angle 319^{\circ}20'$
-2	44.5 $\angle 61^{\circ}40'$	43.8 $\angle 71^{\circ}00'$	47.0 $\angle 107^{\circ}20'$	32.2 $\angle 81^{\circ}10'$	23.3 $\angle 87^{\circ}50'$
-3	18.7 $\angle 81^{\circ}20'$	19.0 $\angle 89^{\circ}10'$	17.9 $\angle 101^{\circ}20'$	11.3 $\angle 99^{\circ}20'$	5.6 $\angle 104^{\circ}00'$
-4	10.7 $\angle 81^{\circ}20'$	11.8 $\angle 98^{\circ}40'$	10.5 $\angle 102^{\circ}00'$	6.1 $\angle 106^{\circ}20'$	2.5 $\angle 100^{\circ}20'$
-5	9.0 $\angle 95^{\circ}40'$	9.0 $\angle 103^{\circ}30'$	7.6 $\angle 107^{\circ}50'$	4.1 $\angle 109^{\circ}50'$	1.5 $\angle 91^{\circ}50'$
-6	7.6 $\angle 108^{\circ}40'$	6.9 $\angle 110^{\circ}50'$	5.7 $\angle 113^{\circ}00'$	3.0 $\angle 109^{\circ}00'$	1.2 $\angle 78^{\circ}20'$

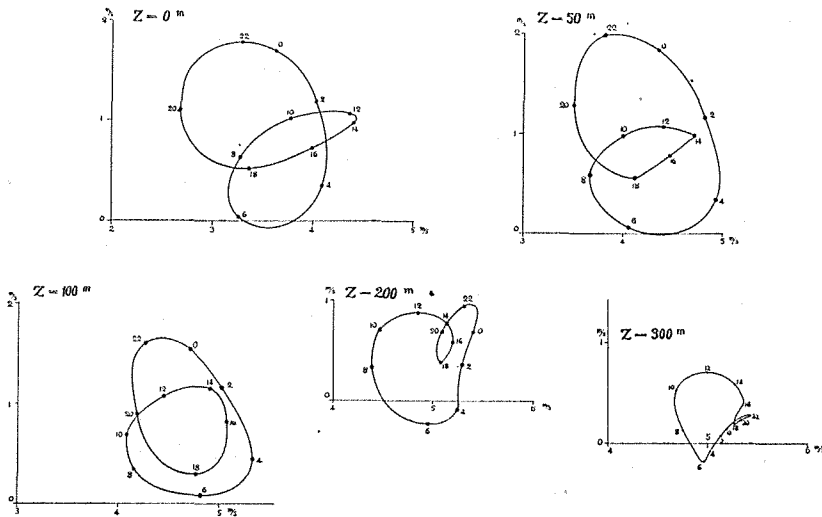
Table 3.  $V+G$  (m./sec., angle degree.)

Height Time	$z=0^m$	$z=50^m$	$z=100^m$	$z=200^m$	$z=300^m$
0 <sup>h</sup>	4.01 $\angle 25^{\circ}10'$	4.71 $\angle 23^{\circ}00'$	4.96 $\angle 18^{\circ}10'$	5.48 $\angle 7^{\circ}00'$	5.20 $\angle 1^{\circ}20'$
2	4.20 $\angle 16^{\circ}30'$	4.96 $\angle 13^{\circ}30'$	5.25 $\angle 12^{\circ}40'$	5.34 $\angle 3^{\circ}50'$	5.15 $\angle 0^{\circ}30'$
4	4.11 $\angle 5^{\circ}00'$	4.94 $\angle 3^{\circ}50'$	5.35 $\angle 4^{\circ}50'$	5.28 $\angle -1^{\circ}10'$	5.04 $\angle -1^{\circ}10'$
6	3.26 $\angle 0^{\circ}30'$	4.05 $\angle 0^{\circ}40'$	4.82 $\angle 0^{\circ}50'$	4.98 $\angle -2^{\circ}40'$	4.98 $\angle -2^{\circ}30'$
8	3.34 $\angle 11^{\circ}00'$	3.69 $\angle 9^{\circ}00'$	4.16 $\angle 4^{\circ}40'$	4.43 $\angle 4^{\circ}00'$	4.77 $\angle 1^{\circ}20'$

Table 3. Continued.

Height Time	$z=0^m$	$z=50^m$	$z=100^m$	$z=200^m$	$z=300^m$
10 <sup>h</sup>	3.91 $\angle 15^\circ 10'$	4.11 $\angle 13^\circ 40'$	4.13 $\angle 9^\circ 40'$	4.55 $\angle 9^\circ 20'$	4.73 $\angle 6^\circ 20'$
12	4.50 $\angle 13^\circ 50'$	4.53 $\angle 13^\circ 40'$	4.57 $\angle 13^\circ 30'$	4.95 $\angle 10^\circ 00'$	5.04 $\angle 7^\circ 40'$
14	4.52 $\angle 12^\circ 30'$	4.82 $\angle 11^\circ 40'$	5.04 $\angle 13^\circ 20'$	5.23 $\angle 8^\circ 30'$	5.31 $\angle 6^\circ 00'$
16	4.06 $\angle 10^\circ 10'$	4.53 $\angle 9^\circ 50'$	5.13 $\angle 9^\circ 20'$	5.26 $\angle 6^\circ 10'$	5.38 $\angle 3^\circ 50'$
18	3.36 $\angle 8^\circ 50'$	4.15 $\angle 7^\circ 30'$	4.78 $\angle 3^\circ 40'$	5.11 $\angle 4^\circ 00'$	5.27 $\angle 1^\circ 40'$
20	2.92 $\angle 22^\circ 40'$	3.74 $\angle 20^\circ 10'$	4.28 $\angle 12^\circ 00'$	5.17 $\angle 7^\circ 40'$	5.35 $\angle 2^\circ 10'$
22	3.50 $\angle 30^\circ 40'$	4.29 $\angle 27^\circ 30'$	4.56 $\angle 20^\circ 40'$	5.42 $\angle 10^\circ 00'$	5.44 $\angle 2^\circ 30'$

Fig. 1.



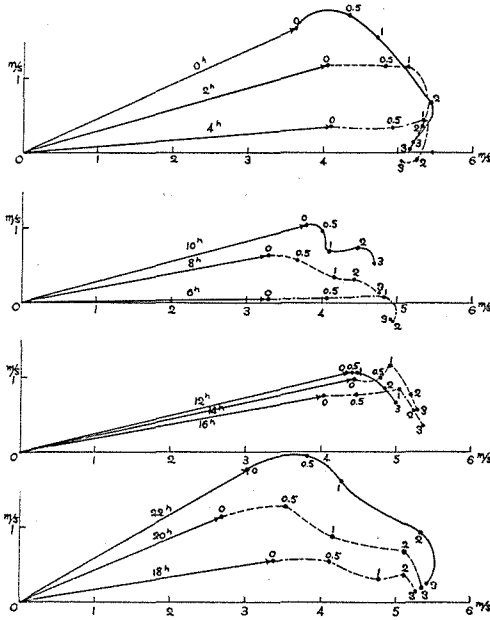
*Ex. 2.* All the assumed data are the same as in *Ex. 1*, except  $k_0 = 2k_1 = 2 \times 10^4$ . Results in this case are indicated by Tables 4 and 5.

#### IV. Conclusions and Remarks

(i) This paper is a short study of the diurnal variation of wind-vector caused by the variation of eddy viscosity. If we compare the proposed theory with the existing theories, we have to make the following remarks :

(a) Retaining the terms which contain  $\frac{\partial}{\partial t}$ , G. I. Taylor's quasi-

Fig. 2.



steady theory is modified by the writers, and a hydro-dynamical theory is obtained which may explain some of the chief diurnal characters of wind direction as well as wind speed.

(b) But as the present theory included the linearization of the non-linear surface condition, it is only valid for semiquantitative purposes. Moreover as the solution is given by the infinite series, inconvenience and inaccuracy unavoidably accompany the numerical computation.

(c) Iswekov's study does not touch our theory; in-

deed, it is an essentially different problem.

(ii) It is clear that the observed diurnal variation at a given locality is not entirely due to the variation of eddy viscosity, i.e., several other causes are associated; therefore a direct identification of the theory with observed facts is very difficult. Moreover the existing statistical records of the diurnal wind-vectors are invalid, because the usual method of the reduction of wind-vector is

Table 4. (Ex. 2)  $V'$  (cm./sec., angle degree.)

	$z=0$	$z=50^m$	$z=100^m$
$\bar{V}$	210 $\angle$ 152°00'	164 $\angle$ 138°00'	127 $\angle$ 123°20'
$n=0$	18.5 $\angle$ 345°50'	14.4 $\angle$ 331°50'	11.2 $\angle$ 317°10'
+1	9.7 $\angle$ 165°40'	4.1 $\angle$ 76°40'	5.5 $\angle$ 17°00'
+2	4.4 $\angle$ 162°50'	2.3 $\angle$ 56°10'	3.9 $\angle$ 0°10'
+3	1.5 $\angle$ 160°10'	1.6 $\angle$ 19°00'	2.8 $\angle$ 346°30'
+4	0.2 $\angle$ 152°00'	1.3 $\angle$ 357°50'	1.8 $\angle$ 337°00'
+5	0.2 $\angle$ 152°00'	0.7 $\angle$ 3°00'	0.9 $\angle$ 337°00'
+6	0.2 $\angle$ 152°00'	0.3 $\angle$ 21°30'	0.6 $\angle$ 340°10'
-1	21.4 $\angle$ 172°00'	11.0 $\angle$ 145°50'	5.2 $\angle$ 89°20'
-2	11.1 $\angle$ 60°50'	11.0 $\angle$ 70°00'	10.4 $\angle$ 71°50'
-3	2.7 $\angle$ 80°30'	2.8 $\angle$ 88°10'	1.3 $\angle$ 94°00'
-4	1.0 $\angle$ 98°50'	1.0 $\angle$ 99°20'	1.0 $\angle$ 100°10'
-5	0.4 $\angle$ 88°30'	0.7 $\angle$ 104°20'	0.4 $\angle$ 105°00'
-6	0.2 $\angle$ 152°00'	0.2 $\angle$ 138°00'	0.1 $\angle$ 123°20'

not suited for testing our theory; although we find that the theoretical results agree to some extent with the well-known facts observed at the

Table 5. (*Ex. 2*)  $V+G$  (m./sec., angle degree.)

Time \ Height	$z=0^m$	$z=50^m$	$z=100^m$
0 <sup>h</sup>	3.22 $\angle 21^{\circ}00'$	4.12 $\angle 18^{\circ}30'$	4.72 $\angle 14^{\circ}10'$
2	3.34 $\angle 19^{\circ}10'$	4.21 $\angle 17^{\circ}00'$	4.78 $\angle 13^{\circ}10'$
4	3.31 $\angle 16^{\circ}20'$	4.04 $\angle 15^{\circ}20'$	4.68 $\angle 12^{\circ}00'$
6	3.28 $\angle 15^{\circ}10'$	3.95 $\angle 14^{\circ}10'$	4.44 $\angle 11^{\circ}50'$
8	3.41 $\angle 15^{\circ}10'$	3.93 $\angle 14^{\circ}20'$	4.35 $\angle 12^{\circ}20'$
10	3.62 $\angle 16^{\circ}10'$	4.04 $\angle 14^{\circ}50'$	4.40 $\angle 13^{\circ}10'$
12	3.78 $\angle 15^{\circ}00'$	4.16 $\angle 14^{\circ}10'$	4.34 $\angle 13^{\circ}30'$
14	3.78 $\angle 14^{\circ}10'$	4.20 $\angle 13^{\circ}40'$	4.57 $\angle 12^{\circ}00'$
16	3.60 $\angle 14^{\circ}00'$	4.14 $\angle 12^{\circ}50'$	4.53 $\angle 12^{\circ}10'$
18	3.32 $\angle 15^{\circ}00'$	3.98 $\angle 13^{\circ}50'$	4.45 $\angle 12^{\circ}00'$
20	3.12 $\angle 17^{\circ}20'$	3.89 $\angle 15^{\circ}30'$	4.43 $\angle 12^{\circ}50'$
22	3.12 $\angle 20^{\circ}10'$	3.96 $\angle 17^{\circ}50'$	4.56 $\angle 14^{\circ}10'$

Eiffel Tower and at Lindenberg.

(iii) The resultant diurnal wind-vector is represented in our theory by a composition of the infinite number of the harmonic components. We see in the numerical examples that the components of the clockwise rotating wind-vectors are predominant in general for the localities in the northern hemisphere. The diurnal and semidiurnal clockwise components which are the most prominent

among them, have the same order in magnitude; and the total amount of the less-prominent components—higher harmonics of the clockwise rotating vectors, and all the components with counterclockwise rotation,—is not negligible. These circumstances combine to give the resultant vector a complex form. Yet, there remains some tendency toward clockwise rotation. This fact has been already found by Sprung and others and has been explained as the result of the deflecting force of the earth's rotation and the frictional force acting near the ground. Our theory explains this physical mechanism more minutely.

(iv) It is worth while to notice the theoretical results of the vertical distribution of wind vectors for every two hours shown in Fig. 2. We shall find that this differs somewhat from the commonly accepted idea. A few meteorologists, assuming a steady condition, consider that any difference from the ordinary spiral shape of the vertical wind vector is due to the eddy viscosity varying as height varies. While our theoretical results also show that even under the assumptions of non-steady condition and constant eddy viscosity, some remarkable differences from the spiral form of the vertical distribution of wind-vector appear on some occasions. The writers of this paper believe that this information must be of some value to those meteorologists who conduct observations by a pilot-balloon or engage in the reduction of those observations.