

PAPER

New Stochastic Algorithm for Optimization of Both Side Lobes and Grating Lobes in Large Antenna Arrays for MPT

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SUMMARY The concept of placing enormous Solar Power Satellite (SPS) systems in space represents one of a handful of new technological options that might provide large scale, environmentally clean base load power to terrestrial markets. Recent advances in space exploration have shown a great need for antennas with high resolution, high gain and low side lobe level (SLL). The last characteristic is of paramount importance especially for the Microwave Power Transmission (MPT) in order to achieve higher transmitting efficiency (TE) and higher beam collection efficiency (BCE). In order to achieve low side lobe levels, statistical methods play an important role. Various interesting properties of a large antenna arrays with randomly, uniformly and combined spacing of elements have been studied, especially the relationship between the required number of elements and their appropriate spacing from one viewpoint and the desired SLL, the aperture dimension, the beamwidth and TE from the other. We propose a new unified approach in searching for reducing SLL by exploiting the interaction of deterministic and stochastic workspaces of proposed algorithms. Our models indicate the side lobe levels in a large area around the main beam and strongly reduce SLL in the entire visible range. A new concept of designing a large antenna array system is proposed. Our theoretic study and simulation results clarify how to deal with the problems of side lobes in designing a large antenna array, which seems to be an important step toward the realization of future SPS/MPT systems.

key words: microwave power transmission, large antenna array, uniform spacing, random spacing, spatial and amplitude tapering, side lobe level, grating lobes, workspace, transmitting efficiency, beam collection efficiency

1. Introduction

In the 1980s and 1990s in Japan, we have performed large investigations on Solar Power Satellites (SPS) and wireless power transmission via microwave (MPT), related by the abbreviations MINIX, ISY-METS, MILAX, SPORTS and SPIRITZ [1]. In such way, the center of MPT technologies research shifted from USA to Japan. The SPS is a huge solar power station in space, which transmits electric power via microwave. The SPS requires a huge phased array antenna with low side lobe levels (SLL) in order to achieve higher transmitting efficiency (TE) and higher beam collection efficiency (BCE).

In his fundamental paper [2] T. Taylor studied the

mathematical relationships involved in the radiation calculation of the line source from the point of view of function theory. Antenna design technique permits the other – than – uniform distributions of the field and in [2] has been investigated how to choose this distribution function to give a radiation pattern with prescribed properties such as, for example, narrow beamwidth of the main lobe and low side lobes. In this original paper was documented the relationships between aperture edge behavior, far side lobes, and array pattern zero locations. His analysis and insights led to a most practical technique for the synthesis of low-sidelobe beams.

A number of applications require a narrow scanned beam, but not commensurably high antenna gain. Since the array beamwidth is related to the largest dimension of the aperture, it is possible to remove many of the elements (or to “thin” an array) without significantly changing its beamwidth. For small or moderate arrays, it can be convenient to formulate the thinning procedure as a side lobe minimization problem (see [3]–[6]). [3] proposes a method that can reduce both the quantities of elements required for a given size aperture and the number of different types of transmitters which would be necessary in an array using an illumination taper. In [4] a linear array with general arbitrarily distributed elements is discussed. A matrix relationship is found between the elements of the array and its far-zone pattern. In [5] general analytical expressions are presented for unequally spaced arrays. These relations allow for the analysis of the non-uniformly spaced array in terms of its equivalent uniformly spaced array. Some equivalence is made between the amplitude and spatial variation in the uniformly and non-uniformly spaced array. An array with monotonically increasing inter element spacing is presented as an example of the theory. In [6] a perturbation procedure for reducing the SL level of discrete linear arrays with uniform amplitude excitation by using non-uniform element spacing is presented. All these procedures [3]–[6] do control both peak and average SLL, but are numerically difficult to implement for large antenna arrays.

The variety of statistical procedures for array thinning exert direct control primarily on the average SLL and can produce peak side lobes for larger than the average level. A paper by Steinberg [7] compares the peak side lobes of 70 algorithmically designed aperiodic arrays with those of 170 random arrays. Both distributions are found to be nearly log-normal. The study shows that most techniques lead to

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very similar average levels.

The statistical method of Skolnik et al. [8] is straightforward to implement for large antenna arrays. The probability density of elements located within the aperture is made proportional to the amplitude of the aperture illumination of a conventional “filled” array. The selection of the element locations is performed statistically by choosing element weights as unity or zero with probabilities proportional to the filled-array taper. This procedure is readily applicable to the design of large antenna arrays. However it is not optimum and in that it does not ensure that peak side lobes are maintained below a given level. In [9] a thinning method is presented to realize the desired aperture distribution in a planar array antenna with elements fixed on an array lattice. In this method elements to be excited are determined by quantizing cumulative weights which are calculated from the desired aperture distribution. In [10] one investigates the use of statistical thinning and quantized element weights to produce low side lobe pattern using large circular array apertures. The last two papers develop further Skolnik et al. method [8] by using discrete, quantized output power levels for the array instead of a continuous taper.

In [11] the effects on radiation pattern when N pairs of symmetrically located radiators are removed at random from a large $(2N_0 + 1)$ -element linear array are studied as a statistical problem. The general analysis is valid for arrays with an arbitrary amplitude distribution which is symmetrical with respect to the center element.

The series of papers of Y. Lo [12]–[16] and [17] and especially the pioneering and fundamental paper [13] present probabilistic study of thinned antenna arrays. Lo addresses the peak-sidelobe issue and shows that a statistical description of these side lobes is possible and yields useful bounds for array design. In [17] mutual coupling effects in phased arrays with randomly located elements are studied.

Taking into account this background we can draw the following conclusion:

1. For conventionally designed arrays where all elements are spaced uniformly, there exists an upper limit to the spacing if the grating lobes are not permitted to appear in the visible region.
2. Deterministic non-uniformly spaced algorithms are numerically difficult to implement for large antenna arrays.
3. Randomly spaced algorithms (the concept of “thin” arrays) are easier to implement, but need of further study in order to determine their merits and drawbacks.

In this paper we develop further the existing algorithms and our previous research [18]–[21] and [22] proposing a new techniques to deal with side lobes and grating lobes.

2. Randomly and Uniformly Spaced Arrays

Consider a linear array along the X axis in Cartesian coordinate system and suppose we are given $N + 1$ equally excited antenna elements by isotropic radiation to be placed at random within an aperture defined by $|X| \leq a/2$ in wavelength,

in accordance with a common probability density function (pdf) $f(x)$.

Assume that the random positions $\{X_n\}$ are independent. Then for each sample vector $\{X_n\}$, $X_n \in R^{N+1}$, there is a sample radiation pattern function given by the magnitude of [13]

$$P(u) = \frac{1}{N+1} \sum_{n=-N/2}^{N/2} \exp(ju x_n) \quad (1a)$$

$$P(\theta) = \frac{1}{N+1} \sum_{n=-N/2}^{N/2} \exp\{j2\pi(\sin\theta - \sin\alpha)X_n\} \quad (1b)$$

θ - the observation angle measured from the normal to the array axis

α - the scan angle measured from the normal to the array axis

$u = a\pi(\sin\theta - \sin\alpha)$ - the observation angle parameter

$\{x_n = 2X_n/a\}$ - normalized workspace

$a = Nd_x$ - the aperture, measured in wavelength

We can determine the array factor (AF) $= |P(u)|^2$ or $|P(\theta)|^2$ as random functions. In (1) if $\{X_n\}$ is considered as positions of conventional uniform spacing $\{X_n = nd_x\}$ the model is automatically transformed in the deterministic one — see (2).

$$\begin{aligned} P(\theta) &= \frac{1}{N+1} \sum_{n=-N/2}^{N/2} \exp\{j2\pi(\sin\theta - \sin\alpha)nd_x\} \\ &= \frac{1}{N+1} \sum_{n=-N/2}^{N/2} \exp(j\psi_n) \end{aligned} \quad (2)$$

where $\psi_n = \frac{2\pi}{\lambda}(\sin\theta - \sin\alpha)nd_x$ and normalized work space equals to $x_n = 2nd_x/N$. We can determine the array factor $AF = |P(\theta)|^2$ as periodic function [23], [24].

A linear array with its peak at α can also have other peak values subject to the choice of spacing d_x . This ambiguity is apparent, since the summation also has a peak whenever the exponent is some multiple of 2π or

$$\frac{2\pi}{\lambda}(\sin\theta - \sin\alpha)d_x = 2\pi p, \quad p = \pm(1, 2, \dots) \quad (3)$$

Such peaks are called grating lobes and are shown from the above to occur at angles θ_p such that

$$\sin\theta_p = \sin\alpha + \frac{p\lambda}{d_x}, \quad p = \pm(1, 2, \dots) \quad (4)$$

for values of p that define an angle with a real sine ($|\sin\theta_p| \leq 1$). This implies that the maximum element spacing for an array scanned to a given angle α at frequency f is $\lambda/2$.

The model (1) is pure stochastic model and was first investigated by Y.T. Lo [13] and will be coded as RA (random array). The model (2) is well known deterministic model of uniform spacing and will be coded as UA (uniform array). Let's summarize the Lo's result [13], [23], who was

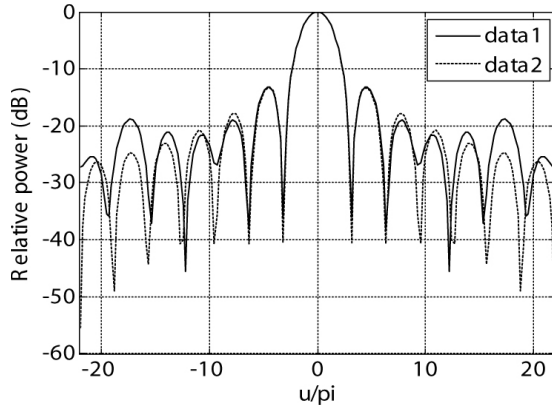


Fig. 1 Radiation characteristics of RA (data1) and UA (data2) with uniform excitation, $N=1000$, average spacing $d_{av} = 2\lambda$, $\theta \in [-0.2^\circ, 0.2^\circ]$.

found the distribution of maximum of SLL outside of the main beam region and that at any “ u ” the probability of antenna response being less than any level r is given by

$$\Pr\{|P(u)| < r, \text{ all } u : \delta < |u| < 2\pi a\} \approx \left[1 - \exp^{-Nr^2}\right]^{[4a]} \quad (5)$$

where δ is the first positive zero of characteristic function

$$\varphi(u) = E\{\exp(jux)\} = \int_{-\infty}^{\infty} f(x) \exp(jux) dx \quad (6)$$

and the bracket $[4a]$ is the integer part of $4a$. This is a chi-squared distribution with two degrees of freedom.

This expression gives the number of elements required to achieve the desired SLL (maximum, not average) with predetermined confident probability of success such as 0.9, 0.95, etc.

Equation (6) is important. It is seen that the mean pattern is identical to the pattern which would be obtained by taking $f(x)$ as a continuous aperture excitation.

Lo shows [23] that outside of the main beam region, the variances of the real and imaginary parts of the pattern are equal and approximately given by $1/2N$, independent of the probability density function $f(x)$. This significant conclusion implies that although the pattern behavior in the main beam region is determined by $f(x)$, outside of the main beam area the variances are determined only by N , the number of elements, not the probability density function $f(x)$. Therefore, in many cases (unless the near-in SLL is of interest), the uniform pdf for $f(x)$ may have advantage to us to maintain a narrow beam. Keeping these suggestions in mind we will search solution of our problem in the strategy of uniform pdf and different non uniform excitation (illumination) functions.

Let's compare this stochastic model RA with the deterministic model of conventional uniform spacing UA model in the near side lobe region — Fig. 1 and in the entire visible range — Fig. 2.

One can make some important conclusions. In the entire visible range there is no grating lobe for RA. However,

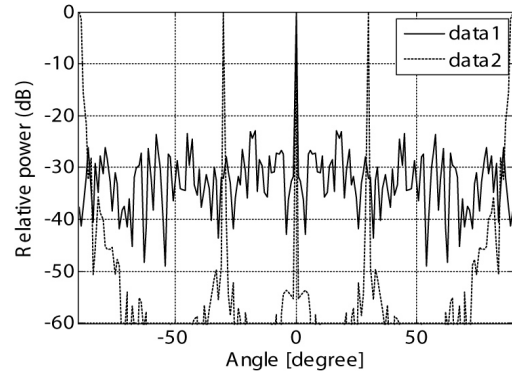


Fig. 2 Radiation characteristics of RA (data1) and UA (data2) with uniform excitation, $N=1000$, average spacing $d_{av} = 2\lambda$, $\theta \in [-90^\circ, 90^\circ]$.

the SLL is sufficiently high for random spacing of elements in comparison with uniform spacing — UA model. When number of elements increases SLL decreases but remains still high for MPT as will be seen further. The SLL of the MPT must be decreased in order to suppress interferences to existent wireless systems. There is an estimation of interference from the MPT in the SPS to the existent wireless systems [25]. However, at the present moment, we can not decide necessary SLL of the MPT to coexistence with the existent wireless systems because conditions of the MPT and the existent wireless systems will be changed.

Second, From Fig. 1 we can see that the near SLL around the main beam is also sufficiently high for both RA and UA models. Therefore suitable excitation function will be sought to mitigate this problem.

All this has stimulated us to search for better solutions.

3. Combined Stochastic Algorithm

Let's consider the sample radiation pattern function given by the magnitude

$$P(\theta) = \frac{1}{N+1} \sum_{n=-N/2}^{N/2} \exp\{j2\pi(\sin\theta - \sin\alpha)(nd_x + X_n)\} \quad (7)$$

where the positions are a linear combination of deterministic one and random one. The AF $|P(\theta)|^2$ consists of two parts. The first part is periodic function and if $d_x > \lambda/2$ grating lobes can not be avoided — see Fig. 2.

Unlike, periodicity of the second part is strongly destroyed from random positions of x_n . It is equivalent of non-uniform spacing and there is no grating lobes, but on the price of relatively high SLL — see again Fig. 2.

The basic role of the algorithm for optimization both side lobes and grating lobes play positions $\{X_n\}$ of antenna elements. This vector $\{X_n\}$, $X_n \in \mathbb{R}^{N+1}$, or its normalized version $\{x_n\}$ creates the work space which plays a fundamental role. Generally $\{x_n\} = \{x_{n\det}\} + \{x_{n\rand}\}$. In Sect. 2, we have considered the models $\{x_{n\rand}\}$ and $\{x_{n\det}\}$ separately that were called RA and UA respectively. In terms of MATLAB

$$\{x_{n\text{det}} = ((-N/2) : 1 : (N/2))/N\} \quad (8)$$

$$\{x_{n\text{rand}} = \text{rn} = -1/2 + \text{rand}(1, N)\} \quad (9)$$

and each of the two workspaces operates over the interval $[-1/2, 1/2]$. Equation (8) means a uniform spacing with N elements in $[-1/2, 1/2]$. Equation (9) means a random spacing with N elements in $[-1/2, 1/2]$.

Let's consider the model (7) over

$$\{x_n\} = \{x_{n\text{det}}\} + \{x_{n\text{rand}}\}, \quad (10)$$

which operates over two times larger workspace. It is non-uniform spacing stochastic algorithm, which suppresses grating lobes, but with respect to SLL it is almost the same as RA algorithm, even with two time larger aperture.

Let's put forward the model (7) over

$$\begin{aligned} \{x_n\} &= \{x_{n\text{det}}\} + \{\varepsilon_{n\text{rand}}\} \\ \{\varepsilon_{n\text{rand}}\} &= \{x_{n\text{rand}}\} / N \end{aligned} \quad (11)$$

where $\{\varepsilon_{n\text{rand}}\}$ is a small random perturbation of the deterministic workspace and N is the number of elements. This model will be called Combined Stochastic Algorithm (CSA) and will compete with existing UA and RA algorithms. Our algorithm is a non-uniform spacing stochastic algorithm, where random workspace is strongly reduced, and positions $\{x_{n\text{rand}}\}/N$ play the role of very small random perturbations around the deterministic positions $\{x_{n\text{det}}\}$. The aperture of antenna array remains unchanged. This algorithm as we will see has any advantages with respect to both UA and RA algorithms. To compare all these models with respect to near and far SLL is more convenient to represent array factor

$$AF = |P(\theta)|^2 \quad (12)$$

or its averaged version as a function of observation angle θ . So we can directly observe, that when N increases the beamwidth becomes narrower and the effect of broadening the beamwidth, when we apply non-uniform amplitude tapering.

In the figures to be followed one depicts array factor $|P(\theta)|^2$ or its averaged version into the near zone around the main beam or entire visible range when changing any parameters. All the figures are prepared for $f = 5.8\text{GHz}$ and 181 observation points ($N_{\text{data}} = 181$) for which the array factor $|P(\theta)|^2$ is calculated. The scan angle α is adjusted to zero degree. The averaged version of the AF is obtained by repeating algorithm one hundred times or more and taking the mean operator of gathered statistics. We have used averaging only to calculate area under the array factor but our CSA does not work by averaging. The final design of antenna element positions is subject to Monte Carlo simulations. However, we do not discuss the Monte Carlo simulations in this paper. All figures are prepared with uniform probability density function and with or without non-uniform amplitude excitation function.

We compare two stochastic algorithms (RA, CSA) with uniform array algorithm (UA) and must clearly distinguish uniform spacing (deterministic) from non-uniform spacing

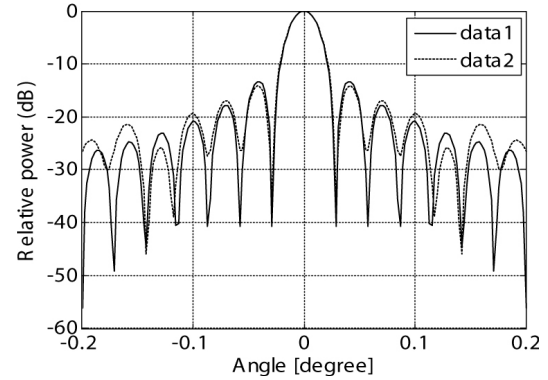


Fig. 3 Radiation characteristics of CSA (data1) and RA (data2), $N=1000$ and uniform excitation $d_{av} = 2\lambda$, $\theta \in [-0.2^\circ, 0.2^\circ]$.

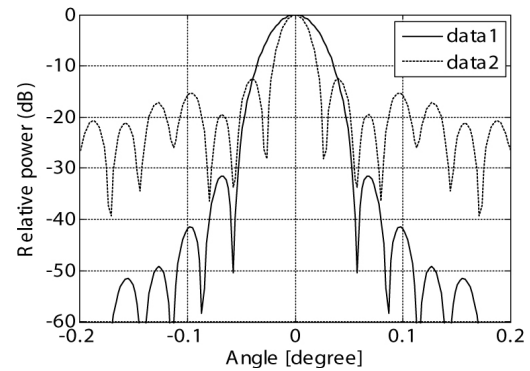


Fig. 4 Radiation characteristics of CSA (data1) and RA (data2), $N=1000$ and $\cos^2(\pi x/2)$ excitation $d_{av} = 2\lambda$, $\theta \in [-0.2^\circ, 0.2^\circ]$.

with uniform pdf $f(x)$ (random).

In Fig. 3, one can see a comparison between the array factors of our algorithm CSA with those of Lo's algorithm RA in the near zone of the main beam, $\theta \in [-0.2^\circ, 0.2^\circ]$, $N = 1000$ and without amplitude tapering of element's excitation, or all elements (with isotropic radiation) are equally excited. There is no substantial difference between the two algorithms. The behavior of our model is almost the same as UA model.

Now let's repeat Fig. 3 by applying a non-uniform excitation function of the kind $\cos^2(\pi x/2)$. In Fig. 4, one can see that in the near zone our algorithm CSA, with non-uniform amplitude tapering, outperforms the Lo's algorithm RA and broadening of beamwidth appears [2]. Its behavior is again nearly the same as UA algorithm.

A special attention deserves the algorithm CSA into the zone larger than that around the main beam $\theta \in [-15^\circ, 15^\circ]$, see Fig. 5 and Fig. 6. For the SPS in geostationary orbit above 36,000 km, it is very important to suppress the SLL within $\pm 8^\circ$ because it covers all the surface of the Earth from the geostationary orbit. One can see a strong reduction of SLL in this zone, which further is constant up to the bounds of entire visible range. The effect of the CSA is occurred by the mixing of UA and RA (see Eq. (11)). In near main-lobe, the strong reduction of the sidelobe levels is occurred

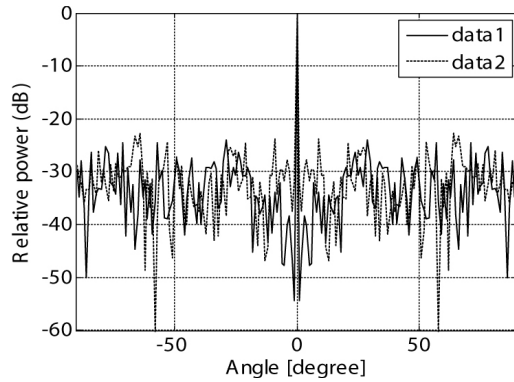


Fig. 5 Radiation characteristics of CSA (data1) and RA (data2), $N=1000$ and uniform excitation $d_{av} = 2\lambda$, $\theta \in [-90^\circ, 90^\circ]$.

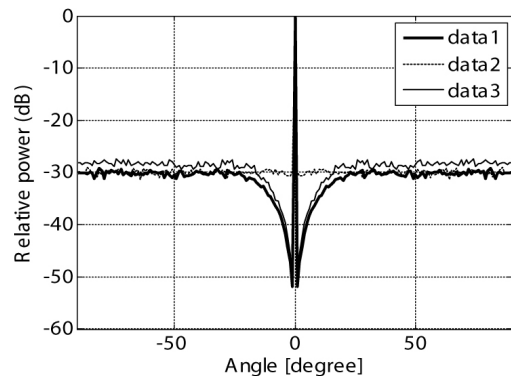


Fig. 6 Average patterns of the CSA (data1) and RA (data2) for uniform excitation and CSA (data3) for $\cos^2(\pi x/2)$ excitation, $N=1000$, $d_{av} = 2\lambda$.

by the UA positioning. The beam pattern of the CSA is very close to that of the UA in near mainlobe. In far mainlobe, the averaged pattern is occurred by the RA. We can control the angle and the reduction level of the strong reduction of the SLL when we change the parameter N in Eq. (11) as a variable number which is considered as fixed number in this section. In Sect. 4, we show a formula and some calculations by changing N which corresponds to c_1 and c_2 in Eq. (13). The angle and the reduction level of the strong reduction of the SLL also depend on the element number N . It is very important to formulate the reduction of the SLL, however, we have not formulated it yet. By applying amplitude tapering with $\cos^2(\pi x/2)$ this level becomes a little higher. This effect may be attractive for MPT and does contribute for less area under the SLL.

From now on in the entire visible range will be used suitable amplitude excitation function which concerns the beamwidth and influence to transmitting efficiency and beam collection efficiency.

Let's see the behavior of our algorithm when N increases and what could we expect as minimum of SLL. Now let's increase number of elements N to 16000, 32000 and 64000. In Fig. 7 and Fig. 8 we fix again entire visible range and no amplitude tapering use.

One can see the influence of number of elements over

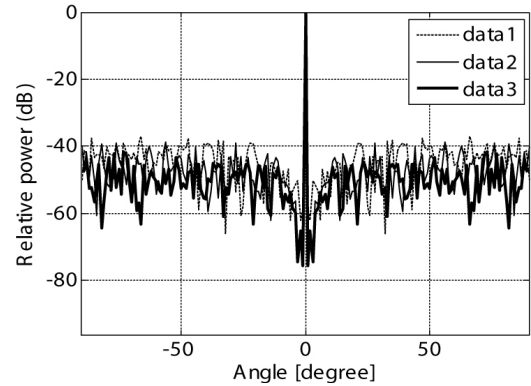


Fig. 7 Radiation characteristics of the CSA, $N=16000$ (data1), $N=32000$ (data2) and $N=64000$ (data3), $d_{av} = 2\lambda$ and uniform excitation.

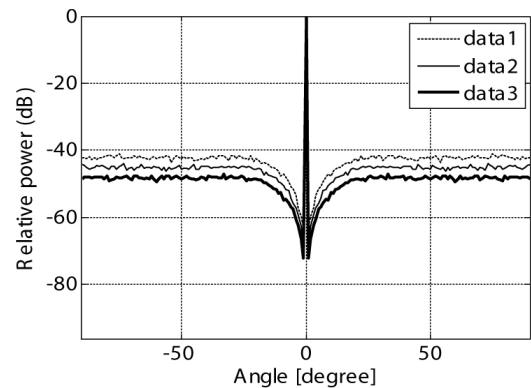


Fig. 8 Average patterns of the CSA algorithm with uniform excitation for $N=16000$ (data1), $N=32000$ (data2) and $N=64000$ (data3), $d_{av} = 2\lambda$.

peak SLL. For $N=16000$ elements this level according to (5) is below -35 dB with 90% probability of success. When increasing this number to $N=32000$ and 64000 the peak SLL is below -37.5 dB and -40 dB respectively. So a large amount of elements need to decrease a little peak SLL. The average SLL for $N=16000$, $N=32000$ and $N=64000$ is respectively -42 dB, -45 dB and -48 dB — see Fig. 8.

4. Further Development of the Problem of Minimization of SLL

Let's rewrite Eq. (11) as follows:

$$\{x_n\} = c_1 \{x_{n \det}\} + c_2 \{x_{n \text{rand}}/N\} \quad (13)$$

The influence of these two constants c_1 and c_2 over the behavior of the workspaces $\{x_{n \det}\}$ and $\{x_{n \text{rand}}\}$ reveals an interesting properties of our algorithm, which was studied in previous section with $c_1 = 1$ and $c_2 = 1$. We have found experimentally the following set of constants.

$\{c_1 = 0.93, c_2 = 0.1\}$ to improve minimization of SLL and no gratings lobes appear — compare Fig. 9 and Fig. 7. Let call this model improved combined stochastic algorithm (ICSA). From now on into entire visible range will be used suitable amplitude excitation function which concerns the beamwidth and influence to transmitting efficiency and

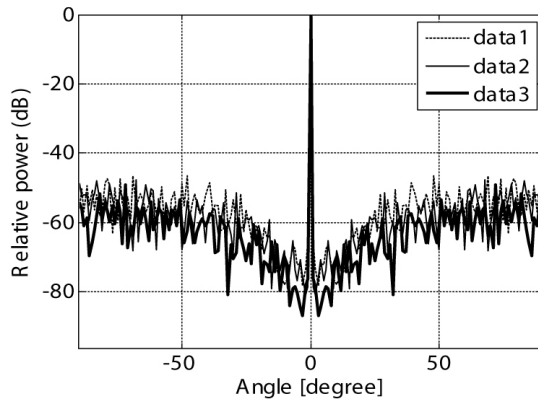


Fig. 9 Radiation characteristics of the ICSA, $N=16000$ (data1), $N=32000$ (data2) and $N=64000$ (data3), $d_{av} = 2\lambda$ and $c_1 = 0.93$, $c_2 = 0.1$.

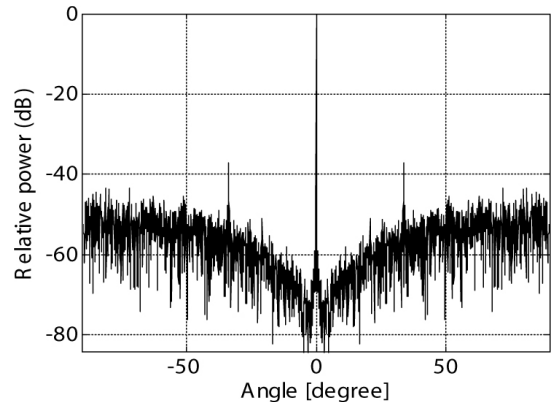


Fig. 12 Radiation characteristics of the ICSA, $N=16000$, $d_{av} = 2\lambda$, $c_1 = 0.90$, $c_2 = 0.1$.

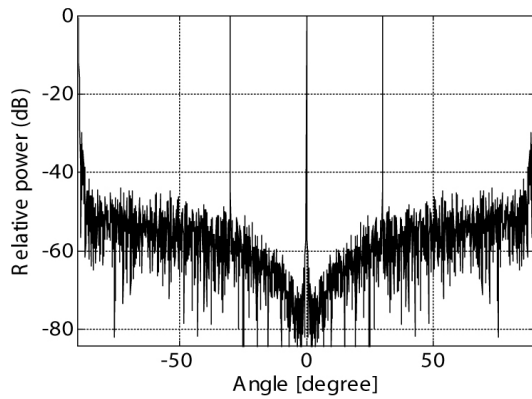


Fig. 10 Radiation characteristics of the ICSA, $N=16000$, $d_{av} = 2\lambda$, $c_1 = 1$, $c_2 = 0.1$.

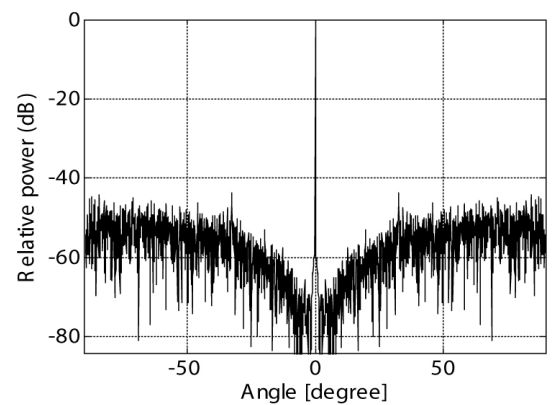


Fig. 13 Radiation characteristics of the ICSA, $N=16000$, $d_{av} = 2\lambda$, $c_1 = 0.93$, $c_2 = 0.1$.

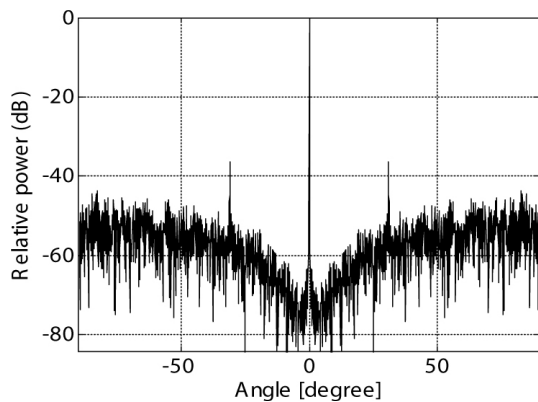


Fig. 11 Radiation characteristics of the ICSA, $N=16000$, $d_{av} = 2\lambda$, $c_1 = 0.97$, $c_2 = 0.1$.

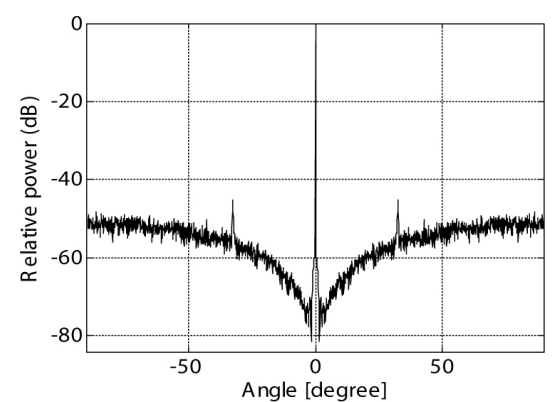


Fig. 14 Average patterns of the ICSA, $N=16000$, $d_{av} = 2\lambda$ and $c_1 = 0.93$, $c_2 = 0.1$.

beam collection efficiency.

Let study our algorithm with $c_1 = 1$, $c_2 = 0.1$; $c_1 = 0.97$, $c_2 = 0.1$; $c_1 = 0.90$, $c_2 = 0.1$ for $N=16000$. To avoid false effect let enhance N_{data} to 1801—see Fig. 10 to Fig. 14. With not enough data point (for example $N=181$) the resolution is low and we can not register grating lobe. It is ‘false effect.’ One can see when decreasing c_2 grating lobes appear. Such grating lobes appear also for $N=32000$

and $N=64000$. We have found experimentally the optimum value of $c_1 = 0.93$. We have reduced SLL in comparison with Fig. 8, independently that a little amount (-45 dB) of grating lobes remains. When decreasing c_2 further the SLL decreases too but grating lobes remains the same.

Let’s further consider the opportunity of using our model with $d_{av} = \lambda$. It is equivalent to shorten the aperture two times with the same number of elements. On the

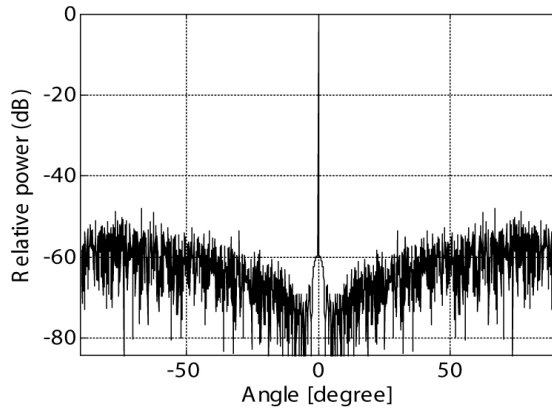


Fig. 15 Radiation characteristics of the ICSA, $N=16000$, $d_{av} = \lambda$, $c_1 = 0.93$, $c_2 = 0.1$.

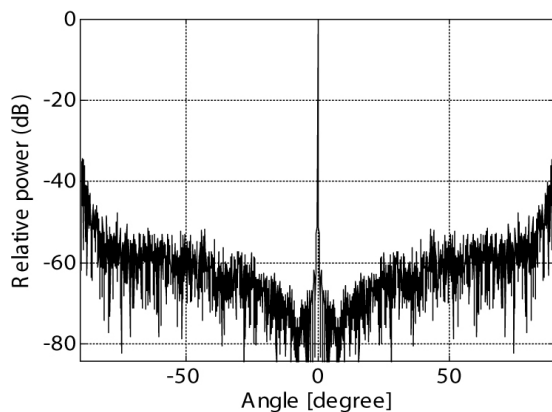


Fig. 16 Radiation characteristics of the ICSA, $N=16000$, $d_{av} = \lambda$, $c_1 = 0.99$, $c_2 = 0.1$.

Fig. 15 and Fig. 16 one can see Radiation characteristics and Average patterns for the set of constants $c_1 = 0.93$, $c_2 = 0.1$. At this we can increase c_1 up to 0.97 without grating lobes appear.

Comparing with Average patterns of Fig. 8 one can see a considerably improvement of SLL for $N=16000$ —from -42 dB (In Lo's algorithm this average level is constant) to -58 dB. There is not grating lobes.

A little enhancement of c_1 to 0.99 causes again grating lobes—see Fig. 16.

Really, stochastic part of our algorithm plays the role of very small perturbation of deterministic workspace.

For $N=32000$ and $N=64000$ the aperture becomes two and four times larger, the beam becomes more and more narrow and transmitted power higher. However, for many reasons the aperture dimensions can not be limitless enlarged and this problem will be discussed further.

5. Two-Dimensional Array

Often, for a rectangular array aperture, a separable amplitude distribution is chosen and the array factors for UA (2) and RA (1) can be written as the product of two independent factors. For the RA with a rectangular aperture of $ab\lambda^2$

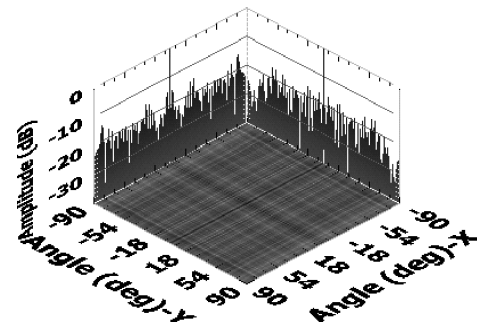


Fig. 17 Radiation characteristics of the RA with uniform excitation, $N=101$, average spacing, $d_{av} = \lambda$, $\theta \in [-90^\circ, 90^\circ]$.

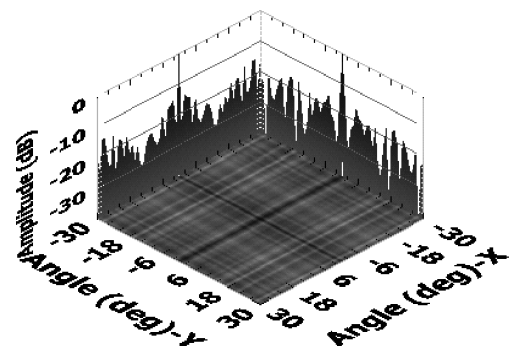


Fig. 18 Radiation characteristics of the RA with uniform excitation, $N=101$, average spacing, $d_{av} = \lambda$, $\theta \in [-30^\circ, 30^\circ]$.

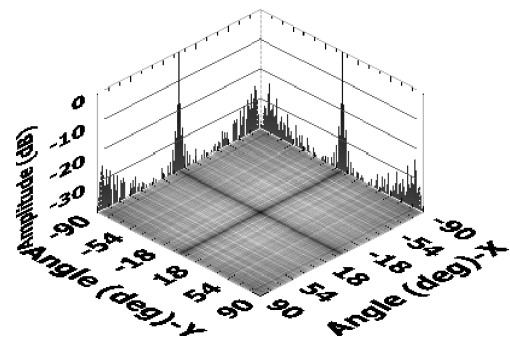


Fig. 19 Radiation characteristics of the ICSA with uniform excitation, $N=101$, average spacing, $d_{av} = \lambda$, $\theta \in [-90^\circ, 90^\circ]$.

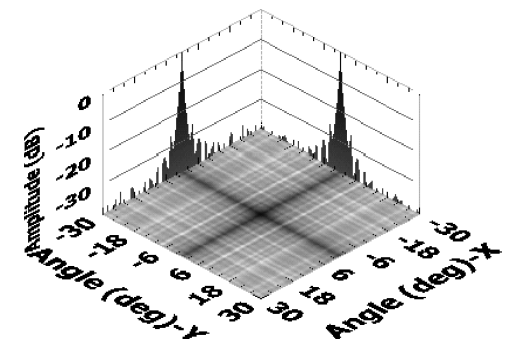


Fig. 20 Radiation characteristics of the ICSA with uniform excitation, $N=101$, average spacing, $d_{av} = \lambda$, $\theta \in [-30^\circ, 30^\circ]$.

in the xy plane with a probability density function $f(x)f(y)$ is chosen. Then the relation between the total number of elements and the SLL is still approximately given by (5), except that [4a] is replaced by [16ab]. The desired SLL will be achieved with a square of predetermined confident probability of success such as 0.9, 0.95 etc.

However, with elements 16000, 32000 and 64000 that we have used in our simulations it is impossible to simulate two-dimensional radiation patterns with ordinary computer resources. At Fig. 17 to Fig. 20 we have depicted two-dimensional implementation of radiation characteristics of the algorithms RA and ICSA for $N=101$. One can see the same strong reduction of SLL occurs in the two-dimensional radiation patterns as in the one-dimensional radiation patterns.

6. Transmitting and Beam Collection Efficiency

To be determined the transmitting efficiency (TE) will be used the area under the peak SLL and the area under the main beam. Then transmitting efficiency can be presented as follows

$$TE = \frac{MB_{\text{area}}}{MB_{\text{area}} + SLL_{\text{area}}} \quad (14)$$

where MB_{area} is main beam area and SLL_{area} is side lobe area. The main beam area is defined as $4\text{ km}\phi$ at the center of beam in this paper.

When N increases, the area of main beam decreases, but average SLL decreases too. It is not accurate to use average SLL, but rather the envelope of peak values of SLL obtained with large amount of observation points $N_{\text{data}}=1801$ in our simulations—see Fig. 15, which we have pre-

pared also for $N=32000$ and $N=64000$. The envelop of peak values of SLL reaches respectively -51 dB , -53 dB and -55 dB .

In Fig. 21 we turn back again to the near zone which becomes narrower and narrower when the number of element N increases. In this figure ICSA is with non-uniform

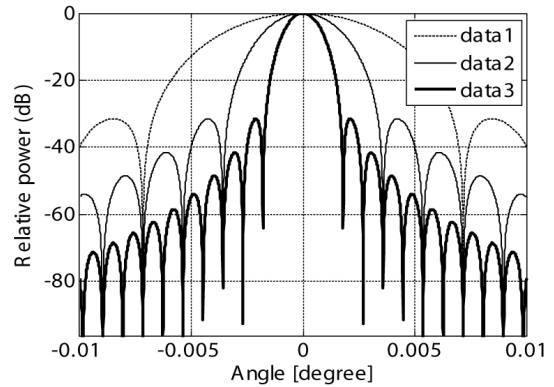


Fig. 21 Radiation characteristics of the ICSA average spacing $d_{\text{av}} = \lambda$ with non-uniform excitation of $\cos^2(\pi x/2)$, $N=16000$ (data1), $N=32000$ (data2) and $N=64000$ (data3).

Table 1 Characteristics of the transmitting part of the system for MPT.

Number of PCM	Number of Antenna Elements	Number of elements in Sub-array	Power [GW]	Diameter [m]		
				TE		
				$d_{\text{av}} = c_1 \lambda$	η_{1D}	η_{2D}
1600	16000	10	1.02	769	0.9067	0.8221
2134	32010	15	1.82	1538	0.8831	0.7799
2560	64000	25	2.62	3076	0.8580	0.7362

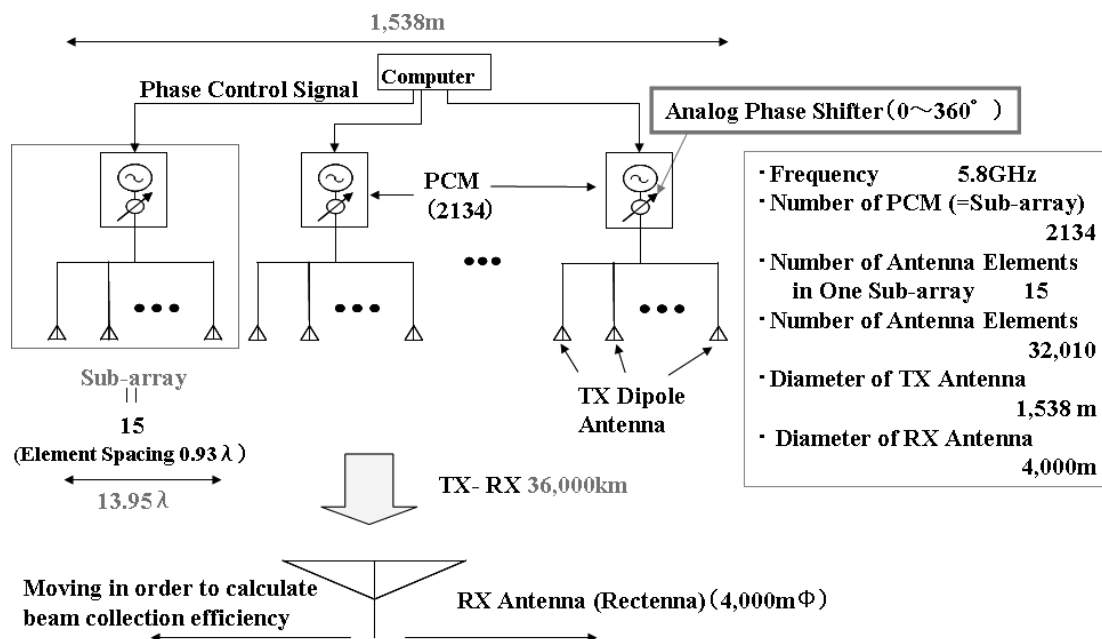


Fig. 22 Block chart of considerable SPS transmitting array. Parametrs are one example for calculation in Table 1.

amplitude tapering with $\cos^2(\pi x/2)$.

Beam collection efficiency (BCE) of the MPT system is the ratio of power that is intercepted by the rectenna to the whole transmitted power and can be expressed as:

$$BCE = \frac{\int_{\theta_r} |P(\theta)|^2 d\theta}{\int_{\theta_w} |P(\theta)|^2 d\theta} \quad (15)$$

where $|P(\theta)|^2$ is the power, θ_r is the angle sector due to rectenna and θ_w is the angle sector $\pm 90^\circ$. One can see from (15) that the lower SLL enhances the BCE.

In Table 1 are presented the features of the transmitting part of the system for MPT, which is shown in Fig. 22, depend on number of elements and possible reduction of workspace. A concept of "units" (sub-arrays or phased controlled magnetrons (PCM)) is adopted [26]. η_{1D} is one dimensional transmitting efficiency of linear array, calculated on the base of Eq. (14) and η_{2D} is two dimensional transmitting efficiency calculated as product of η_{1D} by itself and finally used; The diameter of transmitting antenna in [m] is indicated for different number of antenna elements.

The basic conclusion is that with ICSEA we can achieve a low SLL and no grating lobes appear with reduced number of antenna elements in comparison with conventional Uniform array.

7. Conclusion

1. The pure stochastic algorithms with average spacing more than λ (thinned arrays) really suppress grating lobes but on the price of sufficiently high SLL. So a large amount of elements need to decrease a little SLL.
2. Deterministic non-uniformly spaced algorithms are numerically difficult to implement for large antenna arrays.
3. We propose a new combined stochastic algorithm. It is a new unified approach in searching for reducing SLL by exploiting the interaction of deterministic and stochastic workspaces. It is a non-uniform spacing stochastic algorithm. Really, stochastic part of our algorithm plays the role of very small perturbations of deterministic workspace. So we have succeeded to reduce SLL considerably with out grating lobes appear and achieve high TE and BCE.
4. We propose a new concept of designing the transmitting part of the whole system for MPT.
5. Our study and simulation results clarify how to deal with the problems of side lobes and grating lobes in designing a large antenna array, which seems to be an important step toward the realization of future SPS/MPT systems.

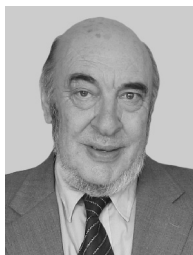
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