# Adaptive-Controlled Forecasting for Parts-Oriented Production

## By

# Katsundo HITOMI\*, Toshio HAMADA\* and Kazushige OKUDA\*\*

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#### Abstract

In Parts-Oriented Production Systems, in which multi-products are produced from several multi-parts, the forecast demand for the parts and products is different from each other. The demand for products depends on the consumers' preference, but the demand for parts depends on the demand for all kinds of various products which contain certain kinds of parts. This paper is concerned with the adaptive-controlled forecasting technique for this kind of production system to fit the actual demand for each part. Namely, it is to decrease the rate of modification of production planning for parts and the total stock, and to stabilize the supply of parts for assembling into products.

## 1. Introduction

As the consumers' preference for products becomes diversified, it is necessary for the production manager to produce many kinds of products. Under these circumstances, it is more preferable for the manager to have common parts for many products as inventory in a parts-storage area, and to assemble these parts into finished products as the consumers' needs arise, rather than to have finished products as inventory. This kind of production system is called "Parts-Oriented Production System", abbreviated POPS. This is an important type of modern production system. The advantage of Parts-Oriented Production Systems over Products-Oriented Production Systems is that the manufacturing lead times are much shorter. With this method, an increase of parts inventory reduces a lack of parts that may occur when orders of products are received. However, it is accompanied by an increase in inventory costs. On the other hand, a decrease of parts inventory reduces the inventory cost, but highly increases the

Department of Precision Mechanics
Faculty of Engineering, Kyoto University

 <sup>\*\*</sup> Department of Industrial Engineering, College of Engineering, University of Osaka Prefecture

possibility of a lack of parts. Therefore, it is necessary for the production manager to forecast the amount of parts needed, and then to decide an appropriate level of parts inventory.

In order to forecast the demand for parts, there are two forecasting methods available for the managar. One is to forecast the demand for parts directly by using a time series of the actual demand for parts, which had been observed until that time. The other is to forecast the demand for products by using a time series of the actual demand for products, and then to calculate the amount of parts necessary to assemble that amount of products. For simplicity, the former forecasting method is denoted as  $(\tilde{F})$ , and the latter is denoted as  $(\tilde{F})$ .

Since each kind of product has its own peculiar demand pattern,  $(\tilde{F})$  reflects the demand pattern of each kind of product directly in the demand for parts. At the same time,  $(\tilde{F})$  also reflects the random component of the demand for each kind of product in the demand for parts. On the other hand, if the demand for parts does not fluctuate heavily period by period, or if the demand for one kind of product depends heavily on that for another kind of product,  $(\tilde{F})$  will seem to be better than  $(\tilde{F})$ . Therefore,  $(\tilde{F})$  is sometimes superior and also sometimes inferior to  $(\tilde{F})$ . From this point of view, a method is proposed in this paper to more precisely forecast the demand for parts in the future by considering both the time series of demand for parts and those for products.

#### 2. Parts-Oriented Production Systems

In the factory concerned in this paper, M kinds of products,  $Q_j$   $(j=1, 2, \dots, M)$ , composed of N kinds of parts,  $P_i$   $(i=1, 2, \dots, N)$ , are produced. Let  $e_{i,j}$  denote the amount of  $P_i$  which is needed to produce a unit of  $Q_j$ .  $e_{i,j}$  is a non-negative integer, and  $e_{i,j}=0$  means that product  $Q_j$  does not contain part  $P_i$ . Let  $X_{j,i}$  and  $Y_{i,i}$  be the amounts of demands for product  $Q_j$  and for part  $P_i$  at period t, respectively. It is assumed that  $S_i$  periods are necessary to fabricate or purchase part  $P_i$ , and also that  $L_j$  periods are necessary to assemble product  $Q_j$ . As mentioned briefly in section 1, in POPS, parts are fabricated or purchased in advance and held as inventory. As soon as the order for products is received, the products are assembled from the parts stocked, and shipped. Some kinds of parts are common for several kinds of products. The framework of this system is depicted in Figure 1. The characteristics and effectiveness of this kind of production system were investigated by Hitomi et al.<sup>1)</sup> and Kuriyama et al.<sup>2)</sup> POPS causes a decrease of lead time, a reduction of product inventory, and an increase of service ratio, where service ratio means the percentage of the amount of demand.

To begin with, a special case where  $S_1 = S_2 = \ldots = S_N = S$  and  $L_1 = L_2 = \ldots = L_M = L$ ,



Fig. 1. Framework of Parts-Oriented Production System

is considered. Since the demand for  $Q_j$  at period t is  $X_{j,t}$ ,  $e_{i,j}X_{j,t}$  pieces of  $P_i$  are required at period t-L to satisfy the demand at period t. Therefore, the following relation must be satisfied between the amount of demand for parts and that for products:

$$\mathbf{Y}_{t-L} = \mathbf{E}\mathbf{X}_t \tag{1}$$

where E,  $X_i$ , and  $Y_{i-L}$  are defined as follows:

$$\mathbf{E} = \begin{bmatrix} e_{1,1} & e_{1,2} \cdots & e_{1,M} \\ e_{2,1} & e_{2,2} \cdots & e_{2,M} \\ \vdots & \vdots & \vdots \\ e_{N,1} & e_{N,2} \cdots & e_{N,M} \end{bmatrix}, \quad \mathbf{X}_{t} = \begin{bmatrix} X_{1,t} \\ X_{2,t} \\ \vdots \\ X_{M,t} \end{bmatrix}, \quad \mathbf{Y}_{t-L} = \begin{bmatrix} Y_{1,t-L} \\ Y_{2,t-L} \\ \vdots \\ Y_{N,t-L} \end{bmatrix}.$$
(2)

At period T, the manager wants to forecast the amount of parts required to produce the products demanded at period T+S+L. Because of the necessity of lead time for assembling  $Q_j$ , the actual demand for  $Q_j$  at period T+L must be confirmed at period T. Hence, the information available for the manager at period T is two time series:  $Y_T$ ,  $Y_{T-1}$ ,  $Y_{T-2}$ ,  $\cdots$ , and  $X_{T+L}$ ,  $X_{T+L-1}$ ,  $X_{T+L-2}$ ,  $\cdots$ . These time series satisfy the relation (1).

Let  $\tilde{X}_{T+S+L}(T)$  be the column vector whose ith component  $\tilde{X}_{j,T+S+L}(T)$  is the amount of demand for product  $Q_j$  at period T+S+L, forecast at period T by using  $X_{j,T+L}, X_{j,T+L-1}, X_{j,T+L-2}, \cdots$ . Let  $\tilde{Y}_{T+S}(T)$  be the column vector whose ith component is the amount of part  $P_i$  needed at period T+S in order to assemble  $\hat{X}_{j,T+S+L}(T)$  pieces of product  $Q_j$  required at period T+S+L. Furthermore, let  $\tilde{Y}_{T+S}(T)$  be the column vector whose ith component  $\tilde{Y}_{i,T+S}(T)$  is the amount of demand for part  $P_i$  at period T+S, forecast at period T by using  $Y_{i,T}, Y_{i,T-1}, Y_{i,T-2}, \cdots$ .

Since the fluctuation of demand for each kind of product has its own characteristics, the fluctuation of demand for each kind of part is complicated. The reason is that common parts are included in various kinds of products. Therefore,  $\tilde{Y}_{i,T+s}(T)$  is generated differently from  $\tilde{Y}_{i,T+s}(T)$ . By taking both forecast values,  $\tilde{Y}_{i,T+s}(T)$  and  $\tilde{Y}_{i,T+s}(T)$ , into consideration, the future demand for parts can be forecast more precisely than by considering one of these forecast values. From this point of view, a method of forecasting the amount of parts needed in the future is proposed in this paper, and the effectiveness of this method is discussed by computer simulation.

#### 3. Forecasting Methods for Parts Demand

Two forecasting methods,  $(\mathbf{\tilde{F}})$  and  $(\mathbf{\tilde{F}})$ , for parts demand introduced in section 1 are defined precisely as follows:  $(\mathbf{\tilde{F}})$  is a forecasting method for parts demand in which parts demand at period T+S is forecast at period T, only by using the time series of the actual parts demand which had been observed until period T.  $(\mathbf{\tilde{F}})$  is a forecasting method for parts demand in which the parts demand of period T+S is forecast at period T, only by exploding the forecast amount of the products demand for period T+S+L. In this paper, another effective forecasting method  $(\mathbf{\hat{F}})$  is proposed, in which the trend of parts demand extended over a long period of time is considered. The trend of products demand is reflected as precisely and also as quickly as possible.

Since the fluctuation of demand for each kind of product has its own characteristics, it is preferable for the manager to use a forecasting technique appropriate to each kind of product when he forecasts that product demand in the future. By the same reason, it is preferable for him to use an appropriate forecasting technique for each kind of part when he forecasts the value of  $\tilde{Y}_{i,T+S}(T)$ ,  $(i=1, 2, \dots, N)$ .

Once the values of  $\tilde{X}_{j,T+S+L}(T)$ ,  $(j=1, 2, \dots, M)$  are forecast by using  $X_{j,T+L}$ ,  $X_{j,T+L-1}$ ,  $X_{j,T+L-2}$ ,  $\dots$ , the value of  $\tilde{Y}_{i,T+S}(T)$  is calculated by taking all the values of  $\tilde{X}_{1,T+S+L}(T)$ ,  $\tilde{X}_{2,T+S+L}(T)$ ,  $\dots$ ,  $\tilde{X}_{M,T+S+L}(T)$  into consideration. On the other hand,  $\tilde{Y}_{i,T+S}(T)$  is calculated only by using  $Y_{i,T}$ ,  $Y_{i,T-1}$ ,  $Y_{i,T-2}$ ,  $\dots$ . Therefore, the value of  $\tilde{Y}_{i,T+S}(T)$  is different from that of  $\tilde{Y}_{i,T+S}(T)$ . In order to get a more precise forecast value for parts demand, the following forecasting method ( $\hat{F}$ ) is proposed.

$$(\hat{\mathbf{F}}): \hat{Y}_{T+s}(T) = \Gamma_T \tilde{Y}_{T+s}(t) + (\mathbf{I} - \Gamma_T) \tilde{Y}_{T+s}(T),$$

where  $\hat{Y}_{T+s}(T)$  is a column *N*-vector whose *i*th component  $\hat{Y}_{i,T+s}(T)$  is the demand of  $P_i$  for period T+S, forecast by method ( $\tilde{F}$ ) at period T.  $\Gamma_T$  is a diagonal matrix of order *N* whose *i*th diagonal component is  $\gamma_{i,T}$  and I is an identity matrix of order *N*. The framework of this forecasting method is depicted in Figure 2. The forecasting method ( $\hat{F}$ ) combines two kinds of forecasts for parts demand. The combination of forecasts is proposed by Bates and Granger<sup>3</sup>, and discussed further by Dickinson<sup>4),5</sup>. In this paper, the applicability of the combination of forecasts to parts-oriented production systems is proposed and discussed.

In order to specify  $\gamma_{i,T}$  in  $(\hat{\mathbf{F}})$ , the following two methods are employed. (M-I): If  $Y_{i,T} = \tilde{Y}_{i,T}(T-S) = \tilde{Y}_{i,T}(T-S)$ , then  $\gamma_{i,T} = \gamma_{i,T-1}$ . Otherwise, let  $\beta_{i,T} = |Y_{i,T} - Y_{i,T}|$ .



Fig. 2. Framework of the forecasting method  $(\hat{\mathbf{F}})$ 

 $\dot{Y}_{i,T}(T-S) |/(|Y_{i,T}-\tilde{Y}_{i,T}(T-S)|+|Y_{i,T}-\tilde{Y}_{i,T}(T-S)|)$ . Then,  $\gamma_{i,T} = w_i\beta_{i,T} + (1-w_i)\gamma_{i,T-1}$ , where  $w_i$  is a given positive constant less than 1 and  $\gamma_{i,0} = 0.5$ . This method is the same as (v) of Bates and Granger<sup>3</sup>.

 $(M-II): \quad \text{If} |Y_{i,T} - \tilde{Y}_{i,T}(T-S)| > |Y_{i,T} - \tilde{Y}_{i,T}(Y-S)|, \text{ then } \gamma_{i,T} = \max \{\gamma_{i,T-1} - \delta_0, 0\}. \text{ If } \\ |Y_{i,T} - \tilde{Y}_{i,T}(T-S)| < |Y_{i,T} - \tilde{Y}_{i,T}(T-S)|, \text{ then } \gamma_{i,T} = \min \{\gamma_{i,T-1} + \delta_0, 1\}. \text{ Moreover, if } \\ |Y_{i,T} - \tilde{Y}_{i,T}(T-S)| = |Y_{i,T} - \tilde{Y}_{i,T}(T-S)|, \text{ then } \gamma_{i,T} = \gamma_{i,T-1}, \text{ where } \gamma_{i,0} = 0.5 \text{ and } \delta_0 \text{ is a small positive constant less than } 1.$ 

In these two methods,  $\gamma_{i,T}$  is determined by  $\gamma_{i,T-1}$ ,  $\tilde{Y}_{i,T}(T-S)$ ,  $\tilde{Y}_{i,T}(T-S)$ , and  $Y_{i,T}$  for T>1.  $\gamma_{i,0}$  is any positive value less than 1, and is predetermined at the outset by the manager.

Both (M-I) and (M-II) are proposed from the standpoint that, if the difference between the present value of parts demand observed and the forecast value by using  $(\tilde{F})$  is smaller than that by using  $(\tilde{F})$ , then a new value of  $\gamma_i$  is adaptively made larger for the next period, that is, more weight is assigned to  $(\tilde{F})$ .

In the following sections, the forecasting methods  $(\hat{F})$  by using (M-I) and

(M-II) are denoted by  $(\hat{F}-I)$  and  $(\hat{F}-II)$ , respectively.

#### 4. Simulation

In this section, the characteristics and the efficiency of the forecasting methods proposed in the previous section are investigated by computer simulation. For this purpose, one kind of part  $P_1$  is considered as a representative for five kinds of products,  $Q_j$  (j=1, 2, 3, 4, 5). Then, the amount of this part needed in a future period is forecast. For simplicity, let E=(1, 1, 1, 1, 1), S=3, and L=2. Furthermore, let  $w_i=0.1$ , and  $\delta_0=0.1$ .

As an evaluation criterion for comparing four forecasting methods,  $(\tilde{F})$ ,  $(\tilde{F})$ ,  $(\hat{F}-I)$ , and  $(\hat{F}-II)$ , the mean squared error of the forecasting value from the value of the actual demand is adopted. Let  $MSE_1$ ,  $MSE_2$ ,  $MSE_3$ , and  $MSE_4$  denote the mean squared errors accompanied by  $(\tilde{F})$ ,  $(\tilde{F}-I)$ , and  $(\hat{F}-II)$ , respectively.

Since the demand for each kind of product has its own peculiar pattern of fluctuation, for example, trend, periodicity, etc., it is preferable for the manager to choose and use an appropriate forecasting method in order to forecast the demand for each kind of product. (With respect to various forecasting methods, see, for example, Johnson and Montgomery<sup>6</sup>).) Products demand is forecast by using Trigg and Leachs' adaptive forecasting procedure with a tracking signal<sup>7</sup>). The same procedure is used to forecast parts demand  $\tilde{Y}_{i,T+s}(T)$ .



Fig. 3. Comparison of actual demand and forecast value for model A. (S=3, L=2)

In order to investigate the efficiency of  $(\hat{F})$ , the following two demand models, model A and model B, are introduced:

(Model A): The time horizon is fixed at 47. From period 3 to period 25, the product demand for  $Q_1$  is generated from  $N(\mu_1, \sigma_1^2)$ , and from period 26 to period 49, the product demand for  $Q_1$  is generated from  $N(\mu'_1, \sigma_1^2)$ , where  $N(\mu, \sigma^2)$  means the normal distribution with a mean  $\mu$  and a variance  $\sigma^2$ . The demand for the other four kinds of products  $Q_j(j=2, 3, 4, 5)$  is generated from  $N(\mu_j, \sigma_j^2)$  from period 3 to period 49.

(Model B): The time horizon is also fixed at 49. The product demand for  $Q_1$  is generated similarly as in the case of model A. However, the product demand for  $Q_j$  (j=2, 3, 4, 5) is generated from  $N(\mu_j, \sigma_2^2)$  from period 3 to period 49, except for the (26+j-2)th period when the demand for  $Q_j$  at that period is generated from  $N(\mu'_j, \sigma_2^2)$ .

As a numerical example for model A, the case where  $\mu_1 = 100$ ,  $\mu'_1 = 200$ ,  $\mu_j = 100$ (j=2, 3, 4, 5) and  $\sigma_j^2 = 25$  (j=1, 2, 3, 4, 5) is considered and examined by computer simulation. The data generated from the computer simulation and the forecast amount of demand are depicted in Figure 3. The mean squared errors are:  $MSE_1 = 846.34$ ,  $MSE_2 = 817.09$ ,  $MSE_3 = 798.60$ , and  $MSE_4 = 811.77$ . The computer simulation for model A was repeated forty times. The values of  $MSE_i(i=1, 2, 3, 4)$  and  $MSE_i/MSE_j$ 



| No.      | MSE <sub>1</sub> | MSE <sub>2</sub> | MSE    | MSE4       | $\frac{MSE_3}{MSE_1}$ | MSE <sub>3</sub> /<br>MSE <sub>2</sub> | MSE <sub>4</sub> /<br>MSE <sub>1</sub> | MSE <sub>4</sub> /<br>MSE <sub>2</sub> |
|----------|------------------|------------------|--------|------------|-----------------------|--|--|--|
| 1        | 846.34           | 817.09           | 798.6  | 0 811.77   | 0.9436                | 0.9774                                 | 0.9592                                 | 0.9935                                 |
| 2        | 964.14           | 576.34           | 686.0  | 9 735.01   | 0.7116                | 0.1904                                 | 0.7623                                 | 1.2753                                 |
| 3        | 683.11           | 742.24           | 650.1  | 7 641.39   | 0.9518                | 0.8760                                 | 0.9389                                 | 0.8641                                 |
| . 4      | 793.24           | 555.15           | 619.8  | 7 699.55   | 0.7814                | 1.1166                                 | 0.8819                                 | 1.2601                                 |
| 5        | 1039.41          | 1081.48          | 998.4  | 0 1034.93  | 0.9605                | 0.9232                                 | 0.9957                                 | 0.9570                                 |
| 6        | 790.47           | 532.76           | 615.2  | 0 672.90   | 0.7783                | 1.1547                                 | 0.8513                                 | 1.2631                                 |
| 7        | 1060.95          | 810.34           | 915.1  | 4 972.76   | 0.8626                | 1.1263                                 | 0.9169                                 | 1.2004                                 |
| 8        | 1082.06          | 948.62           | 992.4  | 9 1040.20  | 0.9172                | 1.0462                                 | 0.9613                                 | 1.0965                                 |
| 9        | 604.69           | 586.10           | 567.3  | 2 593.99   | 0.9382                | 0.9680                                 | 0.9823                                 | 1.0135                                 |
| 10       | 870.58           | 942.98           | 882.6  | 3 874.23   | 1.0138                | 0.9360                                 | 1.0042                                 | 0.9271                                 |
| 11       | 1063.83          | 806.05           | 874.7  | 6 951.27   | 0.8223                | 1.0852                                 | 0.8942                                 | 1.1802                                 |
| 12       | 1305.06          | 1095.71          | 1169.7 | 2 1252.76  | 0.8936                | 1.0675                                 | 0.9599                                 | 1.1433                                 |
| 13       | 1009.53          | 944.83           | 946.4  | 8 981.27   | 0.9375                | 1.0017                                 | 0.9720                                 | 1.0386                                 |
| 14       | 541.82           | 491.41           | 480.4  | 3 505.22   | 0.8867                | 0.9776                                 | 0.9324                                 | 1.0281                                 |
| 15       | 1157.25          | 688.25           | 864.6  | 9 978.65   | 0.7472                | 1.2564                                 | 0.8457                                 | 1.4219                                 |
| 16       | 856.34           | 817.09           | 798.6  | 0 811.77   | 0.9436                | 0.9774                                 | 0.9592                                 | 0.9935                                 |
| 17       | 820.87           | 591.08           | 665.7  | 4 742.99   | 0.8110                | 1.1263                                 | 0.9051                                 | 1.2570                                 |
| 18       | 1035.14          | 978.38           | 995.0  | 5 1015.43  | 0.9613                | 1.0170                                 | 0.9810                                 | 1.0379                                 |
| 19       | 768.08           | 627.53           | 655.2  | 3 672.68   | 0.8531                | 1.0441                                 | 0.8758                                 | 1.0720                                 |
| 20       | 804.60           | 637.01           | 685.1  | 5 752.21   | 0.8515                | 1.0756                                 | 0.9349                                 | 1.1808                                 |
| 21       | 865.07           | 659.61           | 714.9  | 9 760.72   | 0.8265                | 1.0840                                 | 0.8794                                 | 1.1533                                 |
| 22       | 934.25           | 862.37           | 887.1  | 3 910.26   | 0.9496                | 1.0287                                 | 0.9743                                 | 1.0555                                 |
| 23       | 967.25           | 852.14           | 871.1  | 6 911.76   | 0.9007                | 1.0223                                 | 0.9426                                 | 1.0700                                 |
| 24       | 888.14           | 931.89           | 879.2  | 1 900.96   | 0.9900                | 0.9435                                 | 1.0144                                 | 0.9668                                 |
| 25       | 1050.50          | 904.38           | 948.8  | 3 1008.84  | 0.9032                | 1.0491                                 | 0.9603                                 | 1.1155                                 |
| 26       | 762.99           | 593.38           | 643.2  | 1 676.54   | 0.8430                | 1.0840                                 | 0.8867                                 | 1.1401                                 |
| 27       | 779.16           | 686.22           | 710.0  | 7 752.07   | 0.9113                | 1.0348                                 | 0.9652                                 | 1.0960                                 |
| 28       | 980. 29          | 674.52           | 808.0  | 8 971.46   | 0.8243                | 1.1980                                 | 0.9910                                 | 1.4402                                 |
| 29       | 1204.40          | 731.03           | 849.5  | 0 906.28   | 0.7053                | 1.1621                                 | 0.7525                                 | 1.2397                                 |
| 30       | 930. 71          | 606.48           | 750.2  | 2 822.34   | 0.8061                | 1.2370                                 | 0.8836                                 | 1.3559                                 |
| 31       | 784.13           | 564.97           | 607.4  | 0 694.88   | 0.7746                | 1.0751                                 | 0.8862                                 | 1.2300                                 |
| 32       | 903.96           | 842.75           | 849.1  | 9 860.51   | 0.9383                | 1.0065                                 | 0.9519                                 | 1.0211                                 |
| 33       | 931.62           | 527.28           | 653.3  | 3 825.86   | 0.7013                | 1,2391                                 | 0.8865                                 | 1.5663                                 |
| 34<br>25 | 725 50           | 6/1.91<br>509.97 | 690.4  | 0 000,00   | 0.8520                | 1.0275                                 | 0.8130                                 | 1 0624                                 |
| 30<br>36 | 702 47           | 396.37<br>819.20 | 752.8  | 7 748.41   | 1.0718                | 0.9109                                 | 1,0654                                 | 0.9136                                 |
| 37       | 719.91           | 522.97           | 575.8  | 1 666.33   | 0. 7998               | 1.1010                                 | 0.9256                                 | 1.2714                                 |
| 38       | 588.20           | 551.01           | 509.1  | 5 571.17   | 0.8656                | 0.9240                                 | 0.9710                                 | 1.0366                                 |
| 39       | 1096.84          | 985.46           | 953.8  | 1 1083. 59 | 0.8696                | 0.9679                                 | 0.9879                                 | 1.0996                                 |
| 40       | 878.26           | 643.06           | 719.4  | 7 713.35   | 0.8192                | 1.1188                                 | 0.8122                                 | 1.1093                                 |
|          | <u>.</u>         | ·····            | ·      | Total      | 34. 7830              | 42.2271                                | 36. 9288                               | 45. 1304                               |
|          |                  |                  |        | Mean       | 0.8696                | 1,0557                                 | 0, 9232                                | 1.1283                                 |

Table 1. Results of computer simulation for model A.

| No.      | MSE <sub>1</sub> | MSE <sub>2</sub> | MSE     | MSE4                   | MSE <sub>3</sub> /<br>MSE <sub>1</sub> | $\frac{MSE_3}{MSE_2}$ | MSE <sub>4</sub> /<br>MSE <sub>1</sub> | MSE <sub>4</sub> /<br>MSE <sub>2</sub> |
|----------|------------------|------------------|---------|------------------------|--|-----------------------|--|--|
| 1        | 2270.04          | 2319.97          | 1997.7  | 5 2140.58              | 0.8801                                 | 0.8611                | 0.9430                                 | 0.9227                                 |
| 2        | 3323.98          | 2041.71          | 2132.7  | 5 1957.92              | 0.6416                                 | 1.0446                | 0.5890                                 | 0.9590                                 |
| 3        | 3008.59          | 2575.20          | 2272.9  | 7 2263.44              | 0.7555                                 | 0.8826                | 0.7523                                 | 0.8789                                 |
| 4        | 2681.31          | 2202.13          | 2058.2  | 4 2059.94              | 0.7676                                 | 0.9347                | 0.7683                                 | 0.9354                                 |
| 5        | 2395.15          | 2032.09          | 1924.5  | 1 2170.79              | 0.8035                                 | 0.9471                | 0.9063                                 | 1.0683                                 |
| 6        | 3112.04          | 2682.62          | 2461.7  | 6 3023.10              | 0.7910                                 | 0.9177                | 0.9714                                 | 1.1269                                 |
| 7        | 2344. 36         | 2530.42          | 2013.9  | 9 2130.98              | 0.8591                                 | 0.7959                | 0.9090                                 | 0.8421                                 |
| 8        | 2331.42          | 2415.95          | 2103.3  | 4 2102.92              | 0.9022                                 | 0.8706                | 0.9020                                 | 0.8704                                 |
| 9        | 1893. 51         | 1842.68          | 1732.9  | 1 1750.79              | 0.9152                                 | 0.9404                | 0.9246                                 | 0.9501                                 |
| 10       | 2545. 12         | 2219.29          | 2183.8  | 3 2305.66              | 0.8580                                 | 0.9840                | 0.9059                                 | 1.0389                                 |
| 11       | 3123.85          | 2258.94          | 2314.6  | 1 2608.90              | 0.7409                                 | 1.0246                | 0.8352                                 | 1.1549                                 |
| 12       | 2275.02          | 2063.91          | 1885.4  | 7 2009.25              | 0.8288                                 | 0.9135                | 0.8832                                 | 0.9735                                 |
| 13       | 2363. 54         | 2138.70          | 1976.5  | 5 1965.10              | 0.8363                                 | 0.9242                | 0.8314                                 | 0.9188                                 |
| 14       | 2847.44          | 2275.60          | 2155.7  | 2 2225.90              | 0.7571                                 | 0.9473                | 0.7817                                 | 0.9782                                 |
| 15       | 2927.29          | 2459.85          | 2226.7  | 0 2447.28              | 0.7607                                 | 0.9052                | 0.8360                                 | 0. 9949                                |
| 16       | 2270.04          | 2319.97          | 1997.7  | 5 2140.58              | 0.8801                                 | 0.8611                | 0.9430                                 | 0.9227                                 |
| 17       | 2087.39          | 2117.76          | 1679.1  | 3 2915.89              | 0.8044                                 | 0.7929                | 0.9657                                 | 0.9519                                 |
| 18       | 2258.40          | 1920.06          | 1866. 1 | 8 2060.77              | 0.8263                                 | 0.9719                | 0.9125                                 | 1.0733                                 |
| 19       | 2664.26          | 2986.50          | 2328.8  | 8 2564.97              | 0.8741                                 | 0.7798                | 0.9627                                 | 0.8589                                 |
| 20       | 2113.83          | 1767.41          | 1655.3  | 8 1732.23              | 0. 7831                                | 0.9366                | 0.8195                                 | 0.9801                                 |
| 21       | 2220. 59         | 2372.29          | 1765.0  | 5 1925. 23             | 0.7949                                 | 0.7440                | 0.8670                                 | 0.8116                                 |
| 22       | 2014.18          | 2046.27          | 1849.1  | 5 1912.33              | 0. 9181                                | 0.9037                | 0.9494                                 | 0,9345                                 |
| 23       | 2479.85          | 2253.43          | 2014. 1 | 6 2387.02              | 0.8122                                 | 0.8938                | 0.9626                                 | 1.0593                                 |
| 24       | 1650.91          | 1511.47          | 1372.9  | 7 1439.87              | 0.8316                                 | 0.9084                | 0.8733                                 | 0.9526                                 |
| 25       | 2162.27          | 2209.72          | 1887.6  | 1 2038.22              | 0.8730                                 | 0.8542                | 0.9426                                 | 0. 9224                                |
| 26       | 1993.80          | 1964.35          | 1628.5  | 3 1807.63              | 0.8168                                 | 0.8290                | 0.9066                                 | 0.9202                                 |
| 27       | 2485.15          | 2503.43          | 2299.2  | 3 2288.12              | 0.9252                                 | 0.9184                | 0.9207                                 | 0.9140                                 |
| 28       | 2569.49          | 2594.69          | 2189.5  | 6 2463.35              | 0.8521                                 | 0.8436                | 0.9587                                 | 0.9494                                 |
| 29       | 3133.90          | 1978.18          | 1927.2  | 3 1875.32              | 0.6150                                 | 0.9742                | 0.5984                                 | 0.9480                                 |
| 30       | 1960.85          | 1612.02          | 1426.9  | 4 1619.07              | 0.7277                                 | 0.8852                | 0.8257                                 | 1.0044                                 |
| 31       | 1758.92          | 2458.72          | 1436.5  | 2 1664.78              | 0.8167                                 | 0.5843                | 0.9465                                 | 0.6771                                 |
| 32       | 2062.12          | 1844.13          | 1696.1  | 1 1799.09              | 0.8225                                 | 0.9197                | 0.8724                                 | 0.9756                                 |
| 33       | 2162.10          | 2107.49          | 1589.1  | 0 2076.31              | 0.7350                                 | 0.7540                | 0.9603                                 | 0.9852                                 |
| 34<br>25 | 1930.73          | 2226.35          | 1080.6  | 8 1636-10<br>A 9900-81 | 0.8162                                 | 0.7100                | 0.8448                                 | 0.7349                                 |
| 36       | 1473.11          | 2170.10          | 1629.3  | 4 2299.31<br>3 1692.91 | 1 1060                                 | 0.0234                | 1 1017                                 | 0. 6920                                |
| 37       | 2163.27          | 1543.67          | 1368.5  | 6 1385.47              | 0, 6326                                | 0.8866                | 0.6405                                 | 0. 8975                                |
| 38       | 2715.90          | 2996.14          | 2165.2  | 5 2246.21              | 0.7973                                 | 0. 7227               | 0.8271                                 | 0. 7497                                |
| 39       | 2738.17          | 4149.38          | 2461.7  | 4 2727.99              | 0.8990                                 | 0. 5933               | 1.0127                                 | 0. 6683                                |
| 40       | 2303.63          | 2454.81          | 1959.3  | 5 1980.60              | 0.8506                                 | 0. 7982               | 0.8598                                 | 0. 8068                                |
|          |                  |                  |         | Total                  | 32.8015                                | 34. 5498              | 35. 1809                               | 36.9678                                |
|          |                  |                  |         | Mean                   | 0. 8200                                | 0.8637                | 0.8795                                 | 0.9242                                 |

Table 2. Results of computer simulation for model B.

(i=3, 4; j=1, 2) are tabulated in Table 1. It is easily found from this table that both  $(\hat{F}-I)$  and  $(\hat{F}-II)$  are superior to  $(\tilde{F})$ , but in some cases superior and in other cases inferior to  $(\tilde{F})$ .

As a numerical example for model B, the case where  $\mu_1 = 100$ ,  $\mu_2 = 200$ ,  $\mu_3 = 220$ ,  $\mu_4 = 250$ ,  $\mu_5 = 210$ ,  $\mu'_1 = 200$ ,  $\mu'_2 = 100$ ,  $\mu'_3 = 120$ ,  $\mu'_4 = 150$ ,  $\mu'_6 = 110$ , and  $\sigma_j^2 = 100$  (j=1, 2, 3, 4, 5) is considered and examined by computer simulation. The data generated from the computer simulation and the forecast amount of demand are depicted in Figure 4. The mean squared errors are:  $MSE_1 = 2270.04$ ,  $MSE_2 = 2319.97$ ,  $MSE_3 = 1997.75$ , and  $MSE_4 = 2140.58$ . The computer simulation for model B was also repeated forty times. The values of  $MSE_i(i=1, 2, 3, 4)$  and  $MSE_i/MSE_j(i=3, 4; j=1, 2)$  are tabulated in Table 2. Both ( $\hat{F}$ -I) and ( $\hat{F}$ -II) are usually superior to ( $\hat{F}$ ) and ( $\hat{F}$ ). About 10 to 15 percent of the average of MSE is reduced.

It is concluded from these two kinds of experiments that the forecasting method  $(\hat{F}-I)$  is effective in forecasting the parts demand for parts-oriented production.

#### 5. Effects of Lead Time

In section 3, it was assumed that the lead time to fabricate products from parts is the same for all products, and that to produce parts is fixed for all parts. Since this assumption is not always satisfied in actual cases, in this section it is removed, while keeping the forecasting method described in the previous section.

The matrix  $E_r$  is redefined as a generalized form of E introduced in section 2 as follows:

$$\mathbf{E}_{\tau} = \begin{bmatrix} e_{1,1,\tau} & e_{1,2,\tau} & \cdots & e_{1,M,\tau} \\ e_{2,1,\tau} & e_{2,2,\tau} & \cdots & e_{2,M,\tau} \\ \vdots & \vdots & \vdots \\ e_{N,1,\tau} & e_{N,2,\tau} & \cdots & e_{N,M,\tau} \end{bmatrix} \text{ for } \tau = 1, 2, \cdots, L_{max},$$

where  $L_{\max} = \max_{\substack{1 \le j \le M}} L_j$  and  $e_{i,j,\tau}$  pieces of parts are needed to assemble a piece of  $Q_j$ , when  $\tau$  periods are required to assemble product  $Q_j$ . Therefore, if  $\tau_0$  periods are needed to assemble product  $Q_j$ , then  $e_{i,j,\tau} = 0$  for any  $\tau \neq \tau_0$   $(i=1, 2, \dots, N; j=1, 2, \dots, M)$ . By using the above matrix, the following relation is satisfied between the parts demand and the products demand:

$$\mathbf{Y}_T = \sum_{r=1}^{L_{max}} \mathbf{E}_r \mathbf{X}_{T+r}$$

This is a generalized form of Equation (1). In this case, since the forecast of the cumulative amount of parts demand at period T is affected by the forecast of each kind of product, the forecasting procedure becomes complex.

It is not necessary to consider the case where the assumption  $S_1 = S_2 = \cdots = S_n = S$ 

proposed in section 2 is not satisfied, because the purpose of this paper is to forecast the future demand for each kind of part.

## 6. Conclusion

In this paper, forecasting methods which combine two kinds of forecasts for parts demand are proposed for the Parts-Oriented Production System. The effectiveness of the proposed methods was compared with that of conventional forecasting methods. It was found that the proposed forecasting methods are not inferior to, but according to circumstances, are superior to the conventional forecasting methods. The selection of the forecasting method depends heavily on what kind of Parts-Oriented Production System is concerned with in reality, and also on what kinds of parts are common for a variety of products.

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