

## Acoustic Converting Efficiency and Anisotropic Nature of Wood

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It is accepted that both the acoustic converting efficiency and the degree of anisotropy of wood are important factors for the sound board of musical instruments<sup>1,2)</sup>. In this paper, the relationship between these factors were clarified experimentally and theoretically. The specific dynamic Young's modulus ( $E'/\rho$ ) and the loss tangent ( $\tan \delta_L$ ) in the longitudinal (L) direction, and the dynamic shear modulus ( $G'$ ) and the loss tangent ( $\tan \delta_S$ ) in the LT plane (T : tangential direction) for 101 kinds of woods were measured by using flexural and torsional vibration methods.

There was a negative correlation between  $E'/\rho$  and  $\tan \delta_L$  as shown in Fig. 1. This fact indicates that smaller mean microfibril angles give larger  $E'/\rho$  and lower  $\tan \delta_L$  values<sup>3)</sup>. Fig. 2 shows the relationships between the ratio of loss tangents ( $\tan \delta_S/\tan \delta_L$ ) and that of elastic moduli ( $E'/G'$ ). Relatively large  $E'/G'$  and  $\tan \delta_S/\tan \delta_L$  values of wood reflect its anisotropic nature. Fig. 3 shows the relationship between ( $E'/G'$ ) ( $\tan \delta_S/\tan \delta_L$ ) and  $\sqrt{E'/\rho}/\tan \delta_L$ . The former reflects the degree of anisotropy and the latter relates to the acoustic converting efficiency ( $\sqrt{E'/\rho^3}/\tan \delta_L$ ). There was a positive correlation between them. These acoustic properties can be calculated by using a uniaxial cell wall model in which amorphous isotropic matrix is disposed in parallel along the axis of cellulosic fibrils inclining at  $\theta$  to the L direction of wood<sup>4)</sup>. The  $E'/\rho$ ,  $\tan \delta_L$ ,  $G'/\rho$  and  $\tan \delta_S$  can be expressed by

$$\frac{E'}{\rho} \approx \frac{\nu}{\rho_w} \left( \frac{1}{E_{w1}'} + \frac{\theta^2}{G_{w12}'} \right)^{-1}, \quad \tan \delta_L \approx \left( \frac{E_{w1}''}{E_{w1}'^2} + \frac{G_{w12}'' \theta^2}{G_{w12}'^2} \right) \left( \frac{1}{E_{w1}'} + \frac{\theta^2}{G_{w12}'} \right)^{-1},$$

$$\frac{G'}{\rho} \approx \frac{\nu}{\rho_w} \left( \frac{\sin^2 2\theta}{E_{w1}'} + \frac{\cos^2 2\theta}{G_{w12}'} \right)^{-1}$$

and

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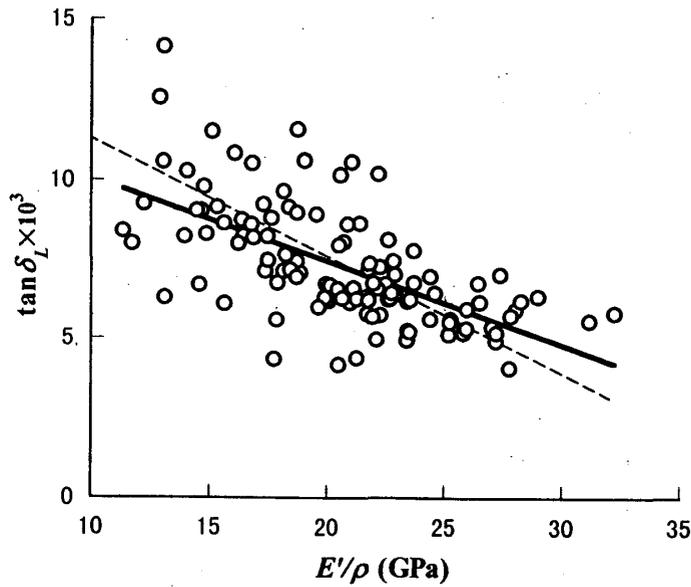


Fig. 1. The relationship between the loss tangent ( $\tan \delta_L$ ) and the specific dynamic Young's modulus ( $E'/\rho$ ) in the longitudinal direction of wood. Note: O, Experimental values; solid line, the regression line of experimental values ( $r = -0.632$ ); dotted line, calculated values.

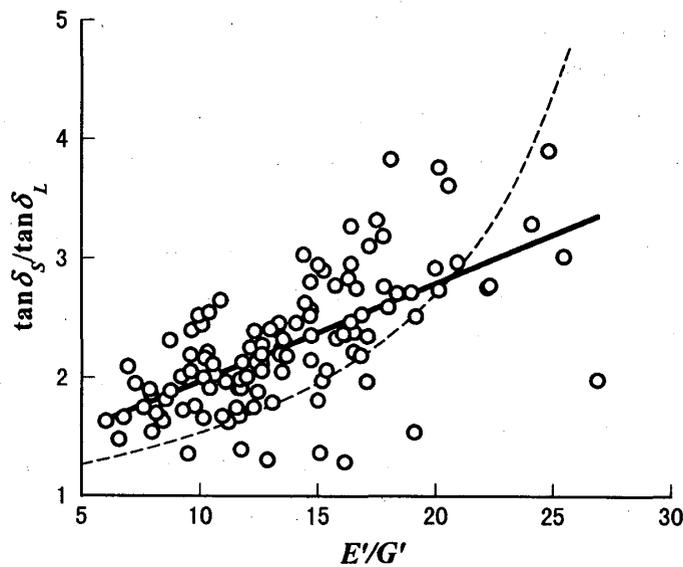


Fig. 2. The relationship between the ratio of loss tangent ( $\tan \delta_S / \tan \delta_L$ ) and that of elastic moduli ( $E'/G'$ ) of wood. Note: O, Experimental values; solid line, the regression line of experimental values ( $r = 0.648$ ); broken line, calculated values.

$$\tan \delta_S \approx \left( \frac{E_{w2}'' \sin^2 2\theta}{E_{w2}'^2} + \frac{G_{w12}'' \cos^2 2\theta}{G_{w12}'^2} \right) \left( \frac{\sin^2 2\theta}{E_{w2}'} + \frac{\cos^2 2\theta}{G_{w12}'} \right)^{-1},$$

where  $\nu$  is the volume fraction of  $S_2$  layer,  $E_{w1}$  and  $E_{w2}$  are the Young's moduli of the cell wall in the parallel (1) and perpendicular (2) to the axis of fibrils,  $G_{w12}$  is the shear modulus

of

the

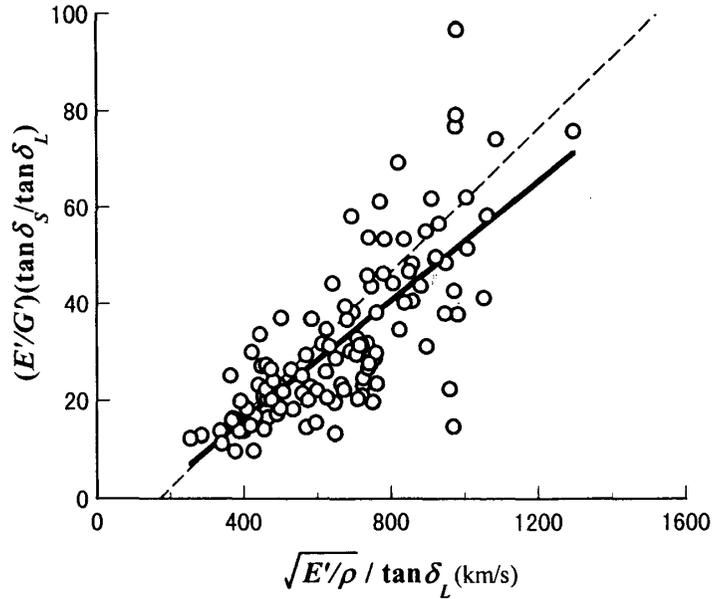


Fig. 3. The relationship between the  $(E'/G')(\tan \delta_s / \tan \delta_L)$  and the sound velocity divided by the loss tangent  $(\sqrt{E'/\rho} / \tan \delta_L)$  of wood. Note: O, Experimental values; line, the regression line of experimental values ( $r=0.752$ ) broken line, calculated values.

cell wall in the 1–2 plane,  $\rho_w$  is the density of the cell wall, respectively. Single and double primes indicate the dynamic modulus and loss modulus, respectively. According to the law of mixtures,  $E_{w1}'$ ,  $E_{w1}''$ ,  $E_{w2}'$ ,  $E_{w2}''$ ,  $G_{w12}'$  and  $G_{w12}''$  can be expressed by

$$E_{w1}' = \varphi E_{f1} + (1 - \varphi) E_m, \quad E_{w1}'' = (1 - \varphi) E_m'' = (1 - \varphi) E_m' \tan \delta_m,$$

$$E_{w2}' \approx E_m' \left( 1 + \frac{\varphi}{1 - \sqrt{\varphi}} \right), \quad E_{w2}'' \approx E_m' \left( 1 + \frac{\varphi}{1 - \sqrt{\varphi}} \right) \tan \delta_m,$$

$$G_{w12}' \approx G_m' \left( 1 + \frac{\varphi}{1 - \sqrt{\varphi}} \right) \quad \text{and} \quad G_{w12}'' \approx G_m' \left( 1 + \frac{\varphi}{1 - \sqrt{\varphi}} \right) \tan \delta_m,$$

where  $E_{f1}$  is the Young's modulus of fibrils along the axis,  $\varphi$  is the volume fraction of fibrils,  $E_m'$ ,  $G_m'$  and  $\tan \delta_m$  are the Young's modulus, shear modulus and loss tangent of the matrix, respectively. Values of  $\nu=0.84$ ,  $E_{f1}=134$  GPa,  $\varphi=0.5$ ,  $E_m=2$  GPa,  $G_m=0.77$  GPa, and  $\tan \delta_m=0.015$  were adopted. Dotted lines in Figs. 1–3 show the calculated values. The calculated values in Fig. 3 predicted that smaller microfibril angles give higher values of acoustic converting efficiency as well as higher degrees of anisotropy.

## References

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